

## Re: PER Drainage design review

(b) (4) [REDACTED]  
[REDACTED]@gallupsurveyors.com>

Mon 11/11/2013 11:32 AM

To: (b) (4) [REDACTED]@eaest.com>;

Cc: Sturgeon, Randy <Sturgeon.Randy@epa.gov>; (b) (4) [REDACTED]@eaest.com>;  
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Categories: PER

1 attachments (3 MB)

PER DITCH STUDY.pdf;

Gentlemen,

See my response to comment 4 below, along with the attachments. Please call or write me if you have any questions.

Thanks-

David Butler

----- Original Message -----

**From:** (b) (4) [REDACTED]  
**To:** (b) (4) [REDACTED]@gallupsurveyors.com  
**Cc:** Sturgeon, Randy (Sturgeon.Randy@epa.gov) ; (b) (4) [REDACTED]  
(b) (4) [REDACTED]@advantusstrategies.com> (b) (4) [REDACTED]@advantusstrategies.com) ; (b) (4) [REDACTED]  
(b) (4) [REDACTED]@salmonsinc.com  
**Sent:** Wednesday, October 23, 2013 1:55 PM  
**Subject:** PER Drainage design review

(b) (4) [REDACTED]

EA has reviewed the latest drainage design and calculations for the PER property sent to EA on October 22. EA concurs with the submitted calculations and approach to manage the 100-year runoff from the 3975 Elm Avenue property. However, the pre- versus post-development ponding conditions have still not been quantified along the 3975 Elm Avenue/PER property line to show improvements to drainage conditions (see #4 below). The storm drain plan view layout has not changed since the last submittal but the storm drain pipe sizes have been increased and the pipe inverts have generally been lowered to decrease the water surface elevations in the system during the 100-year rainfall event. Additionally, a TideFlex valve has been added to the outfall of the storm drain system which conveys water from the 3975 Elm Avenue property. The following are EA comments provided to you on October 2 (in black) followed by EA's observations of the revised October 22 submission in red:

1. The times of concentration for runoff to reach each inlet appear high. This would affect the rainfall intensity, design flow rates, and performance of the system. Please confirm that 20-25 minutes is appropriate for the small drainage areas, especially since much of the area contains impervious surfaces.



The times of concentration have been revised and are appropriate for the drainage area size and land use. Additionally, the runoff coefficients (indicating imperviousness) have been revised to assume the 3975 Elm Avenue property will be fully developed in the future. Previous comment has been satisfied.

2. There appears to be a problem with the hydraulic grade line (HGL) calculations. Many of the computed HGLs are below the pipe inverts (Inlets 7, 6A, 4, 3, 2, 1, and 1A). This may be due to the friction slope used in the HGL calculations which are significantly different from the pipe slopes.

The hydraulic grade line calculations have been revised. The HGLs downstream of the 3975 Elm Avenue property are well below the proposed ground elevation of the PER improvements. HGLs along the 3975 Elm Avenue/PER property boundary are discussed in detail below.

3. Once the HGLs are corrected, it will be important to check the HGL at each manhole/flushed end section (FES) along the PER/3975 Elm Avenue property line to make sure water is not ponding along the proposed retaining wall. As a suggestion, it appears that the storm drain could be lowered to accommodate total capture of runoff from the 3975 Elm Avenue property with no backup. See attached "property line" pdf for concept. Please provide similar cross sections at critical points along the retaining wall for review (especially at STMH-4). Mr. (b) (6) is concerned with additional flow/velocity along the 3975 Elm Avenue property undercutting the existing concrete pad on his property. A cross section with HGL shown (similar to the attached pdf) may ease those concerns.

The HGL at each manhole/FES along the 3975 Elm Avenue/PER property line are contained within the existing ditch. There are 5 FESs along the property line that collect runoff from the 3975 property ranging in size from 12 inches to 36 inches. Water will pond in the ditch while the storm drain is flowing full during the 100-year storm event up to 1 foot as runoff enters the FESs.

4. Pete met with Mr. (b) (6) on 9/24 to discuss drainage patterns of the 3975 Elm Avenue property. Attached is an annotated C2 sheet indicating the drainage patterns on the property as described by Mr. (b) (6) and as confirmed during the visit. EA strongly suggests using similar drainage area delineations to the attached annotations to demonstrate to Mr. (b) (6) that his concerns have been addressed. Also, Mr. (b) (6) is very concerned about the capacity of the ditch between the PER property and his, and he is also very concerned about maintaining positive drainage from this area in the pipe along the swale alignment you are proposing. EA strongly suggests that you perform a pre-development conditions analysis to demonstrate that the proposed PER development will improve the drainage along the PER/3975 Elm Avenue property boundary in the post-development condition. This could be demonstrated through improved water surface elevations and lack of ponding in the ditch between the two properties.

The drainage areas have been revised per EA recommendations and recommended flow patterns have been accounted for. There is ponding in the ditch of up to one foot while runoff enters the storm drain system. Although the system has been designed to collect runoff and convey flows to the outfall effectively, without any significant ponding, it is unknown how this compares to the pre-development condition water surface elevations in the ditch as a pre-development analysis was not performed for comparison. EA still strongly suggests showing a calculation for the pre-development condition runoff and corresponding depth in the property line ditch for comparison to the post-development condition. It is anticipated that a simple flow rate calculation for the 3975 Elm Avenue property and a cross section calculation using Manning's equation would be sufficient to show the pre-development flow depth in the ditch. Additionally, EA recommends adding check dams immediately downstream of each lateral inlet/FES into the main pipeline along the PER/3975 Elm Avenue property boundary to more effectively collect and drain the runoff from the ditch and to reduce the potential of bypass.



Check dams have been added just downstream of flared end sections at structures 1, 1A, 2, and 3. See plan sheets C4 and C5 and detail shown on sheet C7. Calculations for pre and post ponding elevations for two cross sections, A-A and B-B are provided on three 8.2 x 11 sheets. Conclusions on the bottom of sheets 2 and 3 show a lower water surface elevation in the ditch, post developed situation. The ditch in a pre developed state does not have adequate capacity for most of its length. The ditch, altered with the addition of a retaining wall, has capacity and 100 year flows are contained. The reason for the radical difference in pre and post states is most of the water that outfalls to the ditch from the (b) (6) side is intercepted by a new flared end section and piped in an storm sewer independent of the PER storm sewer. Additional, some of the overland flows from the PER site are eliminated in the post development state. See 2 attached drainage area maps. The (b) (6) water is piped and outfalls in the upper reaches of the current ditch and because of lack of slope and the general geometry of the trapazoidal ditch, it does not have capacity for the design storm in its existing predeveloped state. If and when the (b) (6) tract is developed, PER will have provided a storm sewer to accommodate 100 year (quantity, not quality) flows from the (b) (6) site.

Please let Jason Coleman or myself know if you have any further questions.

Pete Pellissier



## PRE DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH

SHEET 1 OF 3  
11/9/13

CHECK WATER SURFACE ELEVATION OF EXISTING DITCH BETWEEN PER AND DIXON: THE WATER SURFACE ELEVATION WILL BE CHECKED AT VARIOUS LOCATIONS ALONG THE RECENTLY CUT PERIMETER DITCH BASED ON FLOWS FROM A PRE DEVELOPMENT STAGE. THE DIXON PROPERTY HAD A DITCH IN THE SAME GENERAL LOCATION PRIOR TO PER PURCHASING THE PROPERTY AND THAT DITCH IS DEPICTED ON THE STEVE BOONE TOPOGRAPHIC SURVEY. SHORTLY AFTER PER PURCHASED AND CLEARED THE PROPERTY, A NEW TRAPAZOIDAL DITCH WAS CUT. THIS DRAINAGE ANALYSIS WILL ATTEMPT TO DETERMINE THE WATER SURFACE ELEVATION IN THE RECENTLY CUT TRAPAZOIDAL DITCH BASED ON A PRE DEVELOPMENT STATE.

PER PLANS ON INSTALLING A RETAINING WALL ON THE PER SIDE, 36" EAST OF THE COMMON BOUNDARY LINE. INSTALLING THE WALL WILL ALTER THE CROSS SECTIONAL GEOMETRY OF THE TRAPAZOIDAL DITCH. CALCULATIONS WILL BE PERFORMED TO DETERMINE THE WATER SURFACE ELEVATION OF THE ALTERED DITCH BASED ON POST DEVELOPMENT CONDITIONS.

### SECTION A-A SHOWN ON PRE DEVELOPMENT DRAINAGE AREA MAP:

TOTAL DRAINAGE AREA: 135,343 S.F.=3.1070 ACRES  
PERVIOUS AREA @ C FACTOR=0.2, 37,539 S.F.=0.8618 ACRES; CA=0.1724  
PERVIOUS AREA @ C FACTOR=0.3, 42,388 S.F.=0.9731 ACRES; CA=0.2919  
IMPERVIOUS AREA @ C FACTOR=0.9, 55,416 S.F.=1.2722 ACRES; CA=1.1450  
SUM OF THE CA's=1.6093; C=0.5179

#### TIME OF CONCENTRATION:

200 L.F. OF OVERLAND FLOW @ 1.5% = 22.5 MINS

151 L.F. OF CHANNEL FLOW @ 1.5 FPS = 1.7 MINS

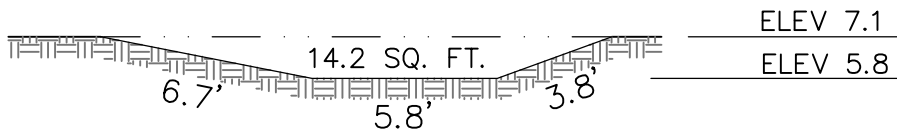
SUM  $T_c$  = 24.2 MINS

$I_{100} = 285.2/24.7+24.2 = 5.83$  IN/HR.

$I_{10} = 201/23.9+24.2 = 4.18$  IN/HR.

$Q_{100} = 1.6093 \times 5.83 = 9.4$  CFS

$Q_{10} = 1.6093 \times 4.18 = 6.7$  CFS



### SECTION A-A

$WP = 6.7 + 5.8 + 3.8 = 16.3'$

$XS\ AREA = 14.2\ S.F.$

$R = A/WP = 14.2/16.3 = 0.87$

$N\ FACTOR\ FOR\ LINING = 0.45$

$SLOPE\ OF\ DITCH = 0.005\ FT/FT$

$Q = 1.486/N \times A \times R^{0.67} \times S^{0.50}$  EQUALS DITCH CAPACITY  
 $Q\ CAPACITY = 3.02 << 6.7\ OR\ 9.4\ CFS$

WATER SURFACE ELEVATION AT SECTION A-A IS 7.1 SINCE IT IS NOT CONTAINED WITHIN THE GEOMETRY OF THE DITCH SECTION.



# POST DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH

SHEET 2 OF 3  
11/9/13

## NOTE:

END SECTION AT STMH-1 TAKES IN 1.93 ACRES FROM THE DIXON TRACT PIPE OUTFALLING AT THAT LOCATION. 1.93 ACRES WILL NO LONGER FLOW THROUGH THE DITCH, BUT WILL BE INTERCEPTED BY THE NEW PER STORM DRAIN AT STMH-1

AREAS DRAINING TO THE DITCH AT AND UPSTREAM OF SECTION A-A

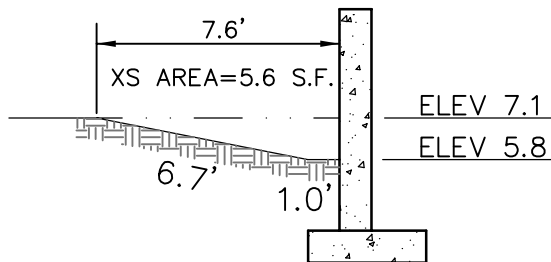
3199 S.F. = 0.0734 AC. X 0.5 = CA = 0.0367

1672 S.F. = 0.0384 AC X 0.5 = CA = 0.0192

SUM CA's: 0.0559

Tc=5 MINS, I100=28502/24.7+5 = 9.60 IN./HR.

Q100=0.0559 X 9.6 = 0.54 CFS



## SECTION A-A

WP=6.7+1.0=7.7

XS AREA=5.6 S.F.

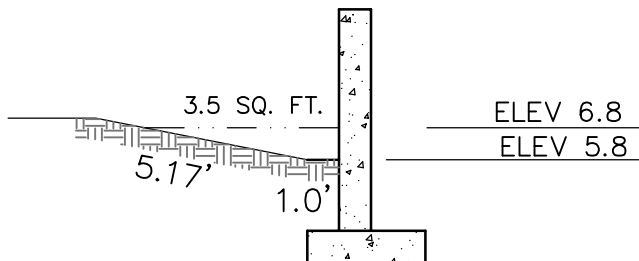
R=A/WP = 5.6/7.7 = 0.73

N FACTOR FOR LINING=0.45

SLOPE OF DITCH=0.005 FT/FT

$$Q = 1.486/N \times A \times R^{0.67} \times S^{0.50} = 1.05 \text{ CFS AT FULL DEPTH OF 1.3'}$$

CAPACITY



WATER DEPTH OF WATER=12": (ELEV 6.80)

WP=5.17+1.0=6.17

XS AREA=3.54 S.F.

R=A/WP = 3.54/6.17 = 0.57

N FACTOR FOR LINING=0.45

SLOPE OF DITCH=0.005 FT/FT

HW ELEV. FROM PIPE CALCULATION  
SHEET LD-269 SHOWS A HEADWATER  
ELEV. OF 6.67

6.80 > 6.67; CONTROLLING ELEV=6.80

$$Q = 1.486/N \times A \times R^{0.67} \times S^{0.50} = 0.56 \text{ CFS, APPROX. = TO 0.54 CFS}$$

CAPACITY

## CONCLUSION:

THE 100 YEAR STORM ON A PRE DEVELOPED CONDITION IS NOT CONTAINED IN THE EX. DITCH SECTION AND WILL REACH A MIN. ELEVATION OF 7.1 (TOP OF DITCH BANK); SINCE WATER IS REMOVED FROM THE DITCH VIA ONSITE GRADING AND WITH THE ADDITION OF A FES AT STMH-1, THE WATER SURFACE PROFILE ELEVATION IS LOWER AT POST DEVELOPED CONDITIONS.



## PRE DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH

SHEET 3 OF 3  
11/9/13

### AREAS:

3.107 AC. AT  $C=0.5179$ ,  $CA=1.6091$

1.2495 AC. AT  $C=0.25$ ;  $CA=0.3123$

SUM  $CA$ 's = 1.9214

### TIME OF CONCENTRATION:

OVERLAND FLOW TIME=22.5 MINS

CHANNEL TIME. 626 L.F. @ 1.5 FPS=6.95 MINS

SUM  $T_c$  = 29.45 mins

$1100=285.2/24.7+29.45 = 5.26$  IN./HR.

$Q_{100}=1.9214 \times 5.26 = 10.1$  CFS

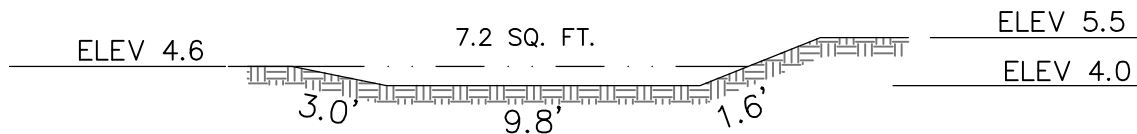
AVE DITCH SLOPE FROM XS A TO XS B:  $5.9-4.7/475' = 0.0025$  FT/FT

XS AREA TO ELEV. 4.6 = 7.2 S.F.

$WP=3.0+9.8+1.6=14.4'$

$R=7.2/14.4=0.50$

N FACTOR FOR LINING=0.45

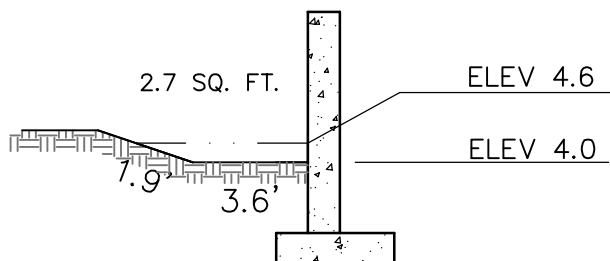


## SECTION B-B

$Q=1.486/N \times A \times R^{0.67} \times S^{0.50}$  EQUALS DITCH CAPACITY  
 $Q$  CAPACITY=0.74<<10.1 CFS

DESIGN STORM ON A PRE DEVELOPED CONDITION  
IS NOT CONTAINED IN THE DITCH GEOMETRY

## POST DEVELOPMENT CALCULATIONS FOR BOUNDARY DITCH



## SECTION B-B

### AREA DRAINING TO XS-B:

1514 S.F.=0.0347 AC.

$C=0.50$

$CA=0.0173$

$T_c=5$  MINS,  $1100=9.60$  IN/HR

$Q_{100}=0.17$  CFS

N FACTOR FOR LINING=0.45

AVG. DITCH SLOPE FROM XS A TO XS B:  $5.9-4.7/475' = 0.0025$  FT/FT

XS AREA TO ELEV. 4.6 = 2.7 S.F.

$WP=1.9'+3.6'=5.5'$

$R=2.7/5.5=0.49$

$Q=1.486/N \times A \times R^{0.67} \times S^{0.50}$  EQUALS DITCH CAPACITY  
 $Q$  CAPACITY=0.28 CFS

### CONCLUSION:

$Q_{100}$  POST DEVELOPMENT=0.17 CFS

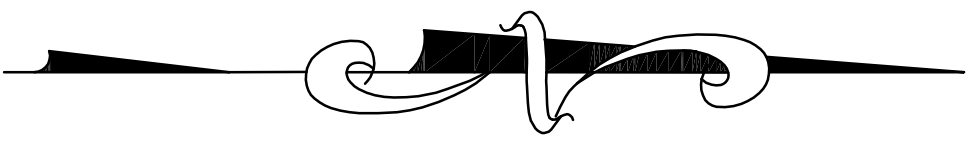
DITCH CAPACITY=0.28 CFS

WATER SURFACE ELEV. WILL BE LESS THAN TOP OF BANK ELEV OF 4.6

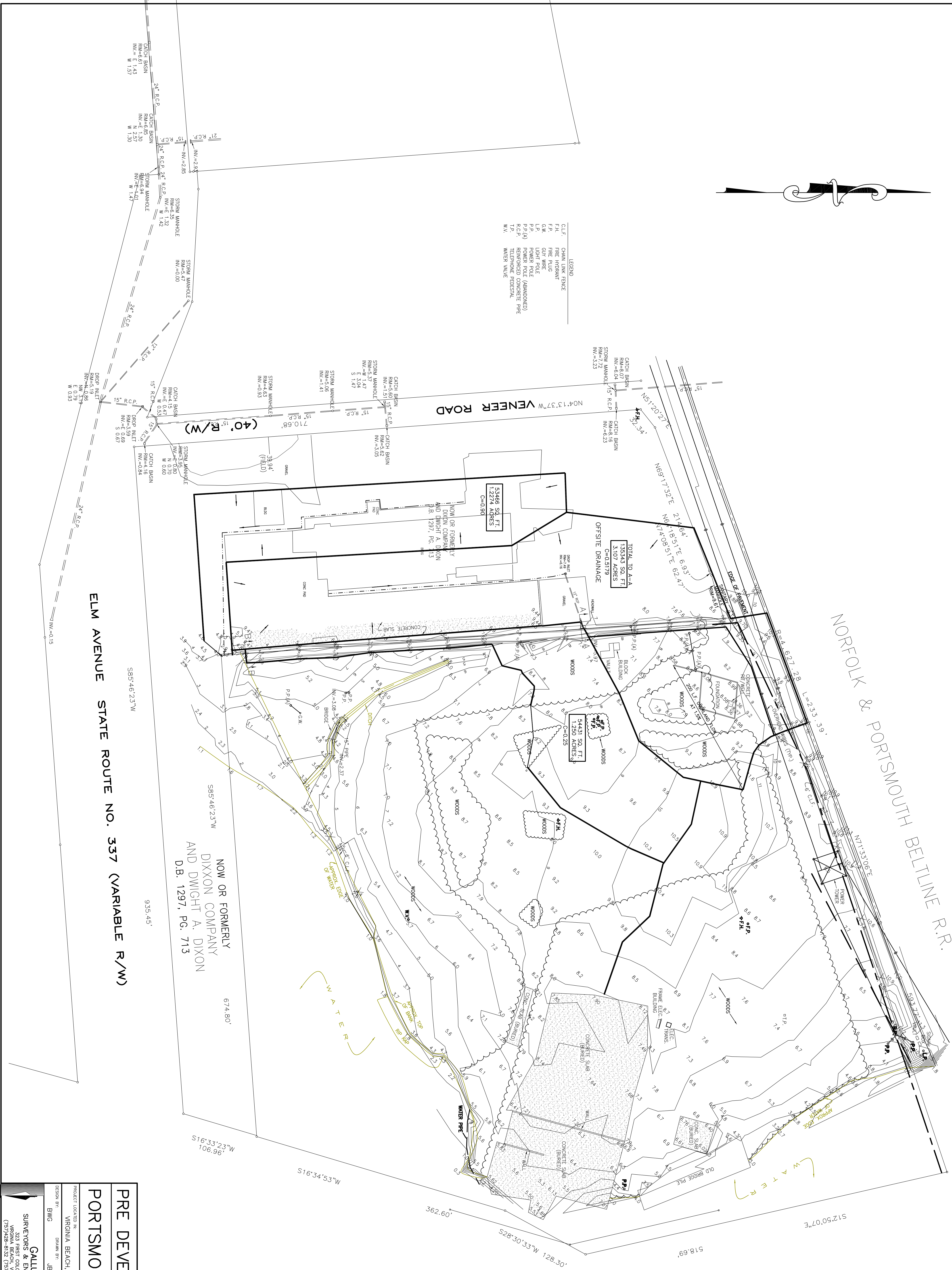
WATER SURFACE ELEV BEFORE DEVELOPMENT IS AT TOP OF BANK ELEV OF 4.6

SINCE THE STORM IS NOT CONTAINED.





- LEGEND
- CL.F. CHAIN LINK FENCE
  - F.P. FIRE PLUG
  - G.W. GUY WIRE
  - L.P. LIGHT POLE
  - P.P. POWER POLE (ARMORED)
  - P.P./A. REINFORCED CONCRETE PIPE
  - T.P. TELEPHONE FEEDSAL
  - W.V. WATER VALVE



ELM AVENUE STATE ROUTE NO. 337 (VARIABLE R/W)

PRE DEVELOPMENT DRAINAGE MAP  
PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN:		MADE FOR:	
VIRGINIA BEACH, VIRGINIA		PER PROPERTIES	
DESIGN BY:	BWG	CHECKED BY:	BWG
DRAWN BY:	JB	DATE:	OCTOBER 2, 2013
GALLUP		SCALE:	1" = 60'
SURVEYORS & ENGINEERS, LTD.			
VIRGINIA FIRST CLASS ROAD		SHEET	3 / 13
VIRGINIA RESURFACING ROAD			
(757) 428-8132 (757) 425-2380 FAX		C3	



1A.	STMH	RM 10.50	8. STMH	RM 9.50	108-24" HDPE @ 0.25%	108-24" HDPE @ 0.25%
	INV 4.37	INV -1.05	10.	RM 9.80	207-24" HDPE @ 0.25%	207-24" HDPE @ 0.25%
1.	STMH	RM 10.50		INV 4.77	104-11" HDPE @ 0.25%	104-11" HDPE @ 0.25%
2.	STMH	RM 10.50	11. DI	RM 9.80	198-24" HDPE @ 0.20%	198-24" HDPE @ 0.20%
	INV 4.04	INV 10.50		RM 9.35	112-12" HDPE @ 0.33%	112-12" HDPE @ 0.33%
3.	STMH	RM 10.50	12. STMH	RM 9.35	123-12" HDPE @ 0.33%	123-12" HDPE @ 0.33%
	INV 3.73	INV 3.33		INV 3.33	59-24" HDPE @ 0.34%	59-24" HDPE @ 0.34%
4.	STMH	RM 9.50	12A. DI	RM 9.50	121-24" HDPE @ 0.34%	121-24" HDPE @ 0.34%
	INV 3.20	INV 3.13		INV 3.13	18A-31" HDPE @ 0.34%	18A-31" HDPE @ 0.34%
5.	STMH	RM 9.35	13. DI	RM 9.35	109-13" HDPE @ 0.30%	109-13" HDPE @ 0.30%
	INV (E) -0.14	INV 2.49 (E/W.5)		INV 2.49 (E/W.5)	94-34" HDPE @ 0.33%	94-34" HDPE @ 0.33%
5.	STMH	RM 9.35		INV 7.29 (N)	109-18" PERFORATED HDPE @ 0.609%	109-18" PERFORATED HDPE @ 0.609%
	INV -0.37	INV 7.29 (N)	14. DI	RM 9.35	89-18" HDPE @ 0.30%	89-18" HDPE @ 0.30%
6.	DI	RM 9.35		INV 2.96	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV (E) -0.58	INV 9.35	15.	RM 9.35	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV (W) 1.87	INV (S) 3.41		INV 3.23	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV (S) 3.41				109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
7.	STMH	RM 10.50	7A. DI	RM 9.50	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV -0.86	INV (E) 3.40		INV (E) 3.40	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
5A.	DI	RM 9.80		RM 9.80	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV 4.10	INV 3.44		INV 3.44	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV 5.09	INV 9.35		INV 4.09	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
10A.	DI	RM 9.80		INV 4.09	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
	INV 4.25	INV 9.80		INV 9.80	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%
		INV -0.57		INV -0.57	109-18" HDPE @ 0.30%	109-18" HDPE @ 0.30%

THE SILT SACK PRODUCT SHOWN ON SHEET C7 IS TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN PERMANENT FOR DRAINAGE STRUCTURES

THE INVERTS SHOWN ON THE DROP INLET DENOTES THE INVERT OF THE PIPES. PROVIDE A 12" DEEP SLUMP (BELOW THE PIPE INVERT) ON THE DROP INLETS FOR MAINTENANCE PURPOSES FOR STRUCTURES 7A, 8A, 9A, AND 13.

O.W. DENOTES REQUIRED OBSERVATION WELLS  
SEE DETAIL ON SHEET C9.

ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET SHAPING  
FINAL SURFACE WILL BE GRAVEL AND CRUSHED CONCRETE

NOW OR FORMERLY  
UNITED STATES OF AMERICA  
D.B. 611, PG. 293

## PIPE SCHEDULE

14-13	4-5	36" HOPE @ 0.15%
196'-5.5"	13-12	HOPE @ 0.15%
INV IN 2.66, INV OUT 2.49	13-11	HOPE @ 0.14, INV OUT -0.37
13-14	5-6	
215'-18" PERFORATED HOPE @ 0.23%	154'-36"	HOPE @ 0.13%
INV IN 2.49, INV OUT 2.00	INV IN -0.37, INV OUT -0.57	
7A-6	6A-7	
344'-36"	220'-36"	HOPE @ 0.13%
INV IN 4.00, INV OUT 1.67	INV IN -0.57, INV OUT -0.86	
8A-7A	7-8	
215'-22"	158'-36"	HOPE @ 0.17%
CL, RCP @ 0.67%	152'-36"	HOPE @ 0.15%
INV IN 3.44, INV OUT 2.00	ON OUTLET	INV IN -1.05, INV OUT -1.05
5A-6	6A-7	
154'-6"	152'-36"	HOPE @ 0.13%
HOPE @ 0.51%	INV IN -1.05, INV OUT -1.23	
INV IN 5.09, INV OUT 3.41	PROVIDE TIEFLY TF-1	
6-0-OUTLET	ON OUTLET END	
144'-42"	HOPE @ 0.50%	
INV IN -0.58, INV OUT -1.30		
PROVIDE TIEFLY TF-1		
ON OUTLET END		

PIPE SCHEDULE

PIPE SCHEDULE	
4-5	150'-56" HOPE @ 0.15%
10-12	150'-56" HOPE @ 0.15%
14-1	150'-56" HOPE @ 0.15%
15-1	150'-56" HOPE @ 0.15%
16-1	150'-56" HOPE @ 0.15%
17-1	150'-56" HOPE @ 0.15%
18-1	150'-56" HOPE @ 0.15%
19-1	150'-56" HOPE @ 0.15%
20-1	150'-56" HOPE @ 0.15%
21-1	150'-56" HOPE @ 0.15%
22-1	150'-56" HOPE @ 0.15%
23-1	150'-56" HOPE @ 0.15%
24-1	150'-56" HOPE @ 0.15%
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28-1	150'-56" HOPE @ 0.15%
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41-1	150'-56" HOPE @ 0.15%
42-1	150'-56" HOPE @ 0.15%
43-1	150'-56" HOPE @ 0.15%
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69-1	150'-56" HOPE @ 0.15%
70-1	150'-56" HOPE @ 0.15%
71-1	150'-56" HOPE @ 0.15%
72-1	150'-56" HOPE @ 0.15%
73-1	150'-56" HOPE @ 0.15%
74-1	150'-56" HOPE @ 0.15%
75-1	150'-56" HOPE @ 0.15%
76-1	150'-56" HOPE @ 0.15%
77-1	150'-56" HOPE @ 0.15%
78-1	150'-56" HOPE @ 0.15%
79-1	150'-56" HOPE @ 0.15%
80-1	150'-56" HOPE @ 0.15%
81-1	150'-56" HOPE @ 0.15%
82-1	150'-56" HOPE @ 0.15%
83-1	150'-56" HOPE @ 0.15%
84-1	150'-56" HOPE @ 0.15%
85-1	150'-56" HOPE @ 0.15%
86-1	150'-56" HOPE @ 0.15%
87-1	150'-56" HOPE @ 0.15%
88-1	150'-56" HOPE @ 0.15%
89-1	150'-56" HOPE @ 0.15%
90-1	150'-56" HOPE @ 0.15%
91-1	150'-56" HOPE @ 0.15%
92-1	150'-56" HOPE @ 0.15%
93-1	150'-56" HOPE @ 0.15%
94-1	150'-56" HOPE @ 0.15%
95-1	150'-56" HOPE @ 0.15%
96-1	150'-56" HOPE @ 0.15%
97-1	150'-56" HOPE @ 0.15%
98-1	150'-56" HOPE @ 0.15%
99-1	150'-56" HOPE @ 0.15%
100-1	150'-56" HOPE @ 0.15%

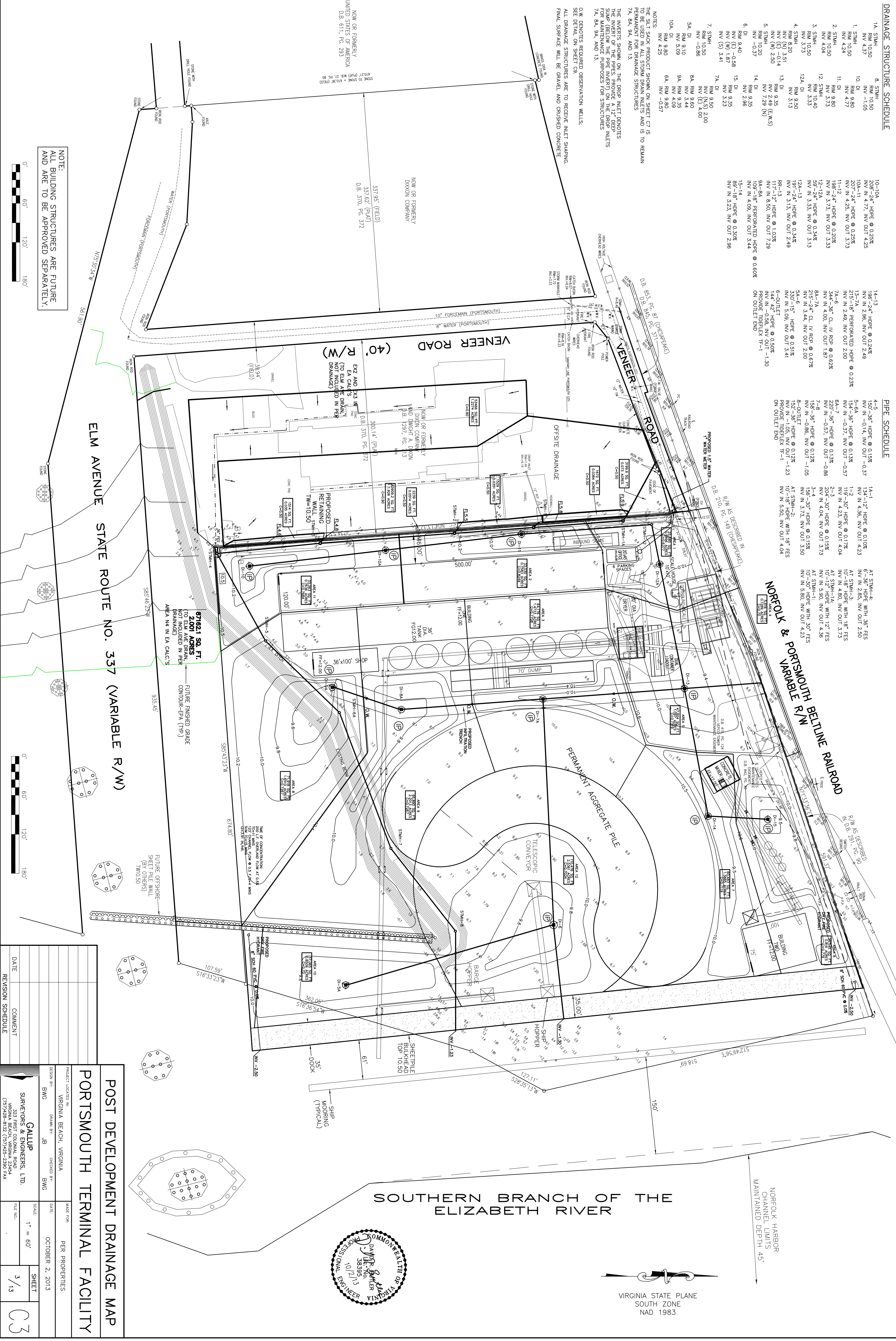
**NEW YORK & PORTSMOUTH BELL LINE RAILROAD**

AT SUMH-4:  
6-36 HOPE WITH 36<sup>00</sup> FES  
INV IN 2.85, INV OUT 2.50

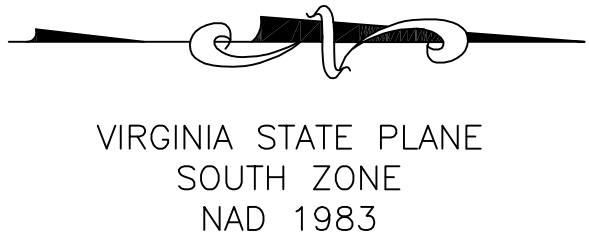
AT SUMH-3:  
10-12 HOPE WITH 18<sup>00</sup> FES  
INV IN 4.80, INV OUT 3.73

AT SUMH-1A:  
10-12 HOPE WITH 12<sup>00</sup> FES  
INV IN 5.50, INV OUT 4.36

AT SUMH-1:  
10-12 HOPE WITH 30<sup>00</sup> FES  
INV IN 5.80, INV OUT 4.23



SOUTHERN BRANCH OF THE  
ELIZABETH RIVER



VIRGINIA STATE PLANE  
SOUTH ZONE  
NAD 1983



## POST DEVELOPMENT DRAINAGE MAP

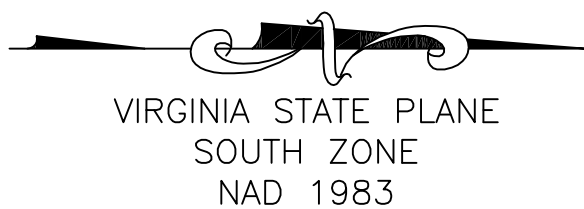
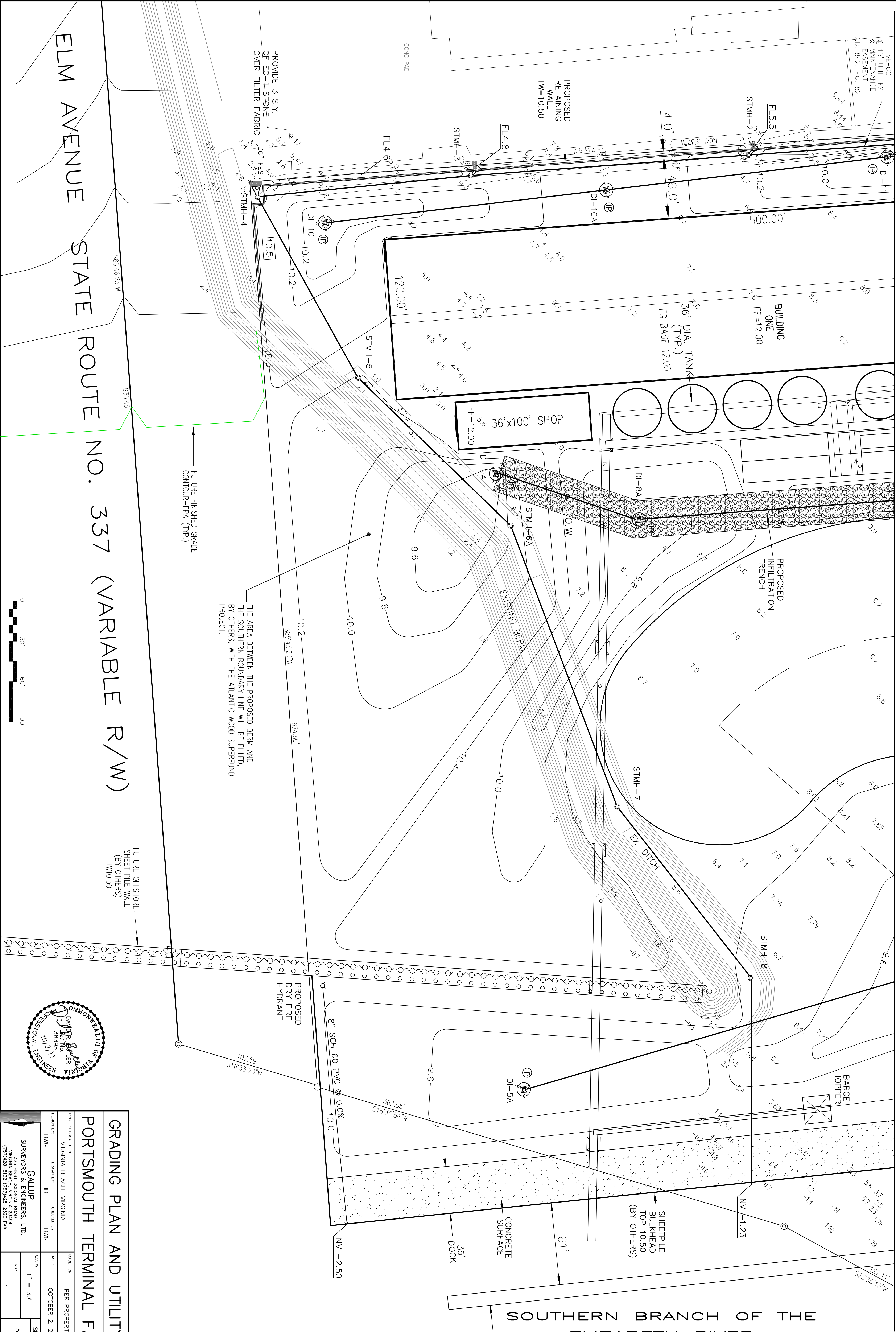
PORTSMOUTH TERMINAL FACILITY			
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG		DATE: OCTOBER 2, 2013	
DRAWN BY: JB		CHECKED BY: BWG	
SCALE: 1" = 60'		SHEET: 3 / 13	
SURVEYORS & ENGINEERS, LTD. 323 FIRST COASTAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 / (757)425-2350 FAX		03	
DATE	COMMENT		
REVISION SCHEDULE			







MATCH LINE SEE SHEET C4



SOUTHERN BRANCH OF THE  
ELIZABETH RIVER

## GRADING PLAN AND UTILITY PLAN

### PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATION: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BMC	DRAWN BY: JB	CHECKED BY: BMC	DATE: OCTOBER 2, 2013
SURVEYORS & ENGINEERS, LTD. VIRGINIA BEACH, VIRGINIA 23464 (757) 428-8132 (757) 425-2390 FAX		SCALE: 1" = 30'	SHEET 5 / 13



ELM AVENUE  
STATE ROUTE NO. 337 (VARIABLE R/W)



A cross-sectional diagram of a roof assembly. It shows a sloped roof section with a vertical wall on the left and a horizontal section on the right. A triangular expansion restraint is installed at the junction of the sloped and horizontal sections. The restraint is labeled "Expansion Restraint" with a line pointing to it. The restraint consists of a central triangular core and two side flaps that extend to the roof surface.

3. THE YELLOW RESTRAINT CORD SHOULD BE VISIBLE AT ALL TIMES. IF THE CORD IS COVERED WITH SEDIMENT, THE SILTSACK SHOULD BE EMPLIED.

### 3.0 Construction Sequence

#### 3.1 General

- 3.1.1** To install Siftsack in the catch basin, remove the grate and place the sack in the opening. Hold approximately six inches of the sack outside the frame. This is the area of the lifting straps. Replace the grate to hold the sack in place.

**3.1.2** When the restraint cord is no longer visible, Silbsack is full and should be emptied.

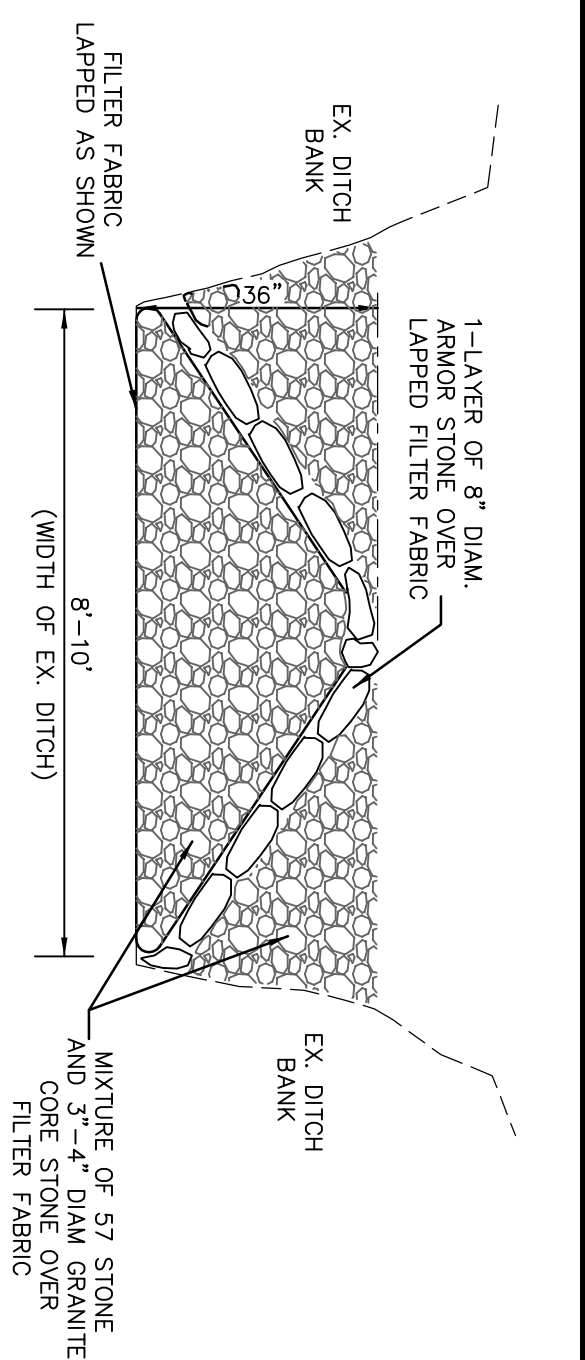
**3.1.3** To remove Sitsack, take two pieces of 1" diameter rebar and place through the lifting loops on each side of the sack to facilitate the lifting of Sitsack.

**3.1.4** To empty Silt sack, place unit where the contents will be collected. Place the rear through the lift straps (connected to the bottom of the sack) and lift. This will lift Silt sack from the bottom and empty the contents. Clean out and rinse. Return Silt sack to its original shape and place back in the basin.

**3.1.5** Silt sack is reusable. Once the construction cycle is complete, remove Silt sack from the basin and clean. Silt sack should be stored out of sunlight until next use.

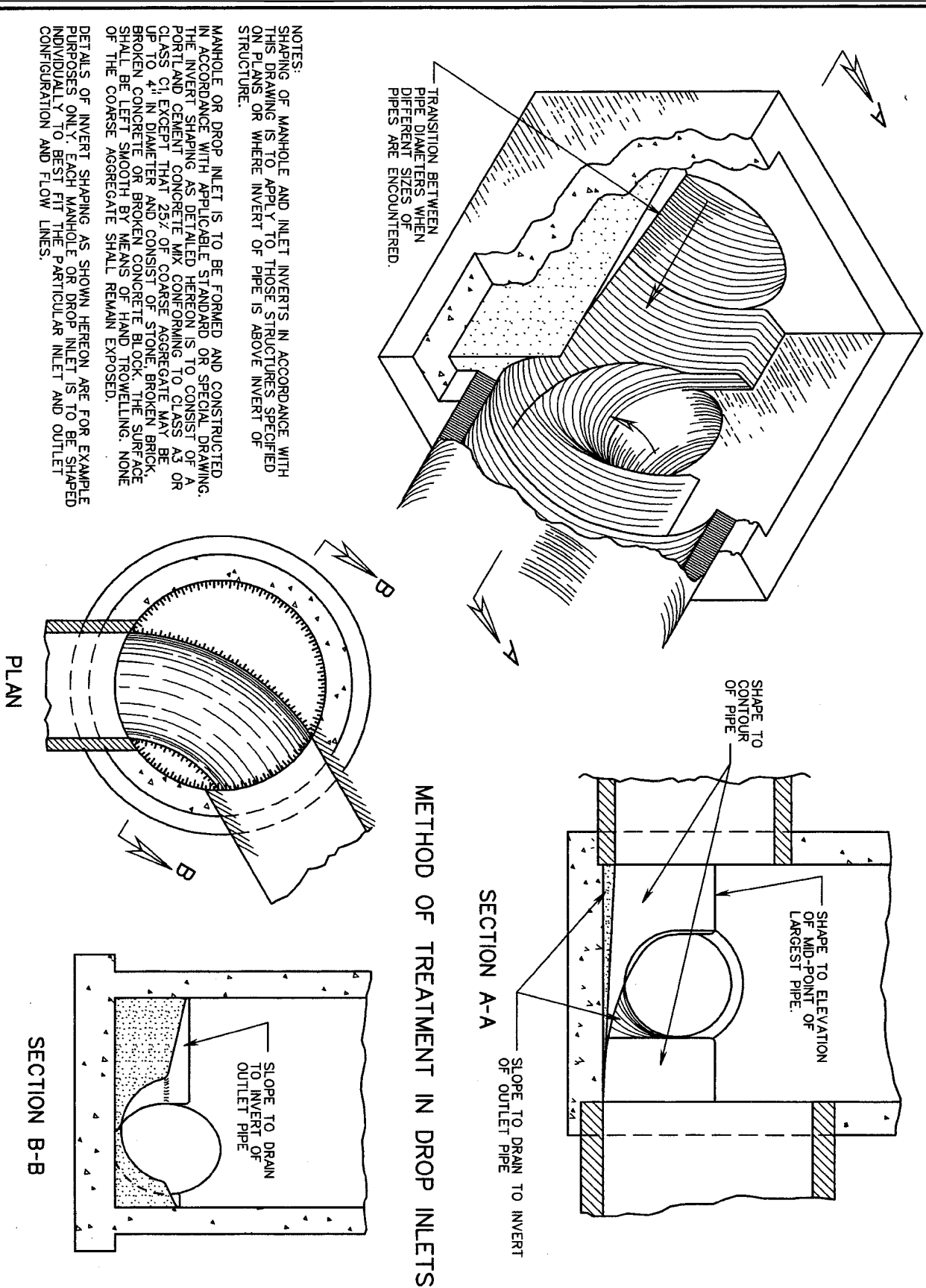
## SILTSACK DETAIL

THE SILT SACK PRODUCT SHOWN ON THIS SHEET TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN PERMANENT FOR DRAINAGE STRUCTURES 12-22



## DETAIL

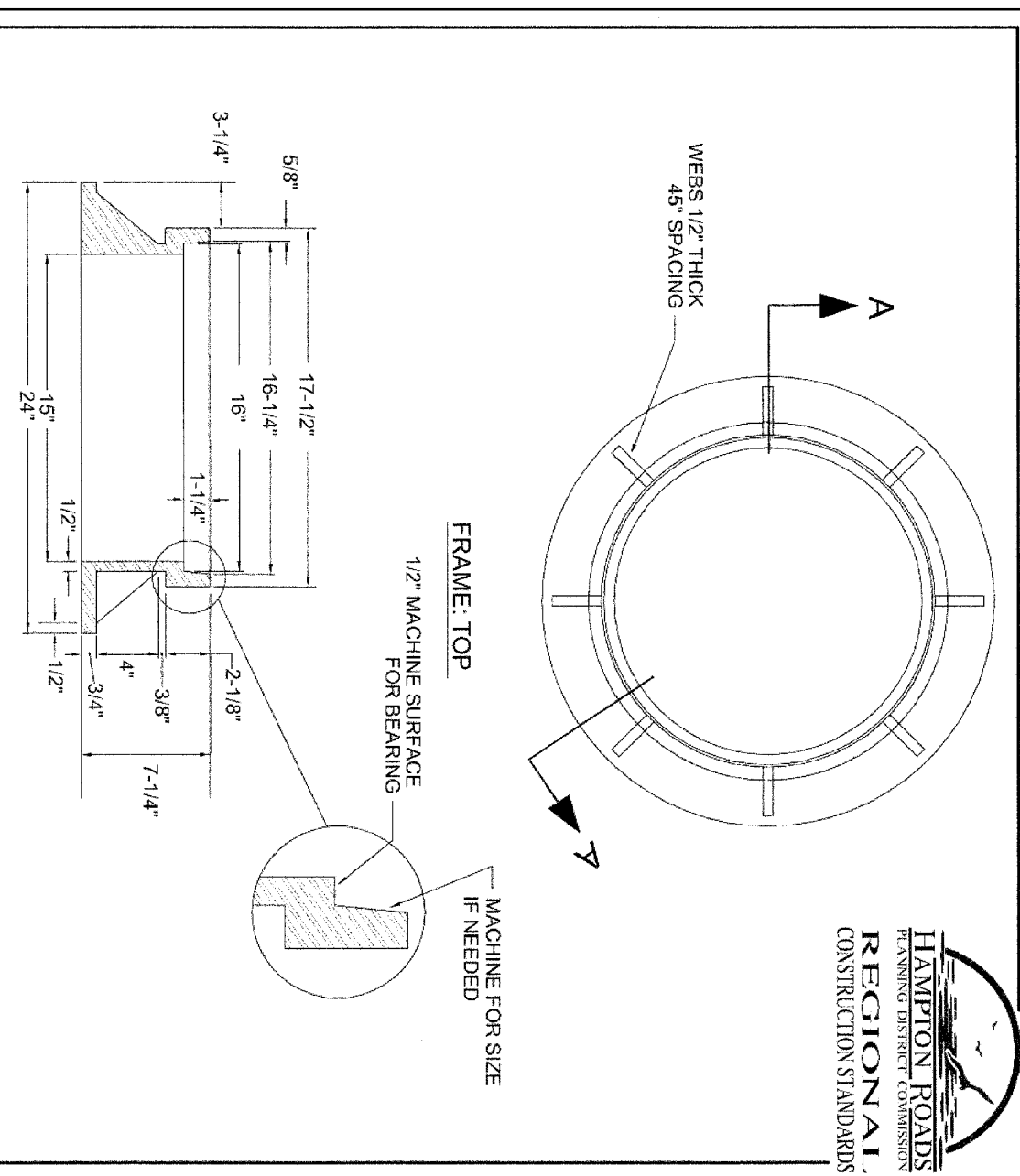
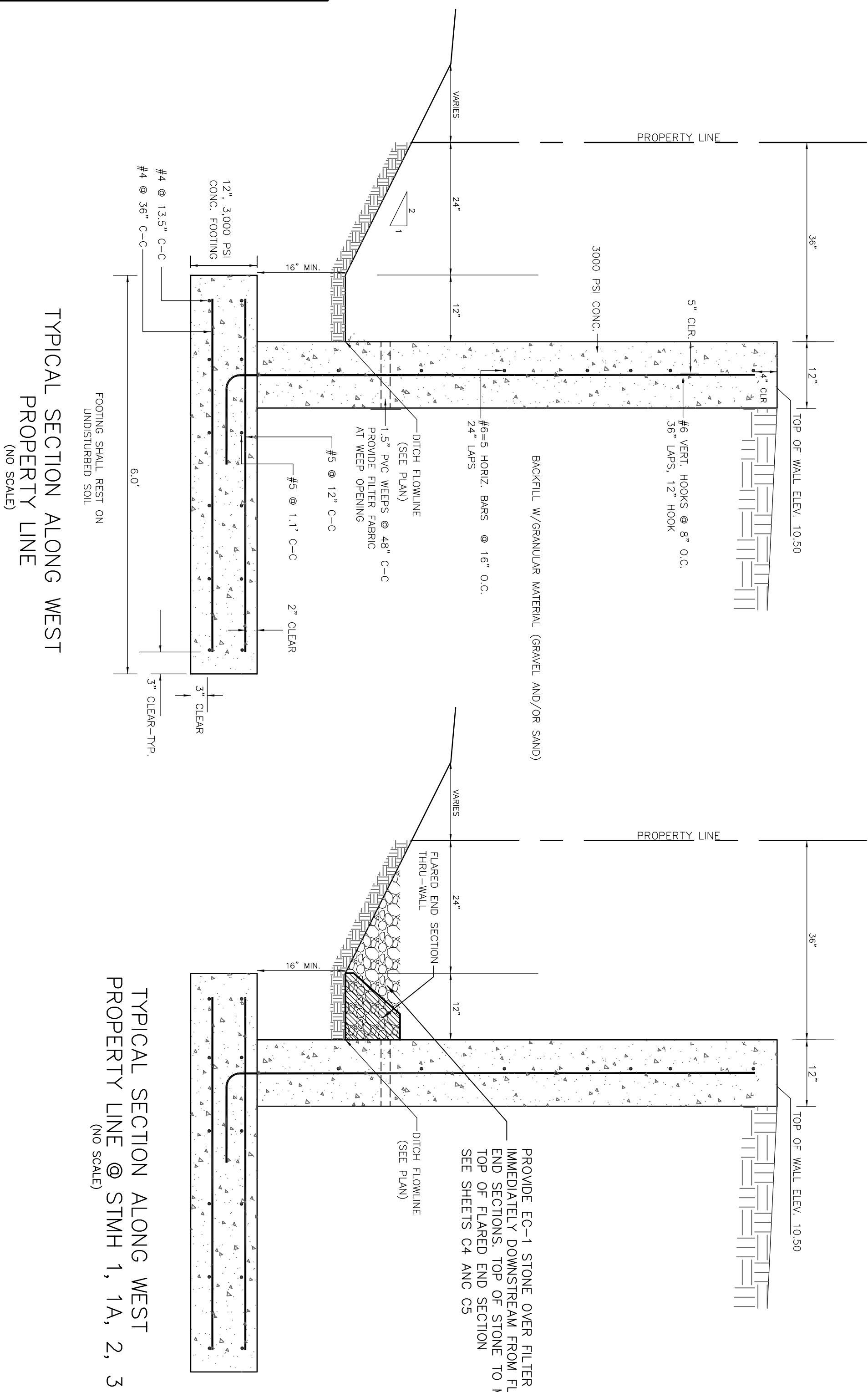
CHECK DAM AT SW CORNER  
OF BOUNDARY  
(NO SCALE)



## STANDARD METHOD OF SHAPING MANHOLE & INLET INVERTS

ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET  
SHAPING WITH THE EXCEPTION OF STRUCTURES 12-22

<b>VDOT</b> ROAD AND BRIDGE STANDARDS SHEET 1 OF 1 REVISION DATE 06/08	<b>STANDARD METHOD OF SHAPING MANHOLE &amp; INLET INVERTS</b>  VIRGINIA DEPARTMENT OF TRANSPORTATION		SPECIFICATION REFERENCE
			302



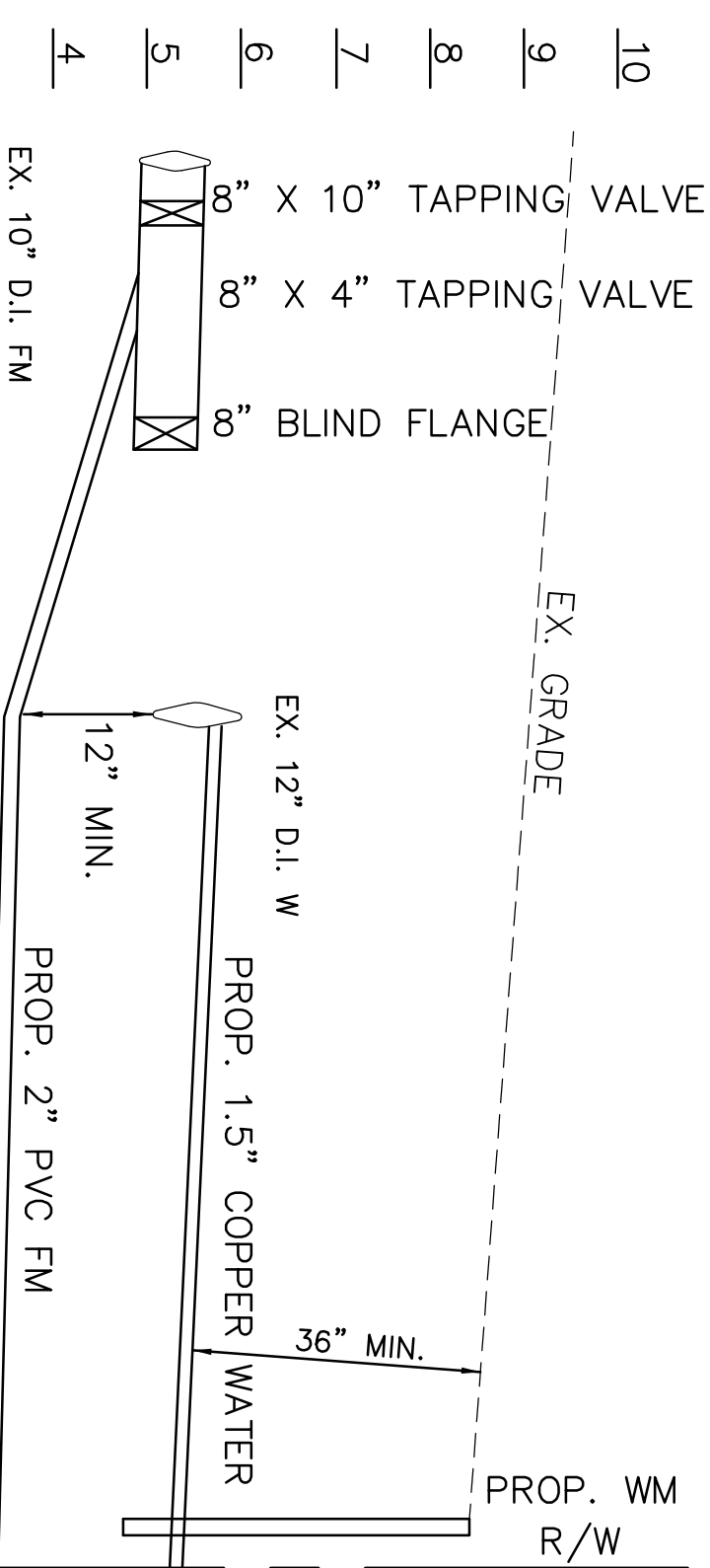
NOTES:

1. VAUVE BONE FIBRE AND COVER TO BE SUPPLIED BY CAPITAL FOUNDRY OF VIRGINIA, INC. MODEL #FBN-191, 180 LBS., OR APPROVED EQUAL.
2. ALL GRAV RICK CASTINGS SHALL CONFORM TO LATEST EDITION OF ASTM A-48, CLASS 30 AND SHALL BE OF UNIFORM QUALITY.
3. ALL CASTING DIMENSIONS SHALL HAVE A TOL. RANGE OF .1875"
4. ALL CASTINGS SHALL BE CLEANED BY SHOT BLASTING AND HAND CHIPPING UTILIZING STANDARD INDUSTRY PRACTICES PRIOR TO SHOP APPLICATION OF ASPHALTIC COATING BY DIPPING.

## STANDARD VALVE BOX FRAME AND COVER

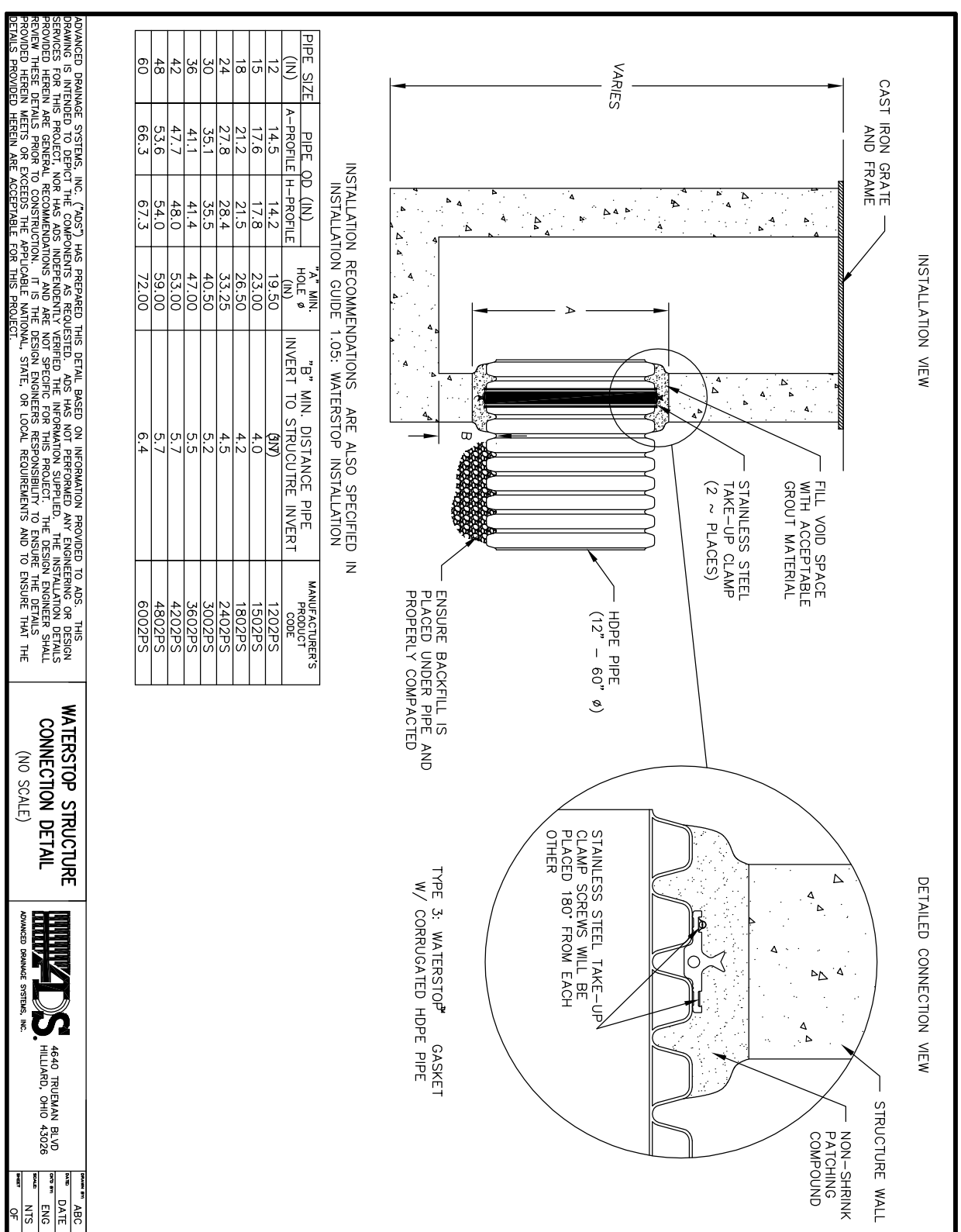
NOT TO SCALE

200.801.803	WATER & SANITARY	DATE 12/10	SHEET NO. 2 OF 2	DRAWING NO. WS_01
-------------	------------------	---------------	---------------------	----------------------



PROFILE:  
FM AND WATER SERVICE CONNECTION

SCALE: 1" = 2' HORIZ  
1" = 2' VERT.



PIPE SIZE (IN.)	CO. (IN.)	HOLE "X" INVERT TO SPOOLING INVERT	"T" RUN DISTANCE FROM SPOOLING INVERT	NUMBER OF PILES PRODUCED
12	14.5	14.42	19.50	120295
15	17.6	17.8	23.00	160925
18	21.2	21.5	26.50	180295
24	27.8	28.4	33.25	240295
30	35.1	35.5	40.50	300295
36	42.1	42.5	47.50	360295
42	47.7	48.0	53.00	420295
48	53.6	54.0	59.00	480295
60	66.3	67.3	72.00	600295

<p>CONTRACT DRAWING SYSTEM, INC. ("CDS") HAS PREPARED THIS DETAIL, BASED ON INFORMATION PROVIDED BY AGS. THIS INFORMATION WAS OBTAINED FROM AGS' RECORDS AND IS NOT VERIFIED BY CDS. CDS DOES NOT WARRANT THE ACCURACY OR COMPLETENESS OF THE INFORMATION PROVIDED, NOR DOES IT WARRANT THAT THE INFORMATION IS SUITABLE FOR ANY PARTICULAR PURPOSE. CDS ASSUMES NO LIABILITY FOR ANY ERRORS OR OMISSIONS IN THIS DETAIL. THE USER OF THIS DETAIL ASSUMES ALL LIABILITY FOR ANY ERRORS OR OMISSIONS IN THIS DETAIL. THE USER OF THIS DETAIL ASSUMES ALL LIABILITY FOR ANY ERRORS OR OMISSIONS IN THIS DETAIL.</p>	<p>WATERSTOP STRUCTURE CONNECTION DETAIL (NO SCALE)</p>		<p>CONTRACT DRAWING SYSTEM, INC. 440 TRIUMPH BLVD CINCINNATI, OHIO 45206 TEL: 513-763-1111 FAX: 513-763-1112 WWW.CDS-INC.COM</p>	DATE	BY	CHKD	APP'D
				DATE	BY	CHKD	APP'D

## DETAILS AND NOTES

### PORTSMOUTH TERMINAL FACILITY

[illegible]



DRAINAGE STRUCTURE SCHEDULE

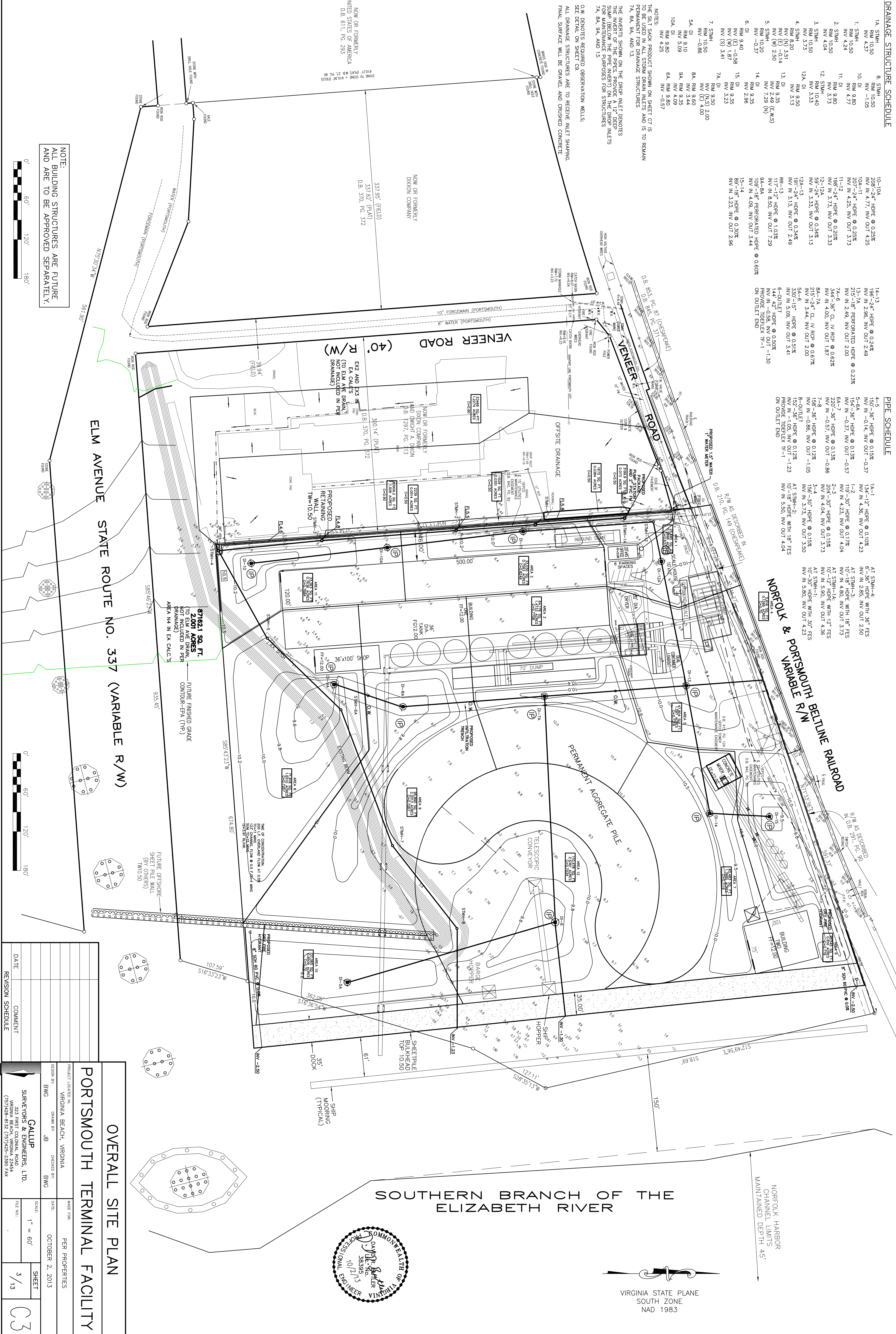
1A. STMH RM 10.50 INV -1.05	8. STMH RM 10.50 INV -1.05	10-10A 208'-24" HOPE @ 0.25% INV IN 4.77, INV OUT 4.25	14-13 196'-24" HOPE @ 0.24% INV IN 2.96, INV OUT 2.49
1. STMH RM 10.50 INV 4.77	10. RM 9.80 INV 4.77	13-7A 207'-24" HOPE @ 0.25% INV IN 4.25, INV OUT 3.73	13-7A 207'-24" HOPE @ 0.23% INV IN 2.49, INV OUT 2.00
2. STMH RM 9.80 INV 4.04	11. DI RM 9.80 INV 4.04	11-12 198'-24" HOPE @ 0.20% INV IN 3.73, INV OUT 3.53	7A-6 344'-36" CL. IV RCP @ 0.62% INV IN 4.00, INV OUT 1.87
3. STMH RM 10.50 INV 3.73	12. RM 10.40 INV 3.73	58'-24" HOPE @ 0.34% INV IN 3.33, INV OUT 3.13	8A-7A 215'-24" CL. IV RCP @ 0.57% INV IN 3.13, INV OUT 2.49
4. STMH RM 9.50 INV 3.51	12A. DI RM 9.50 INV 3.51	12A-13 191'-24" HOPE @ 0.34% INV IN 3.13, INV OUT 2.49	32A-15 345'-15" HOPE @ 0.51% INV IN 5.09, INV OUT 3.41
5. STMH RM 10.37 INV -0.37	13. DI RM 9.35 INV (E) -0.14	RR-13 117'-12" HOPE @ 1.03% INV IN 6.50, INV OUT 7.29	6-OUTLET 144' 42" HOPE @ 0.50% INV IN -0.58, INV OUT -1.30
6. DI RM 9.40 INV (E) -0.58	14. DI RM 9.36 INV (S) 3.41	109'-18" PERFORATED HOPE @ 0.60% INV IN 4.09, INV OUT 3.44	ON OUTLET END
7. STMH RM 10.50 INV -0.86	7A. DI RM 9.50 INV (NS) 2.00	15-14 89'-18" HOPE @ 0.30% INV IN 3.23, INV OUT 2.96	
5A. DI RM 9.10 INV 5.09	8A. RM 6.64 INV (E) 4.00		
10A. DI RM 9.80 INV -0.57	9A. RM 9.35 INV 4.09		
	6A. RM 9.80 INV -0.57		

NOTES:  
 THE SET BACK PRODUCT SHOWN ON SHEET C7 IS TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN PERMANENT FOR DRAINAGE STRUCTURES  
 7A, 8A, 9A, AND 13.  
 THE INVERTS SHOWN ON THE DROP INLET DENOTES SLUMP (BELOW THE PIPE INVERT) ON THE DROP INLETS OR THE INVERTS FOR PURPOSES FOR STRUCTURES 7A, 8A, 9A, AND 13.  
 O.W. DENOTES REQUIRED OBSERVATION WELLS.  
 SEE DETAIL ON SHEET C9.  
 ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET SHAPING.  
 FINAL SURFACE WILL BE GRAVEL AND CRUSHED CONCRETE.

PIPE SCHEDULE

4-5 150'-36" HOPE @ 0.15% INV IN -0.14, INV OUT -0.37	1A-1 134'-12" HOPE @ 0.10% INV IN 4.35, INV OUT 4.23	AT STMH-4 136'-36" WITH 36" FEES INV IN 5.09, INV OUT 2.50
5-6A 197'-36" HOPE @ 0.13% INV IN -0.37, INV OUT -0.57	1A-2 119'-30" HOPE @ 0.17% INV IN 4.23, INV OUT 3.73	AT STMH-3 10'-18" HOPE WITH 18" FEES INV IN 4.80, INV OUT 3.73
6A-7 220'-36" HOPE @ 0.13% INV IN -0.57, INV OUT -0.86	2-3 204'-30" HOPE @ 0.15% INV IN 4.04, INV OUT 3.73	AT STMH-1A 10'-12" HOPE WITH 12" FEES INV IN 5.80, INV OUT 4.35
7-8 158'-36" HOPE @ 0.17% INV IN -0.86, INV OUT -1.05	158'-30" HOPE @ 0.15% INV IN 3.73, INV OUT 3.50	AT STMH-2 10'-30" HOPE WITH 30" FEES INV IN 5.80, INV OUT 4.23
8-OUTLET 152'-36" HOPE @ 0.12% INV IN -1.05, INV OUT -1.23	AT STMH-2 10'-18" HOPE WITH 18" FEES INV IN 5.50, INV OUT 4.04	
144' 42" HOPE @ 0.50% INV IN -0.58, INV OUT -1.30	ON OUTLET END	

NORFOLK & PORTSMOUTH BELTLINE RAILROAD  
 0.8% R/W 169' (OFFSHELF)  
 0.8% R/W 169' (OFFSHELF)  
 0.8% R/W 169' (OFFSHELF)  
 0.8% R/W 169' (OFFSHELF)



SOUTHERN BRANCH OF THE ELIZABETH RIVER

VIRGINIA STATE PLANE  
 SOUTH ZONE  
 NAD 1983

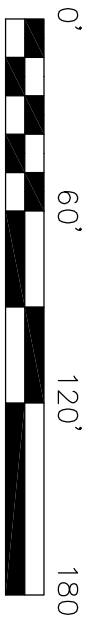
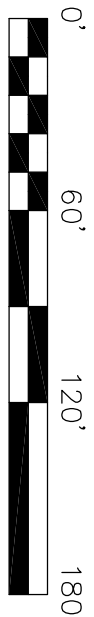


OVERALL SITE PLAN

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATION: VIRGINIA BEACH, VIRGINIA	DRAWN BY: BNC	CHECKED BY: BNC	DATE: OCTOBER 2, 2013	SCALE: 1" = 60'	SHEET: 3 / 13
SURVEYORS & ENGINEERS, LTD.					
323 FIRST CONCRETE ROAD VIRGINIA BEACH, VIRGINIA 23464 (757) 428-8137 (757) 428-2390 FAX					
DATE: REVISION SCHEDULE					

NOTE:  
 ALL BUILDING STRUCTURES ARE FUTURE  
 AND ARE TO BE APPROVED SEPARATELY.





AREA SUMMARY:

C FACTOR FOR ROOF AND CONCRETE=0.90  
C FACTOR FOR GRAVEL=0.70  
C FACTOR FOR GRASS=0.30

DRAINAGE CALCULATIONS  
FOR PER, LOCATED IN  
CITY OF PORTSMOUTH  
REVISED AUGUST 2013

AREA 1:

A TOTAL=25,685 SQ. FT. = 0.5896 AC.  
3588 S.F.=0.0823 AC. X 0.9 = CA=0.0741  
5794 S.F. = 0.1330 AC. X 0.3 = CA=.0399  
16303 S.F.=0.3743 AC X 0.70 = CA=0.2691  
SUM CA'S=0.3760, C=0.6377

AREA 2:

A TOTAL=33030 S.F.=0.7583 AC.  
20626 S.F.=0.4735 AC X 0.90=0.4262  
12404 S.F.=0.2848 A. X 0.70=0.1993  
SUM CA=0.6255, C=0.8249

AREA 3:

64176 S.F.=1.4733 AC.  
22740 S.F.=0.5220 AC. X 0.9=0.4688  
41436 S.F.=0.9512 AC. X 0.7=0.6659  
SUM CA=1.1357, C=0.7708

AREA 4 TO STUB:

5616 S.F. = 0.1289 X 0.70=0.0902

AREA 5:

A TOTAL = 47804 S.F. = 1.0974 AC.  
7635 S.F.=0.1753 AC. X 0.9=0.1577  
40,169 S.F. = 0.9222 AC. X 0.7=0.6455  
SUM CA=0.8032, C=0.7319

AREA 6:

AREA TOTAL=35,545 S.F.=0.816 AC.  
14029 S.F. = 0.3221 AC. X 0.9=0.2899  
21516 S.F.=0.494 AC. X 0.7=0.3457  
SUM CA=0.6357, C=0.779

AREA 7:

AREA TOTAL=60,483 S.F.=1.3885 AC.  
3604 S.F. = 0.0827 X 0.9=.0745  
56,879 S.F.=1.3058 AC. X 0.7=0.914  
SUM CA=0.9885, C=0.7119

AREA 8:

AREA TOTAL=71818 S.F.=1.6510 AC.  
9608 S.F.=0.2206 AC. X 0.90=0.1985  
62310 S.F.=1.4304 AC. X 0.7=1.0013  
SUM CA=1.1998, C=0.7267

AREA 9:

AREA TOTAL=95,890 S.F.=2.2013 AC.  
14484 S.F.=0.3325 AC. X 0.9=0.2993  
81406 S.F.=1.8688 AC. X 0.7=1.3082  
SUM CA=1.6075, C=0.73

AREA 10:

37065 S.F.=0.8509 AC.  
C=0.7, CA=0.5956

AREA 11:

AREA TOTAL=33263 S.F.=0.7636 AC.  
11374 S.F.=0.2611 AC. X 0.9=0.235  
21889 S.F.=0.5025 AC. X 0.7=0.3518  
SUM CA=0.5867, C=0.7684

AREA 12:

AREA TOTAL=110476 S.F.=2.5361 AC.  
1903 S.F.=0.0436 X 0.9=0.0393  
108573 S.F.=2.4924 AC. X 0.7=1.7447  
SUM CA=1.7841, C=0.7034

OFFSITE AREAS FROM DIXON TRACT:

TO STMH-1A

AREA TOTAL=3199 S.F.=0.0735 AC.  
3199 S.F.=0.0735 AC. X 0.5=0.0368

TO STMH-1

AREA TOTAL=85581 S.F.=1.9646 AC.  
1672 S.F.=0.0384 AC. X 0.5=0.0192  
83909 S.F. = 1.9262 AC. X 0.90=1.7337  
SUM CA=1.7529, C=0.8922

TO STMH-2

AREA TOTAL=1529 S.F.=0.0351 AC. X 0.5=.0175

TO STMH-3

AREA TOTAL=2239 S.F.=0.0514 AC. X 0.5=.0257

TO STMH-4

AREA TOTAL=53466 S.F.=1.2274 AC. X 0.9=1.1047

C FACTORS FOR THE DIXON TRACT ASSUME  
ULTIMATE DEVELOPMENT:

SUM OF THE OFFSITE AREAS=146,014 S.F. = 3.352 AC.  
SUM OF THE OFFSITE CA's=2.93755  
ULTIMATE C FACTOR = 2.9376/3.3520 = 0.88

OFFSITE STORM SEWER IS DESIGNED WITH THE  
DIXON TRACT BEING ULTIMATELY DEVELOPED,  
NOT THE CURRENT STATE (CONSERVATIVE)

NOTES:

ONSITE AND OFFSITE DRAINAGE DESIGNED FOR  
THE 100 YEAR STORM. BOTH SYSTEMS ARE  
INDEPENDENT AND SEPARATE. WATER QUALITY  
STORAGE CALCULATIONS WERE PERFORMED BASED  
ON ONE INCH OF RUNOFF OVER THE IMPERVIOUS  
AREAS WITHIN THE REQUIRED DRAINAGE AREA.  
PEAK RUNOFF WILL BE REDUCED SOMEWHAT  
BECAUSE OF INFILTRATION WITH THE BMP TRENCH,  
BUT WAS NOT CONSIDERED IN THE STORM DRAIN  
DESIGN.



## WATER QUALITY CALCULATIONS FOR INFILTRATION TRENCH

AREA 8:  
TOTAL AREA=1.651 AC.  
ROOF A=0.2206 AC.  
GRAVEL AREA=1.4304 AC, 70% IMPERVIOUS=1.0013 AC.  
SUM=1.2219 AC.

AREA 9:  
TOTAL AREA=2.2013 AC.  
ROOF A=0.3325 AC.  
GRAVEL AREA =1.8688 AC., 70% IMPERVIOUS = 1.3082 AC.  
SUM=1.6407 AC.

AREA 3:  
TOTAL AREA=1.4733 AC.  
ROOF A=0.522 AC.  
GRAVEL AREA=0.9512 AC.. 70% IMPERVIOUS=0.6659 AC.  
SUM=1.1879 AC.

AREA 11:  
TOTAL AREA=0.7636 AC.  
ROOF A=0.2611 AC.  
GRAVEL AREA=0.5025 AC, 70% IMPERVIOUS=0.3518  
SUM=0.6129 AC.

AREA 2:  
TOTAL AREA=0.7583 AC.  
ROOF A=0.4735 AC.  
GRAVEL A=0.2847 AC, 70% IMPERVIOUS = 0.1993 AC.  
SUM=0.6728 AC.

AREA 5:  
TOTAL A=1.0974 AC.  
ROOF A=0.1753 AC.  
GRAVEL A=0.9222 AC., 70% IMPERVIOUS = 0.6455 AC.  
SUM=0.8208

AREA 1:  
TOTAL AREA=0.5896 AC.  
ROOF A=0.0823 AC.  
GRAVEL A=0.3743 AC, 70% IMPERVIOUS=0.2619 AC.  
SUM=0.3442 AC.

SUM OF THE AREAS=8.5344 AC.  
SUM OF THE IMPERVIOUS AREAS=6.5012 AC.  
I% = 6.5012 AC./8.5344 AC. = 76.2%

REQUIRED VOLUME IS 1" X WATER QUALITY VOLUME:  
 $(0.5"/12)(6.5012 \text{ AC.}) (43,560 \text{ S.F./AC.}) = 11,799 \text{ CUBIC FEET}$

TRENCH INSTALLED BETWEEN 13 AND 9A:  
LENGTH=544 L.F.  
DEPTH OF 57 STONE=4'  
WIDTH OF TRENCH=13.67'  
VOID VOLUME IS 40% OF TOATL VOLUME  
VOLUME PROVIDED IN VOIDS=(544')(4')(13.67')(0.4) = 11,898 C.F. > 11,799 C.F.

BMP AREA FOR TABLE ON COVER SHEET:  
838.8' X 4' DEEP X 2 SIDES = 4,310 S.F.  
27.3' WIDE X 4' DEEP X 2 SIDES = 55 S.F.  
1,143 S.F. BOTTOM AREA  
TOTAL=5,508 S.F.



FROM BMP CLEARINGHOUSE:

INFILTRATION PRACTICE NUMBER 8, TOTAL MASS LOAD REMOVAL OF TOTAL PHOSPHORUS = 50%

APPLICABLE AREA=14.87 ACRES

1 WATERSHED FOR PORTSMOUTH=54%

EXISTING IMPERVIOUS AREA=1.15 ACRES

USE SITUATION 2, PERFORMANCE BASED WATER QUALITY CALCULATIONS

1 EX.< 1 WATERSHED

1 POST> 1 WATERSHED

$L_{PRE} (WS) = (0.05 + (0.009 \times 54)) \times 14.87 \text{ AC.} \times 2.28 = 18.2 \text{ LBS/YEAR}$

$L_{POST} = (0.05 + (0.009 \times 76.6)) \times 14.87 \times 2.28 = 25.06 \text{ LBS/YR.}$

$RR = L_{POST} - L_{PRE}$

$RR = 25.06 - 18.2 = 6.9 \text{ LBS/YR.}$

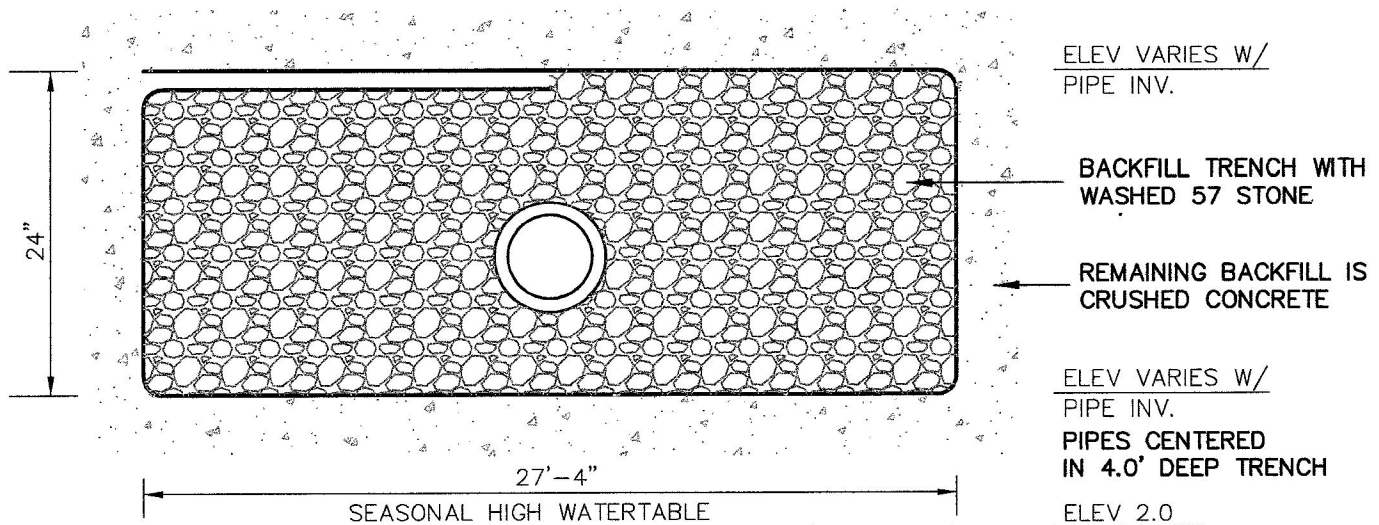
USING INFILTRATION,

$L_{BMP} = (0.05 + (0.009 \times 76.2)) \times 8.5344 \times 2.28 = 14.31 \text{ LBS/YR.}$

$L_{REMOVED \text{ BY BMP}} = 0.50 \times 14.31 = 7.15 \text{ LBS/YR}$

$7.2 \text{ LBS/YR} > 6.9 \text{ LBS/YR}$

WATER QUALITY IS SATISFIED.



TRENCH LENGTH=544 L.F.

INFILTRATION RATE (I)=0.0000713 F/S

VOLUME=L x W x D x 0.4

VOID VOLUME = 40% OF TRENCH VOLUME

Q OUT=I x TOTAL TRENCH AREA

VOID RATIO OF 57 STONE: 0.40

VOID VOLUME OF CRUSHED CONCRETE: 0.30-0.40

TRENCH INSTALLED BETWEEN 13 AND 9A:

LENGTH=544 L.F.

DEPTH OF 57 STONE=2'

WIDTH OF TRENCH=27.34'

VOID VOLUME IS 40% OF TOTAL VOLUME

VOLUME PROVIDED IN VOIDS=(544')(2')(27.34')(0.4) = 11,898 C.F. > 11,799 C.F.

TRENCH AREA: (2' x 544' x 2 SIDES) + (27.34' x 544' x 2) = 31,922 S.F.

0.0000713 F/S x 31,922 S.F. = 2.28 CFS

Q IS REDUCED BY 1.37 CFS

2 YEAR STORM VOLUME FROM HYDROGRAPH=40,561 C.F.

Q OUT=0.0000713 C.F/S PER S.F. x 31,922 S.F. = 2.276 CF/SEC

40,561 C.F./2.276 CFS = 17,821 SEC x 1 MIN/60S x 1 HR./60 MIN x 1 DAY/24 HOURS = 0.21 DAYS

2 YEAR STORM WILL EXFILTRATE IN 0.21 DAYS



### INLET CAPACITY CALCULATIONS

CALCULATIONS PERFORMED USING VDOT GRATE INLET CAPACITY CHART

WIDTH OF STANDARD DROP INLET = 2.17, LENGTH = 2.17'

EQUATION FOR CHART NOMOGRAPH:  $P=2(W+L)$ ;

FOR SINGLE INLET,  $P=2(2.17'+2.17')=8.68$

DI-10

Q100=5.63 CFS

DEPTH AT INLET=0.38'

ELEVATION AT INLET=RIM ELEVATION + DEPTH =  $9.80+0.38'=10.18' < 10.5$

STORM IS CONTAINED

DI-11

Q=0.7583 X 0.8249

TC=5 MINS.

I100 = 9.60 IN/HR

Q100=6.01 CFS

DEPTH=0.39'

ELEV.=0.39'+9.80=10.19 < 100.50

DI-12

TC=10 MINS

I100=8.21

Q100 =  $0.5896 \times 0.6377 \times 8.21 = 3.1$  CFS

DEPTH AT INLET=0.24'

ELEVATION =  $0.24'+9.50=9.74' < 10.5$

DI-13

T=10 MINS

I100=8.21

Q100= $1.0974 \times 0.7319 \times 8.21 = 6.6$  CFS

DEPTH AT INLET = 0.41'

ELEVATION =  $0.41'+9.35=9.76 < 10.5$

DI-14

TC=5 MINS

I100=9.60

Q100= $1.3885 \times 0.7119 \times 9.60 = 9.5$  CFS

DEPTH AT INLET = 0.52'

ELEVATION =  $0.52'+9.35 = 9.87' < 10.5$

DI-15

TC=5 MINS

I100=9.60

Q100= $0.816 \times 0.779 \times 9.60 = 6.1$  CFS

DEPTH AT INLET=0.39'

ELEVATION= $0.39'+9.35 = 9.74 < 10.5$

DI-8A

TC=15.32 MIN

I100=7.13

Q100= $2.2013 \times 0.73 \times 7.13 = 11.5$  CFS

DEPTH AT INLET=0.59'

ELEVATION= $0.59'+9.60 = 10.19' < 10.5$

DI-7A

TC=5 MINS

I100=9.60

Q100= $1.4733 \times 0.7708 \times 9.60 = 10.9$  CFS

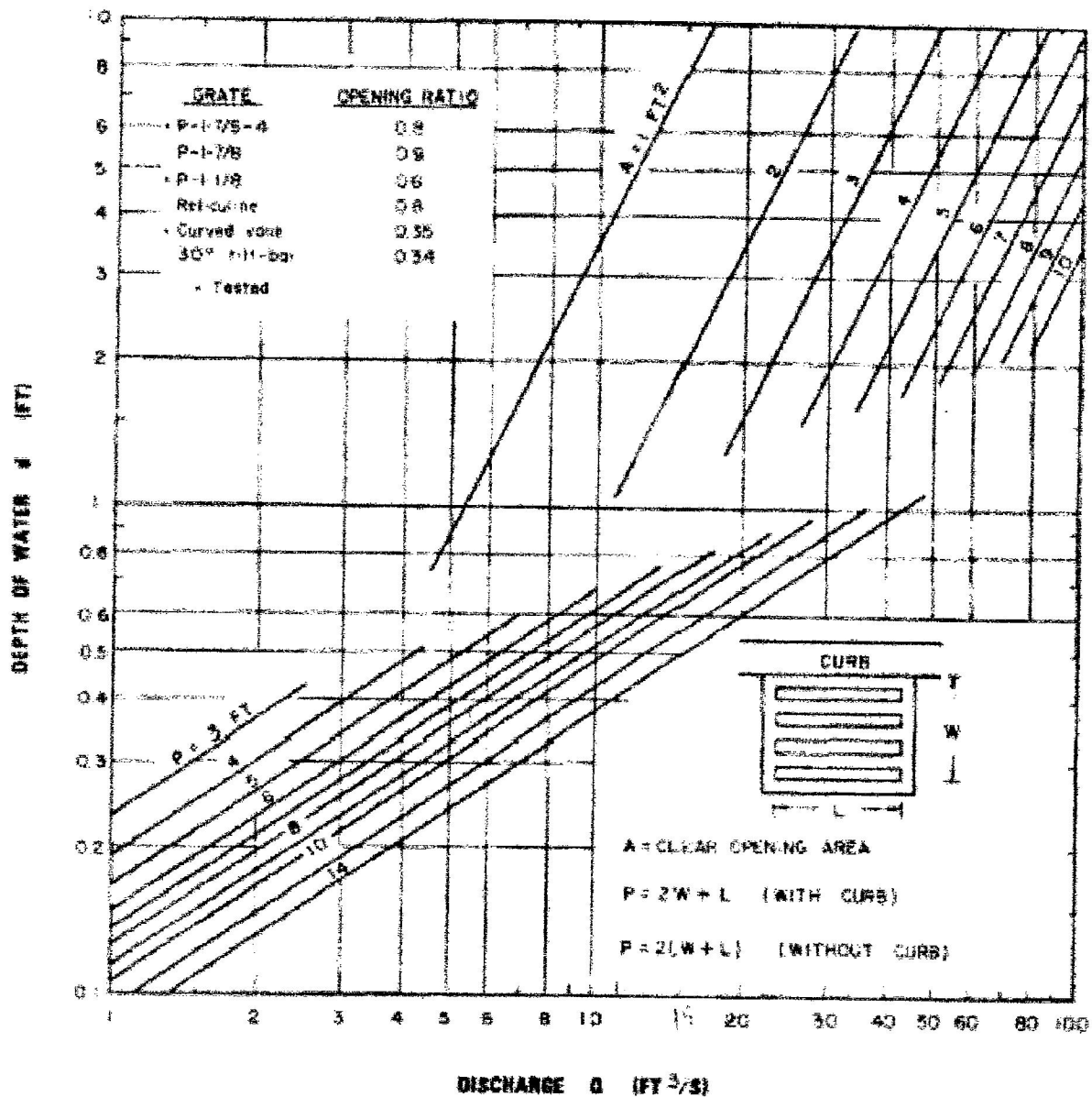
DEPTH AT INLET = 0.57'

ELEVATION= $0.67'+9.50 = 10.17 < 10.5$



# endix 9C-12

## Grate Inlet Capacity in Sump Conditions



Grate Inlet Capacity in Sump Conditions - English Units



FOR HGL CALC'S, THE STARTING HW ELEV.  
USED IS MHW (NAV. 88), ELEV=1.10  
AT EACH UPSTREAM INLET, BEGINING TW ELEV.  
IS EITHER LAST HGL ELEV, DEPTH IN PIPE  
CONVERTED TO ELEV, OR CRITICAL DEPTH  
CONVERTED TO ELEV. IN ALL CASES, THE LAST HGL  
ELEV IS THE CONTROL.

CHECK CONTROL FOR OFFSITE HGL CALC'S:

DEPTH IN PIPE AT NO. 8 USING 24.87 CFS,  $S=0.0012 = 2.44'$ , ELEV.  $= -1.05+2.44'=1.39$ , USE 1.42  
DEPTH IN PIPE AT NO. 7 USING 25.54 CFS,  $S=0.0013 = 2.41'$ , ELEV.  $= -0.86+2.41'=1.55$ , USE 1.74  
DEPTH IN PIPE AT NO. 6A USING 26.02 CFS,  $S=0.0013 = 2.47'$ , ELEV.  $= -0.57+2.47'=1.90$ , USE 2.17  
DEPTH IN PIPE AT NO. 5 USING 26.34 CFS,  $S=0.0036 = 1.69'$ , ELEV.  $= -0.37+1.69'=1.32$ , USE 2.51  
DEPTH IN PIPE AT NO. 4 USING 16.75 CFS,  $S=0.0015 = 1.99'$ , ELEV.  $= 3.51+1.99=5.50$ , USE 5.50  
DEPTH IN PIPE AT NO. 3 USING 16.98 CFS,  $S=0.0015 = 2.02'$ , ELEV.  $= 3.73+2.02=5.75$ , USE 5.83  
DEPTH IN PIPE AT NO. 2 USING 17.11 CFS,  $S=0.0016 = 1.97'$ , ELEV.  $= 4.04+1.97=6.01$ , USE 6.26  
DEPTH IN PIPE AT NO. 1 USING 0.35 CFS,  $S=0.0010 = 0.37'$ , ELEV.  $= 4.24+0.37=4.61$ , USE 6.52







## HYDRAULIC GRADE LINE

## OFFSITE

BEGIN TW Elev. MIN = 1.0

PROJECT: PER PROPERTIES

05/12/2013

## JUNCTION LOSS

INLET STATION	Outlet Water Surface Elev.	D <sub>o</sub>	Q <sub>o</sub>	L <sub>o</sub>	S <sub>f</sub> %	H <sub>f</sub>	V <sub>o</sub>	H <sub>o</sub>	Q <sub>i</sub>	V <sub>i</sub>	QV <sub>i</sub>	V <sub>i</sub> <sup>2</sup> 2g	H <sub>i</sub>	Angle	H <sub>A</sub>	H <sub>t</sub>	1.3 H <sub>t</sub>	0.5 H <sub>t</sub>	Final H	Inlet Water Surface Elev.	Rim Elev.
3	1.10	36"	24.40	152	.134	.203	4.04	.063	24.87	4.04	102.47	.0584	.089	53°	.021	.24	-	.12	.33	1.42	10.50
7	1.42	36"	24.87	153	.139	.219	4.20	.063	25.64	4.20	107.27	.274	.090	17°	.034	.193	-	.10	.52	1.74	10.50
6A	1.74	36"	25.54	220	.147	.3225	4.20	.0685	26.02	4.20	109.28	.274	.090	25°	.060	.225	-	.11	.43	2.17	10.50
5	2.17	36"	26.02	154	.152	.234	4.20	.068	26.34	4.60	113.53	.314	.1101	17.5°	.041	.219	-	.11	.34	2.51	10.50
4	2.51	36"	26.34	150	.150	.233	4.60	.079	16.75	3.99	66.38	.247	.089	90°	.173	.333	-	.17	.40	2.91	10.50 *
3	5.50	36"	16.75	150	.167	.26	3.99	.062	16.93	4.00	67.92	.248	.087	0°	-	.149	-	.074	.33	5.83	10.50/5.9
2	5.83	36"	16.93	204	.171	.349	4.00	.062	17.11	4.12	70.49	.264	.092	0°	-	.150	-	.08	.43	6.26	10.50/6.9
1	6.26	36"	17.11	126	.174	.219	4.12	.065	0.35	1.34	0.47	.028	.0098	0°	-	.076	-	.04	.26	6.52	10.50/6.9
1A	6.52	12"	0.35	129	.010	.012	1.34	.007	-	-	-	-	-	0°	-	.007	-	.02	.004	6.54	10.50/7.4

DEPT 6 e 8 using 24.87 cfs, S<sub>o</sub> = .0012 = 2.44' Elev. = -1.05 + 2.44 = 1.39DEPT 7 using 25.54 cfs, S<sub>o</sub> = .0013 = 2.41' Elev. = -0.86 + 2.41 = 1.55DEPT 6 using 26.02 cfs, S<sub>o</sub> = .0013 = 2.41' Elev. = -0.57 + 2.41 = 1.90DEPT 5 using 26.34 cfs, S<sub>o</sub> = .0030 = 1.69 Elev. = -0.37 + 1.64 = 1.32 (use 2.51)DEPT 4 using 16.75 cfs, S<sub>o</sub> = .0015 = 2.30' Elev. = 3.51 + 1.99 = 5.50DEPT 3 using 16.93 cfs, S<sub>o</sub> = .0015 = 2.30' Elev. = 3.51 + 1.99 = 5.50DEPT 2 using 17.11 cfs, S<sub>o</sub> = .0015 = 2.30' Elev. = 3.51 + 1.99 = 5.50DEPT 1 using 17.11 cfs, S<sub>o</sub> = .0015 = 2.30' Elev. = 3.51 + 1.99 = 5.50DEPT 1A using 17.11 cfs, S<sub>o</sub> = .0015 = 2.30' Elev. = 3.51 + 1.99 = 5.50

50° K = 0.50

40° K = 0.43

30° K = 0.35

25° K = 0.30

20° K = 0.25

15° K = 0.19

10° K = 0.13

5° K = 0.06

\* Elev. 2.9 = Ex. Elev. on

(6000)



MHW ELEV. = 1.1005  
MLW ELEV. = -1.6554  
LD-229  
July 2000

DATE DRAINAGE

ROUTE:

PROJ:

PER PROPERTIES

STORM SEWER DESIGN

COUNTY:

DISTRICT: REV AUG. 2013

COMPUTATIONS

DESCRIPTION:

1.00' 285.2/24.7276

SHEET OF

FROM POINT	TO POINT	AREA DRAIN "A" ACRES	RUN OFF COEF. C	CA	INLET TIME MIN-UTES	RAIN FALL IN./HR.	RUN OFF Q C.F.S.	INVERT ELEVATIONS		SLOPE FT./FT.	DIA. IN.	CAPA. CITY C.F.S.	VEL. F.P.S.	FLOW TIME MIN.	REMARKS
								UPPER END	LOWER END						
10	11	.7636	.7684	.5837	5	9.00	5.68	4.77	3.73	.0025	24"	12.25	3.82	1.82	(V610)
11	12	.7583	.8249	.0255	6.89	9.03	10.94	3.73	3.33	.0020	24"	10.96	3.49	0.83	✓
12	12A				7.72	8.30	13.93	3.33	3.13	.0034	24"	14.29	5.18	0.19	✓
12A	13	.5346	.6377	.376	7.91	8.75	13.89	3.13	2.49	.0034	24"	14.29	5.18	0.61	✓
RR TRACKS	13	.1234	.70	.0902	10	8.22	0.74	8.50	7.29	.0103	12"	3.92	3.37	0.51	
9A	8A	1.651	.7207	1.1998	15	7.13	8.01	4.09	3.44	.0000	13"	3.81	5.63	0.32	✓
8A	7A	2.2013	.73	1.6055	15.32	7.13	20.01	3.44	2.00	.0007	24"	20.06	6.33	0.49	✓
15	14	.816	.779	.6357	8.5	8.59	5.46	3.23	2.96	.0030	18"	6.23	3.93	.37	✓
14	13	1.3335	.7113	.9385	8.87	3.47	13.79	2.90	2.49	.0024	24"	13.86	5.03	.65	✓
13	7A	1.0974	.7313	.3032	9.52	8.33	34.22	2.49	2.00	.0023	30"	34.65	5.59	.64	✓
7A	6	1.4733	.7703	1.1356	15.81	7.04	56.67	4.00	1.87	.0002	36"	56.89	9.13	.02	✓
5A	6	.8509	.70	.5956	9.50	8.34	4.99	5.09	3.41	.0051	15"	5.00	4.64	1.19	✓
6	OUT	2.5361	.7034	1.7839	10.47	6.93	72.27	-0.58	-1.30	.0005	42"	77.07	9.11	.26	✓

10	10A	.5867	.5867	.5867	5	9.00	5.63	4.77	4.25	.0025	24"	12.25	3.82		
10A	11	.5867	.5867	.5867	5	9.00	5.63	4.25	3.73	.0025	24"	12.25	3.82		







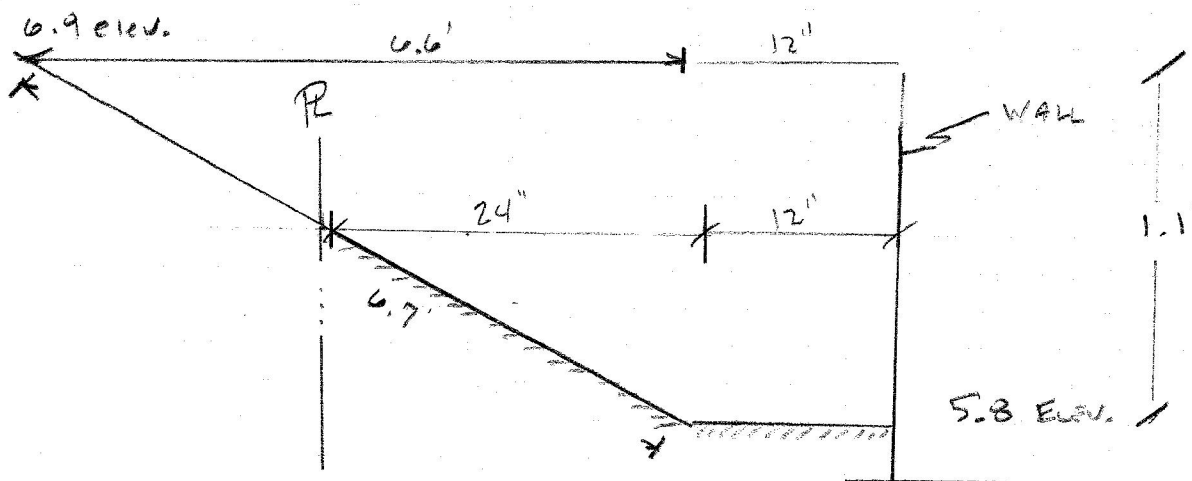
CHECK DITCH CAPACITY NEAR STMH-1

$$Q_{100} = CAI$$

$$= (0.5)(1.0384)(10.0) = 0.19 \text{ cfs}$$

30" FES DOWNSTREAM  
TO PICK UP OPPOSITE RUNOFF

FORM LD-269 SHOWS HW DENTAS 0.37', ELEV. = 6.07, TOP BANK = 6.9



$$XS = (6.9 - 5.8)(1.0) = 1.1 \text{ ft}^2$$

$$+ 0.5 \times 6.6' \times 1.1' = 3.63 \text{ ft}^2 / \Sigma = 4.73$$

$$W.P. = 6.7 \times 1.02 = 7.7$$

$$R = 4.73 / 7.7 = 0.61$$

n FACTOR = 0.45, DENSE GROWTH,  $S_o = 0.005 \text{ F/F}$

$$Q_{cap.} = 1.486 / n A R^{2/3} S_o^{1/2}$$

$$= (1.486 / 0.45) (4.73) (0.61)^{0.67} (0.005)^{0.5}$$

$$= 0.79 \text{ cfs} > 0.19 \text{ cfs}$$



[illegible]



## ENTRANCE LOSS COEFFICIENTS ( $K_e$ ) OUTLET CONTROL, FULL OR PARTIALLY FULL

Type of Structure and Design of Entrance	Coefficient
Pipe, Concrete	
Mitered to conform to fill slope	0.7
End-section conforming to fill slope	0.5
Projecting from fill, square cut end	0.5
Headwall or headwall and wingwall	
Square-edge	0.5
Rounded (radius = 1/12 D)	0.2
Socket end of pipe (groove end)	0.2
Projecting from fill, socket end (groove end)	0.2
Beveled edges, 33.7° or 45° bevels	0.2
Side or slope-tapered inlet	0.2
Pipe, Corrugated Metal (or Corrugated HDPE)	
Projecting from fill (no headwall)	0.9
Mitered to conform to fill slope, paved or unpaved slope	0.7
Headwall or headwall and wingwall, square-edge	0.5
End section conforming and to fill slope	0.5
Beveled edges, 33.7° or 45° bevels	0.2
Side or slope-tapered inlet	0.2
Box, Reinforced Concrete	
Wingwalls parallel (extension of sides), square edged at crown	0.7
Wingwalls at 10° to 25° or 30° to 75° to barrel, square edged on 3 edges	0.5
rounded on 3 edges to radius of 1/12 barrel	0.2
Wingwalls at 30° to 75° to barrel, crown edge rounded to radius 1/12 of barrel	0.2
Side or slope-tapered inlet	0.2

Note:

End Section conforming to fill slope made of metal, concrete, or HDPE, are the sections commonly available from manufacturers. From limited hydraulic test they are equivalent in operation to a headwall in both inlet and outlet control. Some end sections incorporating a closed taper in their design have a superior hydraulic performance. These latter sections can be designed using the information given for the beveled inlet.



## OUTLET CONTROL, CIRCULAR CONCRETE PIPE RECOMMENDED MANNING'S n-VALUES

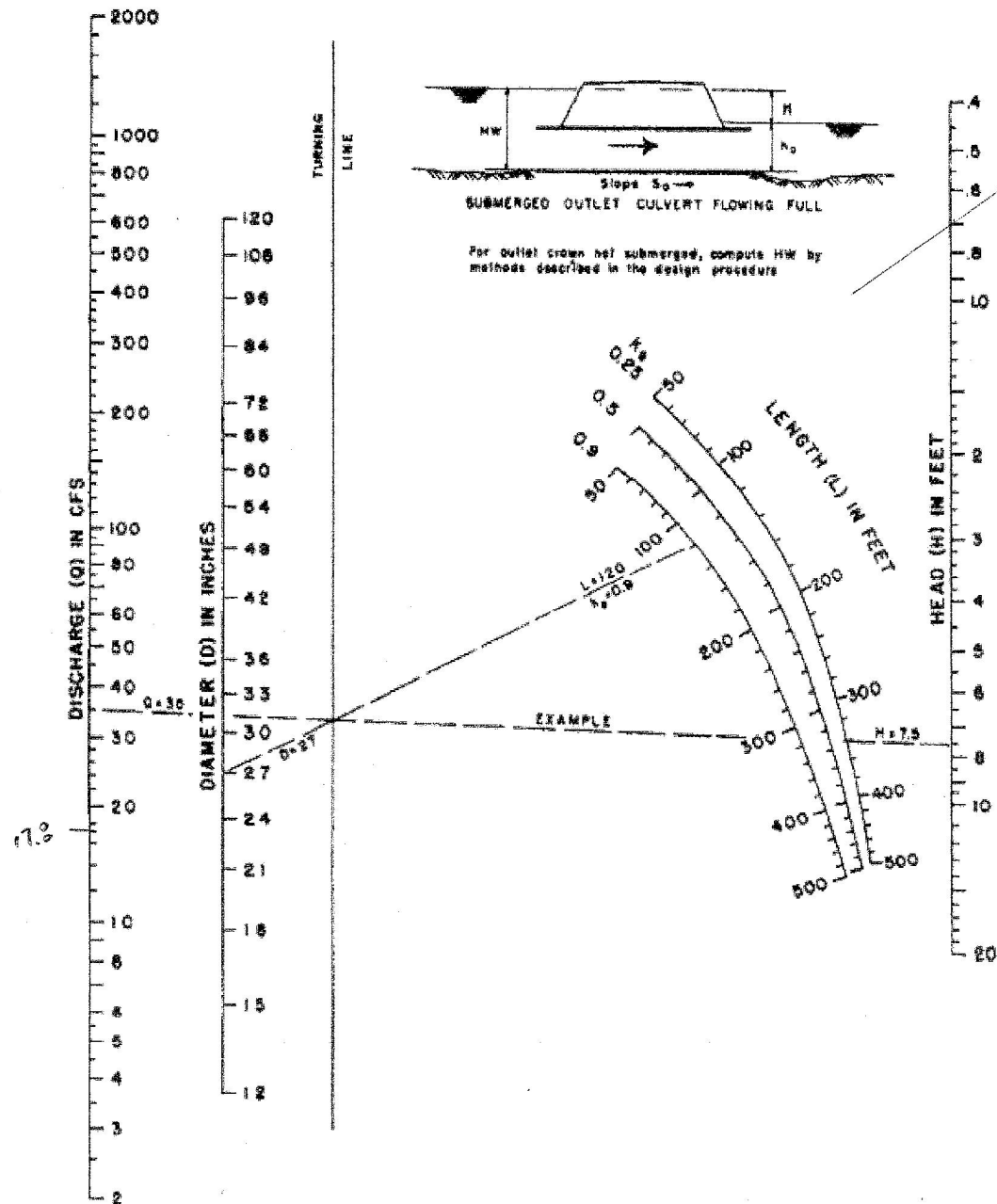
Type of Conduit	Wall Description	Manning's n
Concrete Pipe	Smooth walls	0.010 - 0.013
Concrete Boxes	Smooth walls	0.012 - 0.015
Corrugated Metal	2 2/3 by 1/2 inch	0.022 - 0.027
Pipes and Boxes, Annular or	corrugations	
Helical Pipe	6 by 1 inch	0.022 - 0.025
	corrugations	
	5 by 1 inch	0.025 - 0.026
	corrugations	
	3 by 1 inch	0.027 - 0.028
	corrugations	
	6 by 2 inch	0.033 - 0.035
	structural plate	
	9 by 2 1/2 inch	0.033 - 0.037
	structural plate	
Corrugated Metal	2 2/3 by 1/2 inch corrugations	0.012 - 0.024
Pipe		
Spiral Rib Metal	Smooth walls	0.012-0.013
(Steel or Alum.)		
PVC	Smooth interior	0.010 - 0.012
Polyethylene (PE or HDPE)	Smooth interior	0.011 - 0.013
Corrugated PE or HDPE	Corrugated interior	0.022 - 0.026

Note 1: The values indicated in this table are recommended Manning's "n" design values. Actual field values may vary depending on the effects of abrasion, corrosion, deflection, and joint conditions. Concrete pipe with poor joints and deteriorated walls may have "n" values of 0.014 to 0.018. Corrugated metal with join and wall problems may also have higher "n" values, and in addition, may experience shape changes which could adversely affect the general hydraulic characteristics of the culvert.

Note 2: For further information concerning Manning n values for selected conduits consult Hydraulic Design of Highway Culverts, Federal Highway Administration, HDS No. 5, page 163.



## OUTLET CONTROL, CIRCULAR CORRUGATED METAL PIPE



HEAD FOR  
STANDARD  
C. M. PIPE CULVERTS  
FLOWING FULL  
 $n = 0.024$

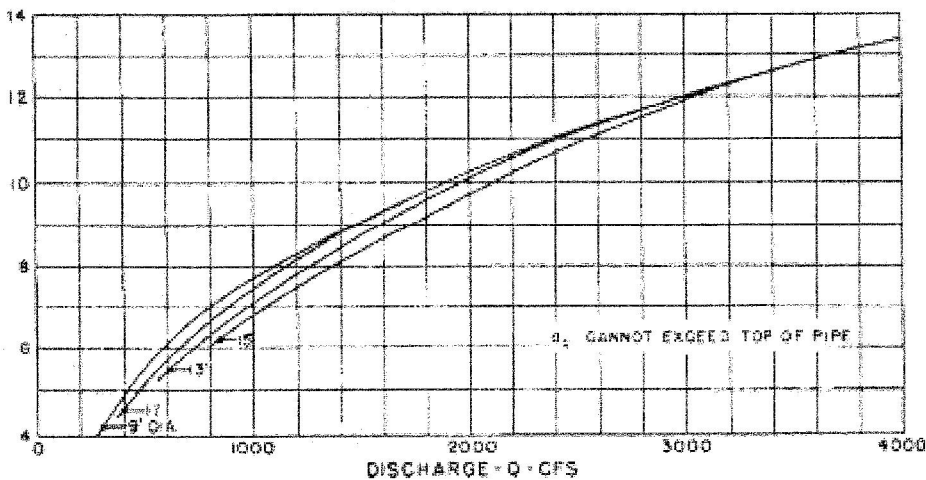
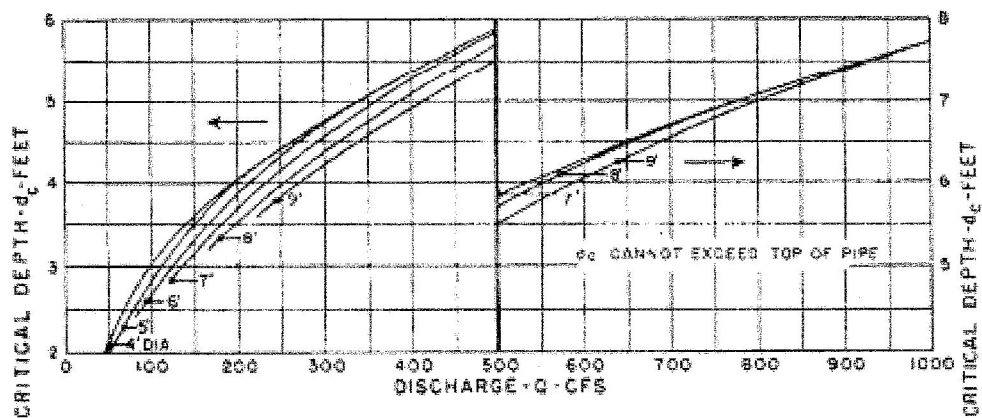
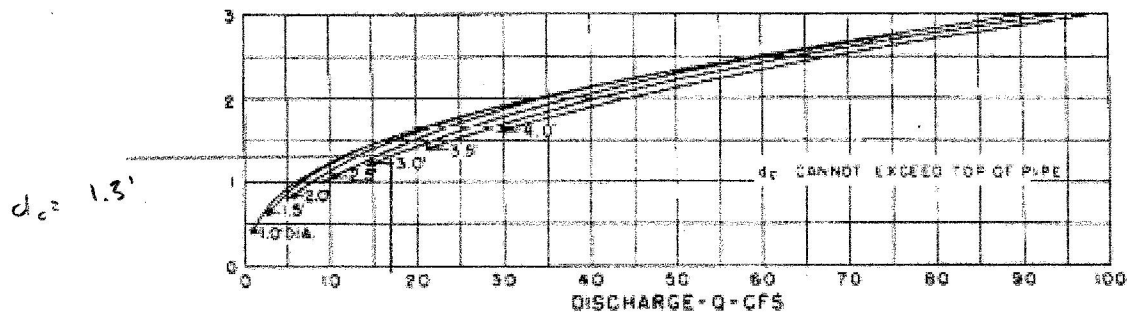
BUREAU OF PUBLIC ROADS JAN. 1953



## CRITICAL DEPTH, CIRCULAR PIPE



CHART 4



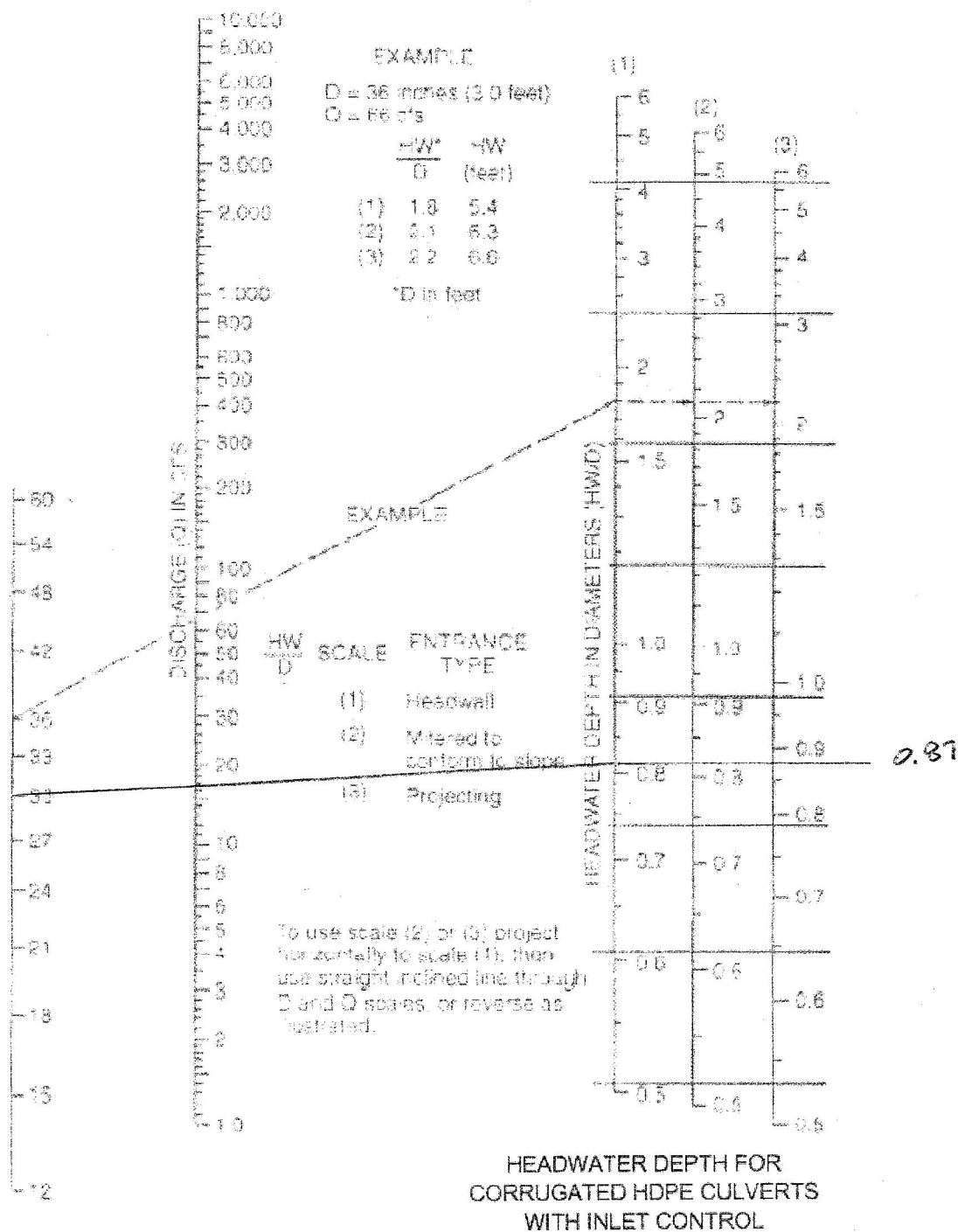
BUREAU OF PUBLIC ROADS

JAN. 1964

CRITICAL DEPTH  
CIRCULAR PIPE



## INLET CONTROL, CIRCULAR HDPE PIPE





# Hydrograph Plot

English

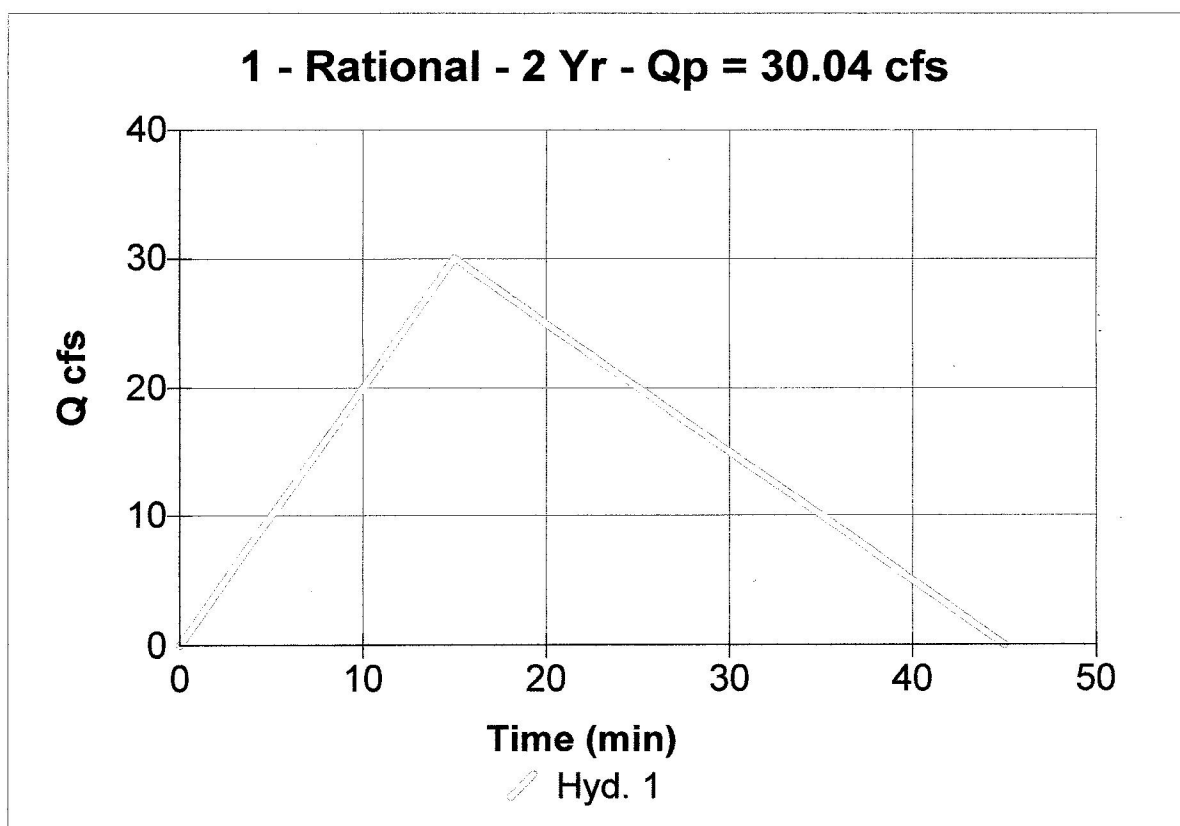
## Hyd. No. 1

### 2 YEAR STORM AT BMP

Hydrograph type = Rational  
Storm frequency = 2 yrs  
Drainage area = 8.5 ac  
Intensity = 3.91 in  
I-D-F Curve = NORFOLK1.IDF

Peak discharge = 30.04 cfs  
Time interval = 1 min  
Runoff coeff. = 0.9  
Time of conc. (Tc) = 15 min  
Reced. limb factor = 2

Total Volume = 40,561 cuft





Performance Database (NPRPD). In addition, we have liberally borrowed from the cutting-edge ideas expressed in the newer BMP stds & specs from other states in the region.

To assist in development of these BMP stds & specs, a literature search was performed to compile data to support updated runoff volume reduction and pollution removal capabilities for different BMPs. Based on the research findings, runoff volume reduction rates were assigned and removal rates for Total Phosphorus were updated for various BMPs, as shown in **Table 4.1**. The explanation for these decisions can be found in the Technical Memorandum: The Runoff Reduction Method [pdf] developed for DCR and others by the Center for Watershed Protection, in support of DCR's regulation and Handbook revision processes.

**Table 4.1. BMP Pollutant Removal Efficiencies (March 1, 2011)**

Practice Number	Practice	Removal of TP by Runoff Reduction (RR, as %) (based upon 1 inch of rainfall)	Removal of TP by Treatment – Pollutant (EMC) Reduction (PR, as %)	Total Mass Load Removal of Total Phosphorus (TR, as %)
1	Rooftop Disconnection	25 or 50 <sup>1</sup>	0	25 or 50 <sup>1</sup>
2	Sheetflow to Vegetated Filter or Conserved Open Space 1	25 to 50 <sup>1</sup>	0	25 to 50 <sup>1</sup>
	Sheetflow to Vegetated Filter or Conserved Open Space 2 <sup>5</sup>	50 to 75 <sup>1</sup>	0	50 to 75 <sup>1</sup>
3	Grass Channel	10 to 20 <sup>1</sup>	15	23
4	Soil Amendments	Used to decrease runoff coefficient for turf cover at the site. See the design specs for Roof Disconnection, Sheet Flow to Vegetated Filter or Conserved Open Space, and Grass Channels		
5	Vegetated Roof 1	45	0	45
	Vegetated Roof 2	60	0	60
6	Rainwater Harvesting	Up to 90 <sup>3, 5</sup>	0	Up to 90 <sup>3, 5</sup>
7	Permeable Pavement 1	45	25	59



	<b>Permeable Pavement</b>	<b>75</b>	<b>25</b>	<b>81</b>
	<b>2</b>			
<b>8</b>	<b>Infiltration 1</b>	<b>50</b>	<b>25</b>	<b>63</b>
	<b>Infiltration 2</b>	<b>90</b>	<b>25</b>	<b>93</b>
<b>9</b>	<b>Bioretention 1</b>	<b>40</b>	<b>25</b>	<b>55</b>
	<b>Bioretention 2</b>	<b>80</b>	<b>50</b>	<b>90</b>
	<b>Urban Bioretention</b>	<b>40</b>	<b>25</b>	<b>55</b>
<b>10</b>	<b>Dry Swale 1</b>	<b>40</b>	<b>20</b>	<b>52</b>
	<b>Dry Swale 2</b>	<b>60</b>	<b>40</b>	<b>76</b>
<b>11</b>	<b>Wet Swale 1</b>	<b>0</b>	<b>20</b>	<b>20</b>
	<b>Wet Swale 2</b>	<b>0</b>	<b>40</b>	<b>40</b>
<b>12</b>	<b>Filtering Practice 1</b>	<b>0</b>	<b>60</b>	<b>60</b>
	<b>Filtering Practice 2</b>	<b>0</b>	<b>65</b>	<b>65</b>
<b>13</b>	<b>Constructed Wetland 1</b>	<b>0</b>	<b>50</b>	<b>50</b>
	<b>Constructed Wetland 2</b>	<b>0</b>	<b>75</b>	<b>75</b>
<b>14</b>	<b>Wet Pond 1</b>	<b>0</b>	<b>50 (45) <sup>4</sup></b>	<b>50 (45) <sup>4</sup></b>
	<b>Wet Pond 2</b>	<b>0</b>	<b>75 (65) <sup>4</sup></b>	<b>75 (65) <sup>4</sup></b>
<b>15</b>	<b>Extended Detention Pond 1</b>	<b>0</b>	<b>15</b>	<b>15</b>
	<b>Extended Detention Pond 2</b>	<b>15</b>	<b>15</b>	<b>31</b>



- SPECIAL NOTES
- Maximum allowable slopes on driveways shall be 12:1. Driveways shall be placed to nearest joint. Contractor to verify limits of all drives with the Engineer.
  - Preserve all power poles not in conflict. Coordinate relocation of conflicting power poles with the Engineer and company. Cost of utility pole relocations shall be by utility owner.
  - All drives shall be concrete in the R.O.W.
  - There shall be a minimum of six inches between adjacent driveway entrance aprons as measured at the curb.
  - Removal and replacement of gravel drives and tie-ins at the edge of aprons is the responsibility of the contractor. Coordinate limits of work with the Engineer. Drives shall be a minimum of 4" gravel beyond existing R.O.W. (see plans for locations).
  - All water meters and sanitary sewer cleanouts must be set behind the curb within the City right-of-way.
  - Coordinate replacement of outdated meters with the Engineer and the City Public Utilities Department.
  - All fence removal and replacement shall be coordinated by the Engineer and homeowner.
  - The Contractor shall adjust the tie-in length for new walks to accommodate steps as directed by the Engineer.
  - The Contractor shall remove and replace curb and gutter as necessary to complete utility work. Curb and gutter shall be replaced in 20 foot sections. The cost of replacing this curb and gutter will not be measured separate for payment and will be included in the respective utility pay item.
  - All items of work required by the documents to complete the project, but not specifically included in a pay item shall be considered an incidental item in accordance with Specification Section 109.

LEGEND

- |  |                      |  |                           |
|--|----------------------|--|---------------------------|
|  | FIRE HYDRANT         |  | OVERHEAD WIRE             |
|  | CURB & GUTTER        |  | LIGHT POLE                |
|  | EDGE OF PAVEMENT     |  | POWER POLE                |
|  | SWALE                |  | CATCH BASIN               |
|  | CTV BOX              |  | SANITARY SEWER MANHOLE    |
|  | SIGN                 |  | STORM DRAIN MANHOLE       |
|  | STREET LAMP          |  | INVERT                    |
|  | TELE. BOX            |  | GRADE TO DRAIN            |
|  | SEWER CLEAN OUT      |  | FINISHED GRADE            |
|  | WATER METER          |  | FLOW LINE                 |
|  | WATER VALVE          |  | TOP OF CURB               |
|  | FENCE                |  | FIRE HYDRANT              |
|  | MANHOLE              |  | PROP. ELEVATION           |
|  | CATCH BASIN          |  | PROP. CONTOUR             |
|  | PROPOSED DROP INLET  |  | EXIST. ELEVATION          |
|  | PROPOSED STORM SEWER |  | VEGETATED WETLANDS        |
|  | SEWER PIPE           |  | TEMPORARY BENCHMARK (TBM) |
|  | WATER LINE           |  | FLARED END SECTION        |
|  |                      |  | IRON ROD FOUND            |

THIS PLAN DOES NOT GUARANTEE THE EXISTENCE OR LOCATION OF THE UNDERGROUND UTILITIES SHOWN HEREON, NOR DOES IT GUARANTEE THE NON-EXISTENCE OF UNDERGROUND UTILITIES WHICH MAY BE PRESENT. THIS PLAN DOES NOT GUARANTEE THE ABSENCE OF CONFLICTS WITH UNDERGROUND UTILITIES. IF, DURING THE COURSE OF CONSTRUCTION, DISCREPANCIES ARE DISCOVERED BETWEEN THE UNDERGROUND UTILITIES SHOWN ON THIS PLAN AND ACTUAL FIELD CONDITIONS, THE CONTRACTOR SHALL NOTIFY GALLUP SURVEYORS & ENGINEERS, LTD. BEFORE PROCEEDING WITH FURTHER CONSTRUCTION.

IT SHALL BE THE OWNER'S/DEVELOPER'S RESPONSIBILITY TO ASCERTAIN THE EXISTENCE AND/OR NON-EXISTENCE OF THE FOLLOWING WITH REGARDS TO THIS SITE.

- DEED RESTRICTIONS
- JURISDICTIONAL WETLANDS
- HAZARDOUS MATERIALS

PREPARED FOR:

PER PROPERTIES  
P.O. BOX 57008  
VIRGINIA BEACH, VA. 23457  
PHONE: 757-426-6824  
FAX: 757-721-9071  
ATTN: JIM SALMONS

PREPARED BY:

GALLUP SURVEYORS & ENGINEERS, LTD.  
323 FIRST COLONIAL ROAD  
VIRGINIA BEACH, VIRGINIA 23454  
PHONE: 757-428-8132  
FAX: 757-425-2390

# COMMERCIAL SITE PLAN FOR PER PROPERTIES

NOTE:  
THIS PLAN IS TO BE USED FOR EROSION AND SEDIMENT CONTROL, DRAINAGE STRUCTURE AND PIPE INSTALLATION ONLY. THE PROPOSED BUILDINGS AND VARIOUS INFRASTRUCTURE SHOWN ARE ILLUSTRATIVE ONLY AND ARE NOT TO BE CONSTRUCTED UNTIL THE CITY OF PORTSMOUTH HAS APPROVED THE COMMERCIAL SITE PLAN

SITE DATA

LEGAL: PROPERTY LABELED "PORTSMOUTH PORT AND INDUSTRIAL COMMISSION SHOWN ON BOUNDARY SURVEY OF THE PROPERTY OF PORTSMOUTH PORT AND INDUSTRIAL COMMISSION, PORTSMOUTH, VIRGINIA RECORDED IN MAP BOOK 22, PAGE 109, 110  
ADDITIONAL REFERENCE: DEED BOOK 772, PAGE 381

ZONED: INDUSTRIAL

BENCHMARK: CITY OF PORTSMOUTH BM STATION 41-35  
IRON ROD SET FLUSH WITH PAVEMENT LOCATED IN THE APPROXIMATE CENTERLINE OF VENEER RD., NORTHWEST FROM A FIRE HYDRANT LOCATED ON THE EAST SIDE OF VENEER ROAD, 34.5' NORTHEAST OF CENTER OF FACE OF CATCH BASIN, AND 16.9' EAST OF BACK OF CURB; ELEVATION 4.30  
DATUM: NAVD 88

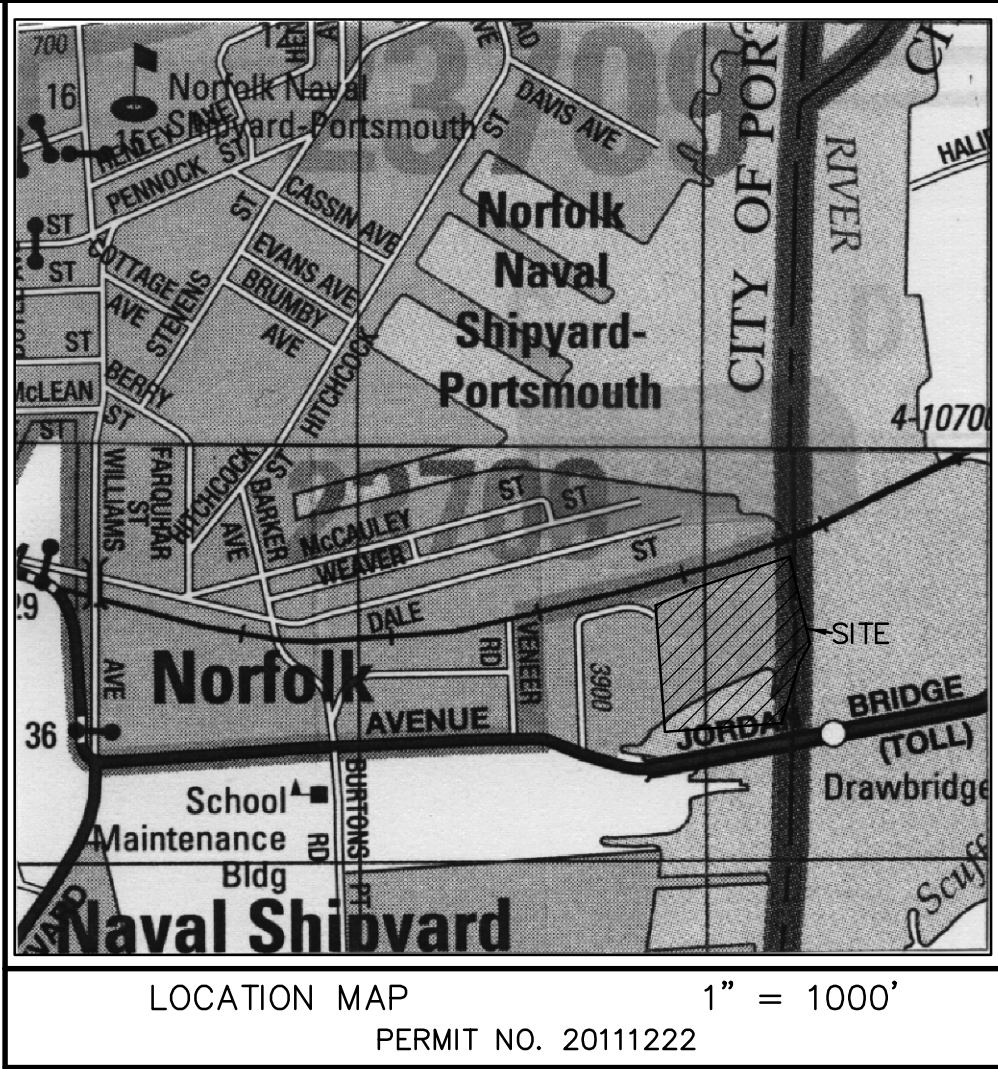
FLOOD ZONE INFORMATION:  
ACCORDING TO F.E.M.A.'S FLOOD INSURANCE RATE MAP (F.I.R.M.), THE PROPERTY SHOWN HEREON APPEARS TO FALL WITHIN FLOOD ZONE 'B', AND ZONE A4 COMMUNITY PANEL NO. 515529-0060B, MAP REVISED 11/02/83, BASE FLOOD EL. 8.5 (NGVD 29) (BASE FLOOD ELEVATION ADJUSTED TO NAV 88 IS APPROXIMATELY 7.8)

PORTSMOUTH STANDARD NOTES

- ALL CONSTRUCTION METHODS AND MATERIALS SHALL CONFORM TO THE HRPDC STANDARDS & SPECIFICATIONS AS MODIFIED BY THE PORTSMOUTH SPECIAL CONDITIONS.
- ELEVATIONS SHOWN HEREON ARE BASED ON CITY OF PORTSMOUTH (NAV 88) DATUM.
- ALL CONCRETE SHALL BE CLASS A3 AIR-ENTRAINED (3,000 P.S.I.).
- TEMPORARY DRAINAGE DURING CONSTRUCTION SHALL BE PROVIDED BY THE CONTRACTOR TO RELIEVE AREAS THAT MAY CAUSE DAMAGE TO ROADWAYS.
- PRIOR TO CONSTRUCTION OR EXCAVATION, THE CONTRACTOR SHALL ASSUME THE RESPONSIBILITY OF LOCATING ANY UNDERGROUND UTILITIES (PUBLIC OR PRIVATE) THAT MAY EXIST AND CROSS THROUGH THE AREA OF CONSTRUCTION THAT IS NOT SHOWN ON THESE PLANS. UTILITY COMPANIES SHALL BE NOTIFIED 48 HOURS IN ADVANCE OF ANY EXCAVATION IN THE PROXIMITY OF THEIR UTILITIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR REPAIRING, AT HIS EXPENSE, ANY EXISTING UTILITIES DAMAGED DURING CONSTRUCTION.
- PRIOR TO CONSTRUCTION WITHIN ANY EXISTING PUBLIC RIGHT-OF-WAY, THE CONTRACTOR SHALL OBTAIN ALL NECESSARY PERMITS FROM THE CITY OF PORTSMOUTH, VIRGINIA.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR REPLACING WITH MATCHING MATERIALS ANY PAVEMENT, DRIVEWAYS, WALKS, CURBS, ETC. THAT MUST BE CUT OR THAT IS DAMAGED DURING CONSTRUCTION.
- ALL STORM SEWER PIPES, DROP INLETS, AND CURB INLETS SHALL BE CLEANED OF DEBRIS AND ERODED MATERIALS AT LAST STAGES OF CONSTRUCTION.
- ALL SLOPES WITHIN RIGHT-OF-WAY OR IN CITY EASEMENTS SHALL BE TOP-SOILED AND SEEDED IN ACCORDANCE WITH CITY OF PORTSMOUTH SPECIFICATIONS.
- PAVEMENT REPLACEMENT WITHIN THE CITY RIGHT-OF-WAY SHALL MATCH THE EXISTING PAVEMENT.
- BEFORE YOU DIG, TO MISS THE UTILITIES, CALL MISS UTILITY OF TIDEWATER AT 811.

CONSULTANTS

BOUNDARY SURVEY PREPARED BY STEVE BOONE AND ASSOCIATES, P.C., RECORDED IN M.B. 22, P. 109, 110  
CONTAINMENT BERM SHOWN OBTAINED FROM PLANS TITLED, "REMEDIAL DESIGN - PHASE 2, EAST SIDE CONTAINMENT BERM, ATLANTIC WOOD INDUSTRIES SUPERFUND SITE, PREPARED BY EA ENGINEERING, SCIENCE, AND TECHNOLOGY, DATED 1/2011  
UTILITIES SHOWN OBTAINED FROM PLANS TITLED, "REMEDIAL DESIGN - PHASE 2, EAST SIDE CONTAINMENT BERM, ATLANTIC WOOD INDUSTRIES SUPERFUND SITE, PREPARED BY EA ENGINEERING, SCIENCE, AND TECHNOLOGY, DATED 1/2011, AND FROM FIELD SURVEY BY GALLUP SURVEYORS AND ASSOCIATES, AND FROM CITY RECORD DRAWINGS.



CONSTRUCTION SEQUENCE

- OBTAIN ALL REQUIRED PERMITS
- INSTALL SILT FENCE
- INSTALL CONSTRUCTION ENTRANCE
- ADJUST SILT FENCE AS REQUIRED
- PLACE CRUSHED CONCRETE FILL MATERIAL IN 6" LIFTS
- EXCAVATE FOR BMP AND STORM DRAINS
- INSTALL FILTER FABRIC, PIPES, INLETS, AND 57 STONE
- CONTINUE FILLING AND ADJUSTING BERM
- INSTALL INLET PROTECTION AS INLETS ARE SET.

ANY AND ALL MATERIAL/DEBRIS TRACKED ONTO A PUBLIC ROAD SURFACE SHALL BE CLEANED THOROUGHLY AT THE END OF EACH DAY. SEDIMENT SHALL BE REMOVED FROM ROADS BY SHOVELING AND/OR SWEEPING AND BE TRANSPORTED TO A SEDIMENT CONTROL DISPOSAL AREA.

ALL CRACKED CONCRETE IN THE R/W SHALL BE REMOVED AND REPLACED TO THE NEAREST JOINT. PATCHING IS NOT ACCEPTABLE.

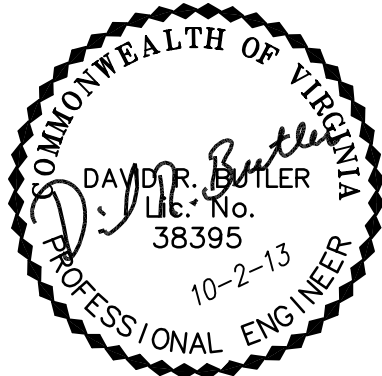
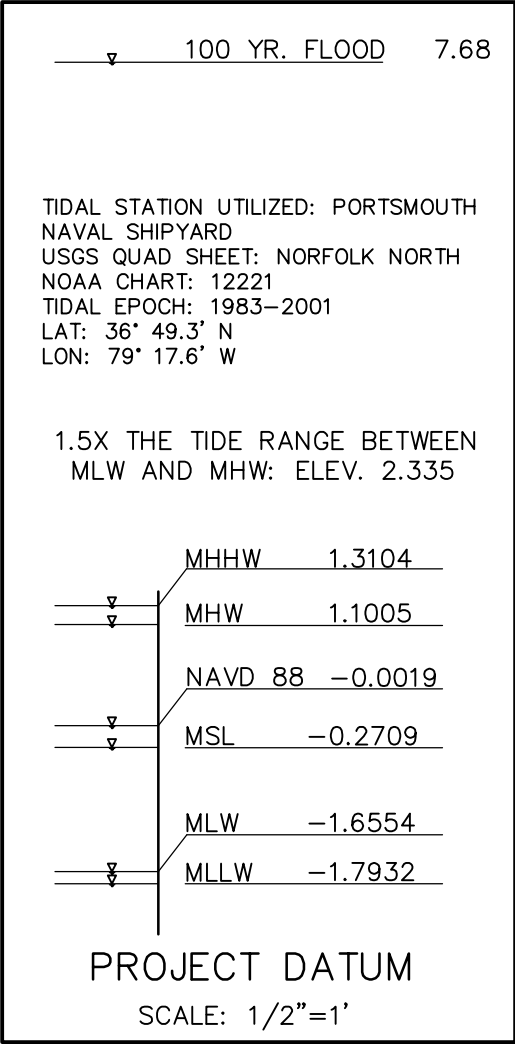
THE SITE CONTRACTOR SHALL HAVE A RESPONSIBLE LAND DISTURBER (RLD) CERTIFICATION.

ALL EXCAVATED MATERIAL FROM CONSTRUCTION SHALL BE DISPOSED OF IN A LAWFUL MANNER.

ALL DISTURBED AREAS SHALL BE SEEDED. (SEE SCHEDULE)

## INDEX:

SHEET 1--COVER SHEET  
SHEET 2--EROSION CONTROL PLAN  
SHEET 3--OVERALL SITE PLAN  
SHEET 4-5--GRADING AND UTILITY PLAN  
SHEET 6--DRAINAGE DETAILS AND NOTES  
SHEET 7--DETAILS AND NOTES  
SHEET 8--UTILITY DETAILS AND NOTES  
SHEET 9--BMP DETAILS AND NOTES  
SHEET 10-11--PUMP STATION NOTES AND DETAILS  
SHEET 12--EROSION CONTROL DETAILS AND NOTES  
SHEET 13--EROSION CONTROL NOTES



DATE	REVISION

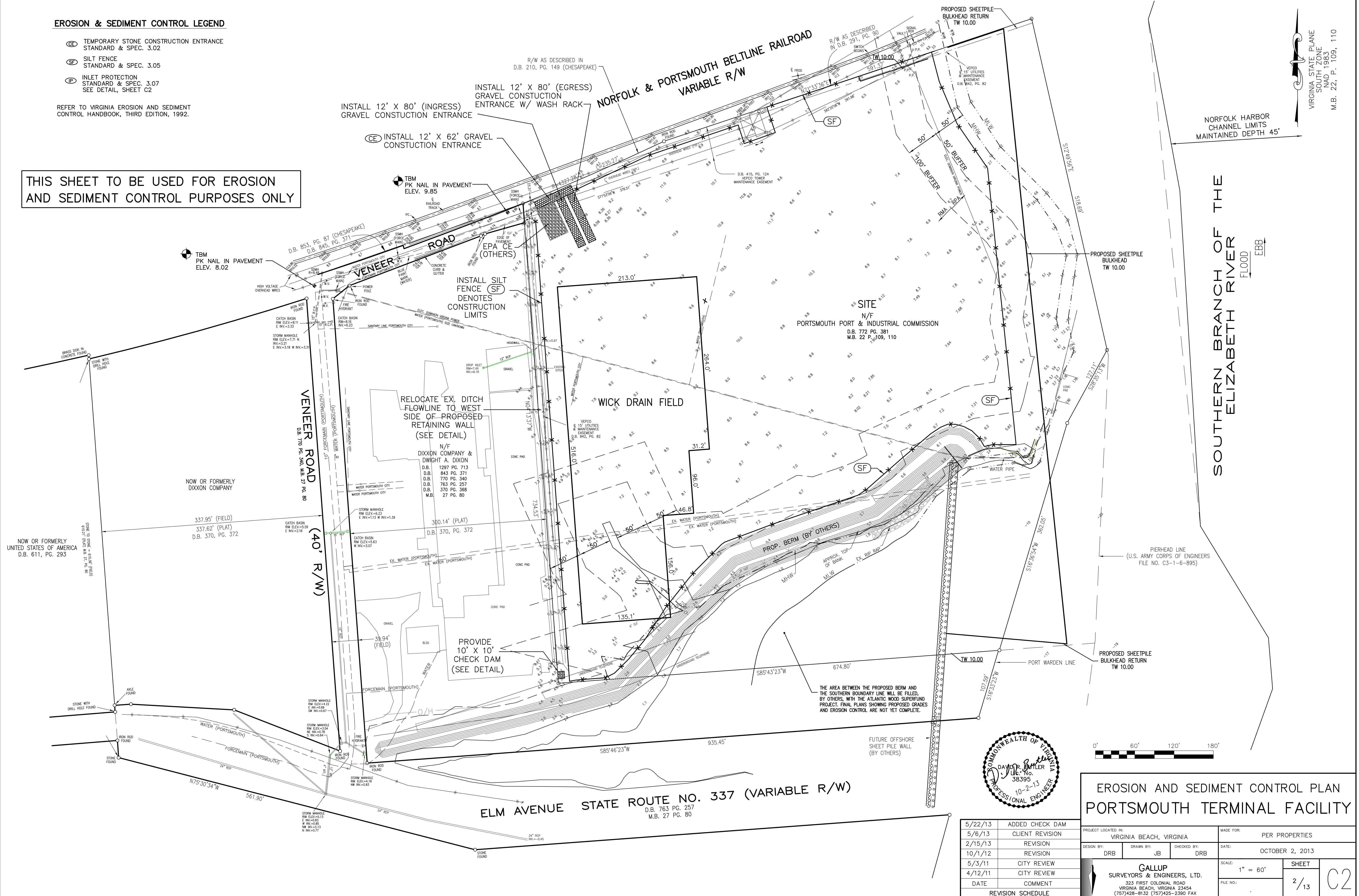


EROSION & SEDIMENT CONTROL LEGEND

- (CE) TEMPORARY STONE CONSTRUCTION ENTRANCE  
STANDARD & SPEC. 3.02
- (SF) SILT FENCE  
STANDARD & SPEC. 3.05
- (IP) INLET PROTECTION  
STANDARD & SPEC. 3.07  
SEE DETAIL, SHEET C2

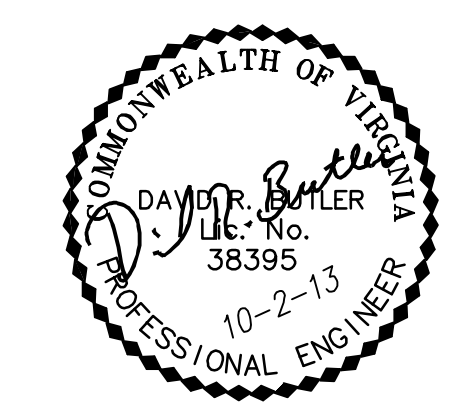
REFER TO VIRGINIA EROSION AND SEDIMENT  
CONTROL HANDBOOK, THIRD EDITION, 1992.

THIS SHEET TO BE USED FOR EROSION  
AND SEDIMENT CONTROL PURPOSES ONLY



SOUTHERN BRANCH OF THE  
ELIZABETH RIVER  
FLOOD  
EBB

VIRGINIA STATE PLANE  
SOUTH ZONE  
NAD 1983  
M.B. 22, P. 109, 110

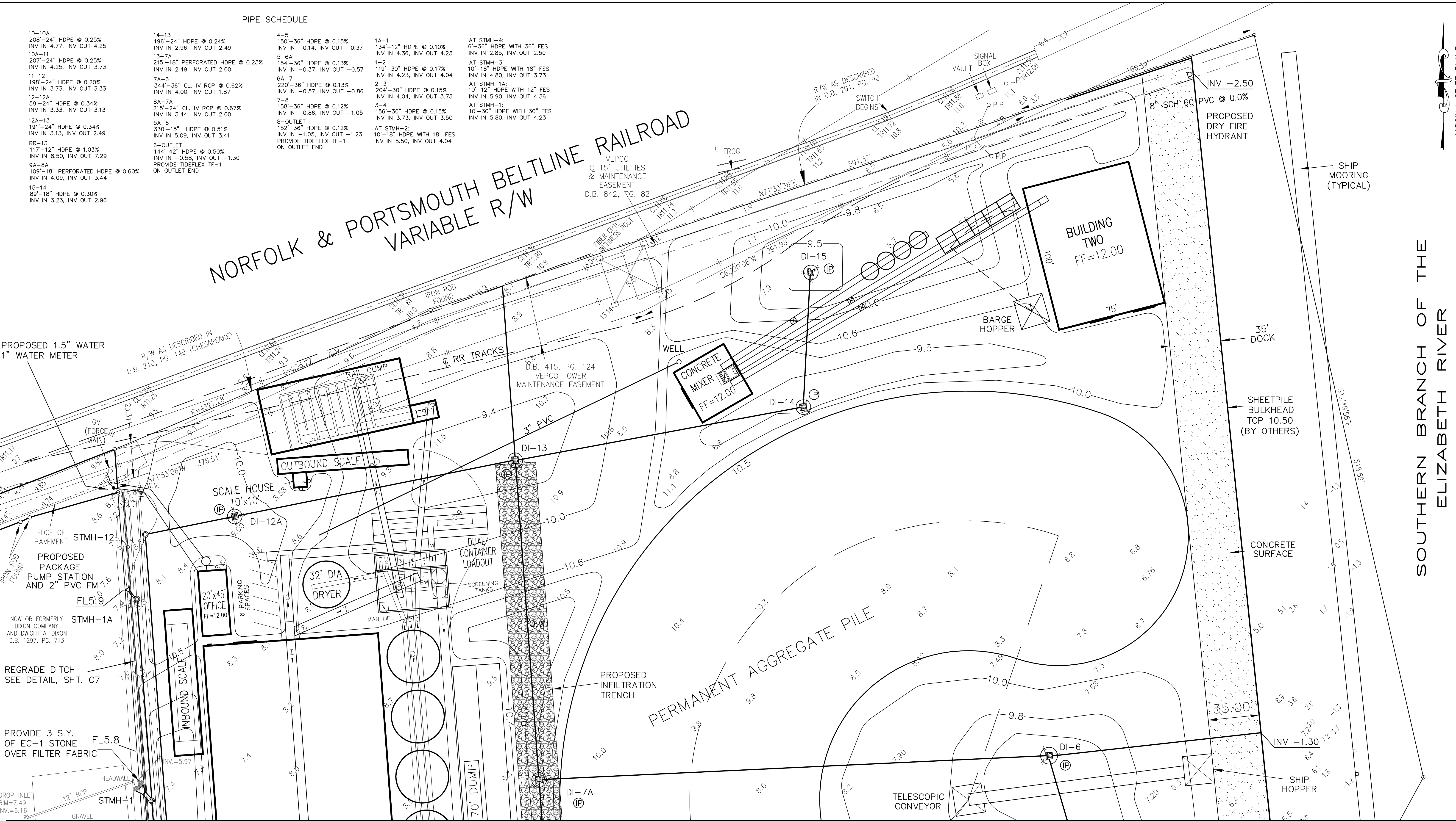


EROSION AND SEDIMENT CONTROL PLAN PORTSMOUTH TERMINAL FACILITY			
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE: OCTOBER 2, 2013
CALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 60'	SHEET 2/13
DATE 5/22/13		FILE NO.:	
5/6/13		C2	
2/15/13			
10/1/12			
5/3/11			
4/12/11			
DATE			
COMMENT			
REVISION SCHEDULE			









10-10A 208'-24" HDPE @ 0.25% INV IN 4.77, INV OUT 4.25	14-13 198'-24" HDPE @ 0.24% INV IN 2.96, INV OUT 2.49	4-5 150'-36" HDPE @ 0.15% INV IN -0.14, INV OUT -0.37	1A-1 134'-12" HDPE @ 0.10% INV IN 4.36, INV OUT 4.23	AT STMH-4: 6'-36" HDPE WITH 36" FES INV IN 2.85, INV OUT 2.50
10A-11 207'-24" HDPE @ 0.25% INV IN 4.25, INV OUT 3.73	13-7A 215'-18" PERFORATED HDPE @ 0.23% INV IN 2.49, INV OUT 2.00	5-6A 154'-36" HDPE @ 0.13% INV IN -0.37, INV OUT -0.57	1-2 119'-30" HDPE @ 0.17% INV IN 4.23, INV OUT 4.04	AT STMH-3: 10'-18" HDPE WITH 18" FES INV IN 4.80, INV OUT 3.73
11-12 198'-24" HDPE @ 0.20% INV IN 3.73, INV OUT 3.33	7A-6 344'-36" CL. IV RCP @ 0.62% INV IN 4.00, INV OUT 1.87	6A-7 220'-36" HDPE @ 0.13% INV IN -0.57, INV OUT -0.86	2-3 204'-30" HDPE @ 0.15% INV IN 4.04, INV OUT 3.73	AT STMH-1A: 10'-12" HDPE WITH 12" FES INV IN 5.90, INV OUT 4.36
12-12A 59'-24" HDPE @ 0.34% INV IN 3.33, INV OUT 3.13	8A-7A 215'-24" CL. IV RCP @ 0.67% INV IN 3.44, INV OUT 2.00	7-8 158'-36" HDPE @ 0.12% INV IN -0.86, INV OUT -1.05	3-4 156'-30" HDPE @ 0.15% INV IN 3.73, INV OUT 3.50	AT STMH-1: 10'-30" HDPE WITH 30" FES INV IN 5.80, INV OUT 4.23
12A-13 191'-24" HDPE @ 0.34% INV IN 3.13, INV OUT 2.49	RR-13 117'-12" HDPE @ 1.03% INV IN 8.50, INV OUT 7.29	8-OUTLET 152'-36" HDPE @ 0.12% INV IN -1.05, INV OUT -1.23 PROVIDE TIDEFLEX TF-1 ON OUTLET END	AT STMH-2: 10'-18" HDPE WITH 18" FES INV IN 5.50, INV OUT 4.04	
9A-8A 109'-18" PERFORATED HDPE @ 0.60% INV IN 4.09, INV OUT 3.44	6-OUTLET 144'-42" HDPE @ 0.50% INV IN -0.58, INV OUT -1.30 PROVIDE TIDEFLEX TF-1 ON OUTLET END			
15-14 89'-18" HDPE @ 0.30% INV IN 3.23, INV OUT 2.96				

PROPOSED 1.5" WATER  
1" WATER METER

NOW OR FORMERLY  
DIXON COMPANY  
AND DWIGHT A. DIXON  
D.B. 1297, PG. 713

REGRADE DITCH  
SEE DETAIL, SHT. C7

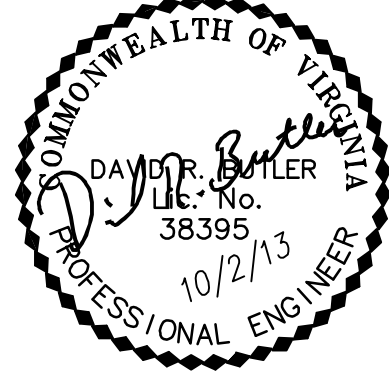
PROVIDE 3 S.Y.  
OF EC-1 STONE  
OVER FILTER FABRIC

DROP INLET  
RIM=7.49  
INV.=6.16

DRAINAGE STRUCTURE SCHEDULE

1A. STMH RIM 10.50 INV 4.36	6. DI RIM 9.40 INV (E) -0.58 INV (W) 1.87 INV (S) 3.41	11. DI RIM 9.80 INV 3.73	7A. DI RIM 9.50 INV (N,S) 2.00 INV (E) 4.00
1. STMH RIM 10.50 INV 4.23	7. STMH RIM 10.50 INV -0.86	12. STMH RIM 10.40 INV 3.33	8A. RIM 9.60 INV 3.44
2. STMH RIM 10.50 INV 4.04	5A. DI RIM 9.10 INV 5.09	12A. DI RIM 9.50 INV 3.13	9A. RIM 9.35 INV 4.09
3. STMH RIM 10.50 INV 3.73	10A. DI RIM 9.80 INV 4.25	13. DI RIM 9.35 INV 2.49 (E,W,S) INV 7.29 (N)	6A. RIM 9.80 INV -0.57
4. STMH RIM 8.20 INV (N) 3.50 INV (E) -0.14 INV (W) 2.50	8. STMH RIM 10.50 INV -1.05	14. DI RIM 9.35 INV 2.96	
5. STMH RIM 10.20 INV -0.37	10. DI RIM 9.80 INV 4.77	15. DI RIM 9.35 INV 3.23	

NOTES:  
THE SILT SACK PRODUCT SHOWN ON SHEET C7 IS  
TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN  
PERMANENT FOR DRAINAGE STRUCTURES  
7A, 8A, 9A, AND 13.  
  
THE INVERTS SHOWN ON THE DROP INLET DENOTES  
THE INVERT OF THE PIPES. PROVIDE A 12" DEEP  
SUMP (BELOW THE PIPE INVERT) ON THE DROP INLETS  
FOR MAINTENANCE PURPOSES FOR STRUCTURES  
7A, 8A, 9A, AND 13.  
  
O.W. DENOTES REQUIRED OBSERVATION WELLS;  
SEE DETAIL ON SHEET C9.  
  
ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET SHAPING.  
SURFACE AREA OF THE SITE WILL BE GRAVEL



GRADING PLAN AND UTILITY PLAN

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
CALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 30'	SHEET 4 / 13

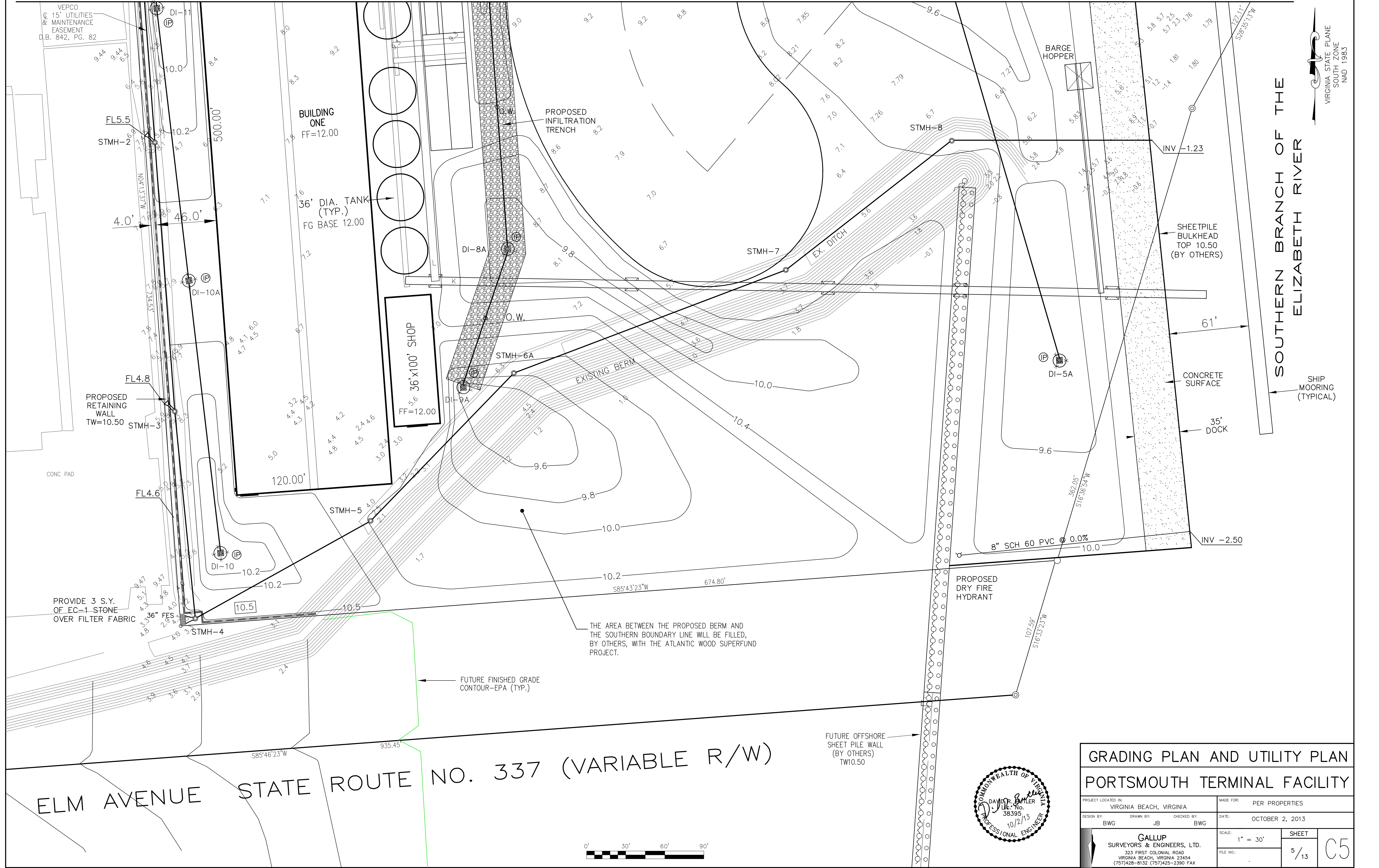
C4

SOUTHERN BRANCH OF THE  
ELIZABETH RIVER





MATCH LINE SEE SHEET C4



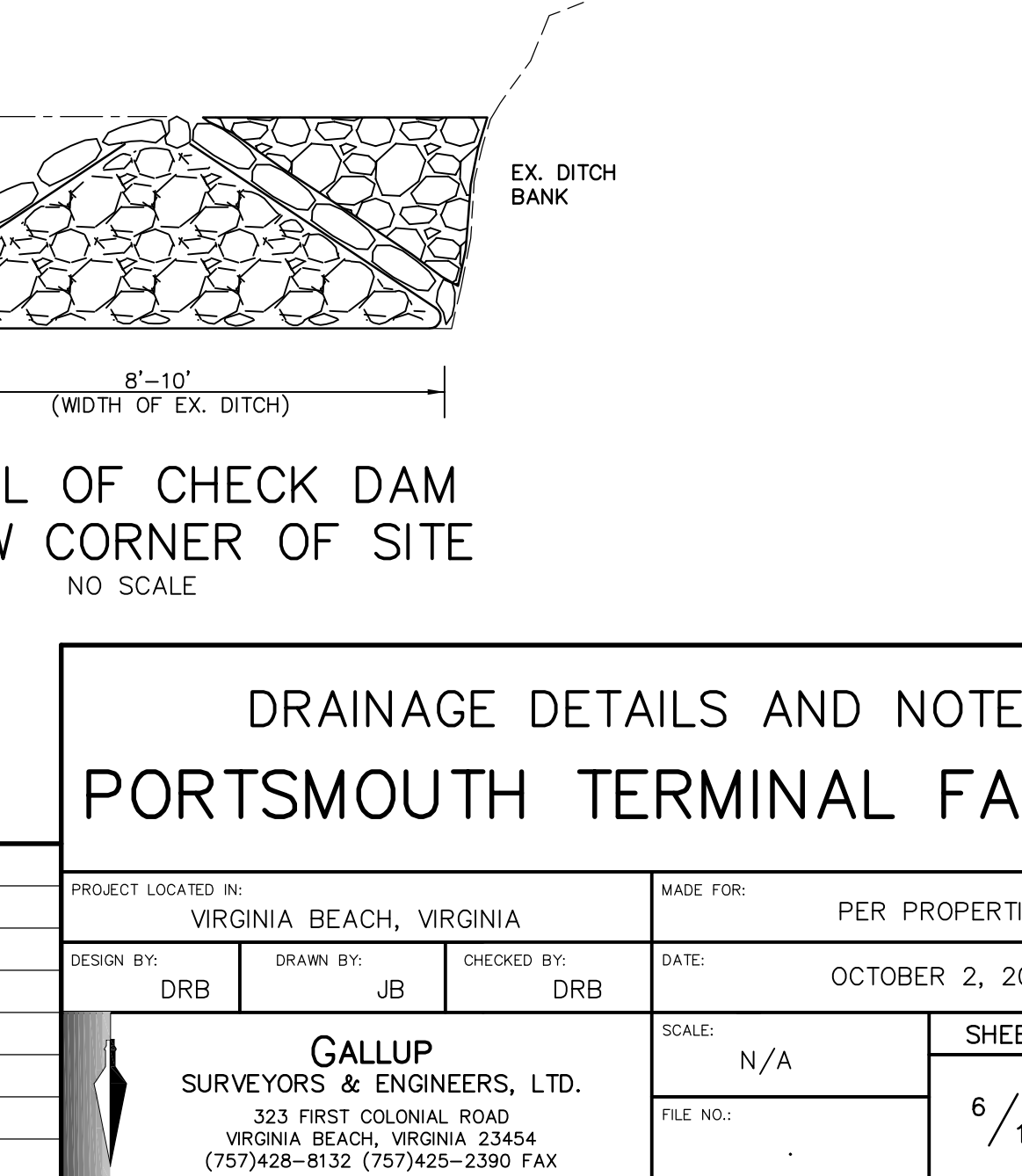
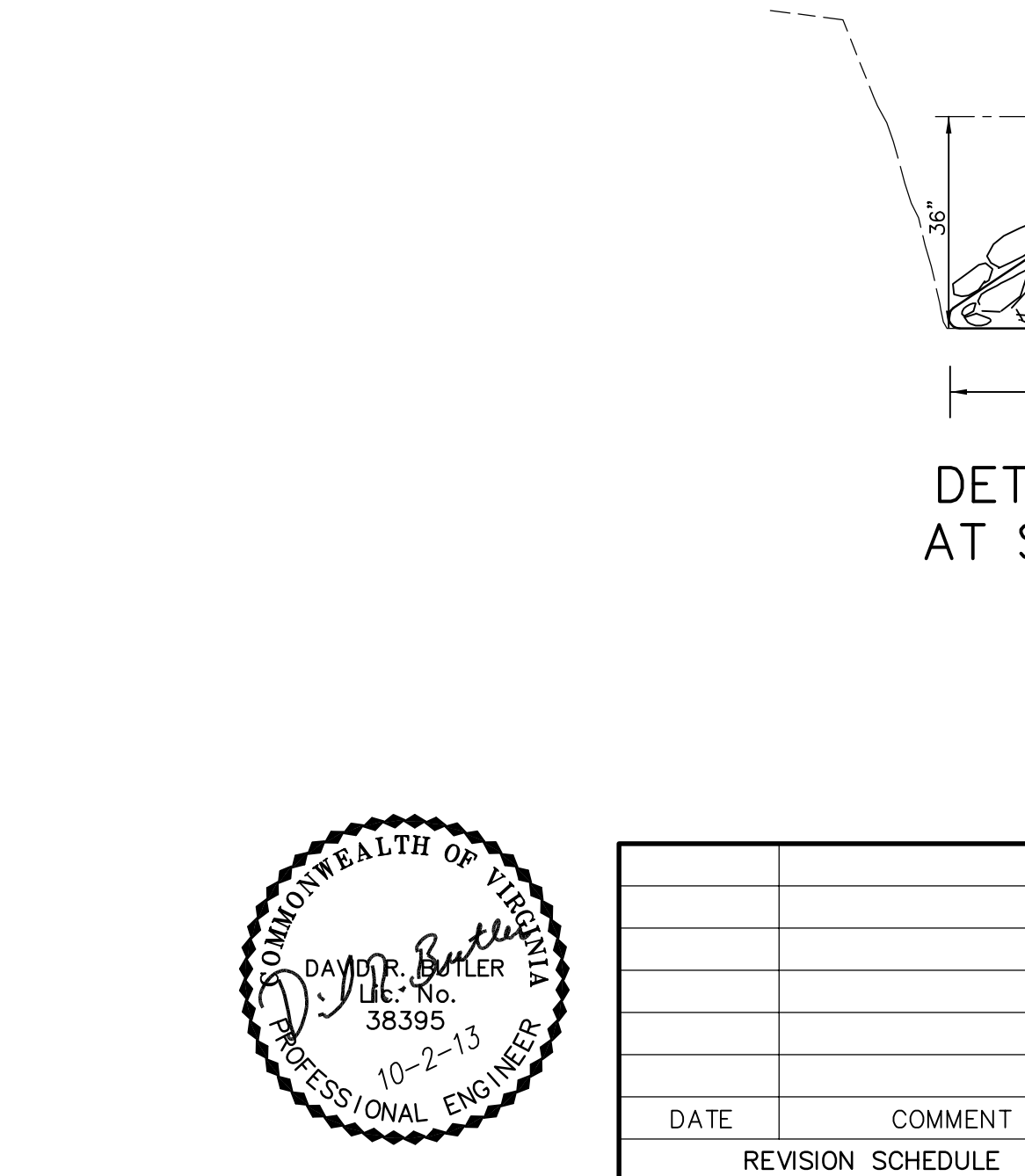
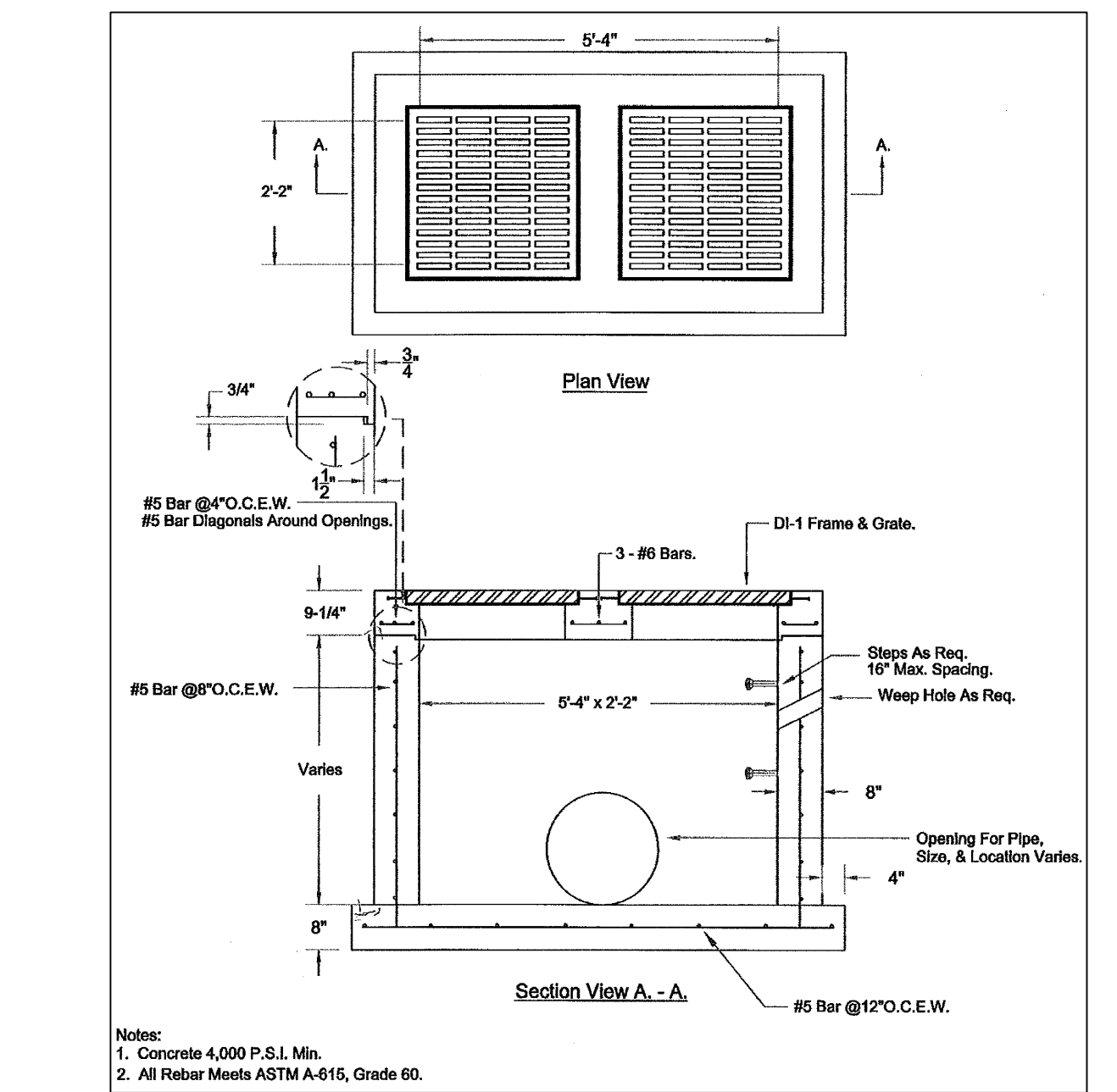
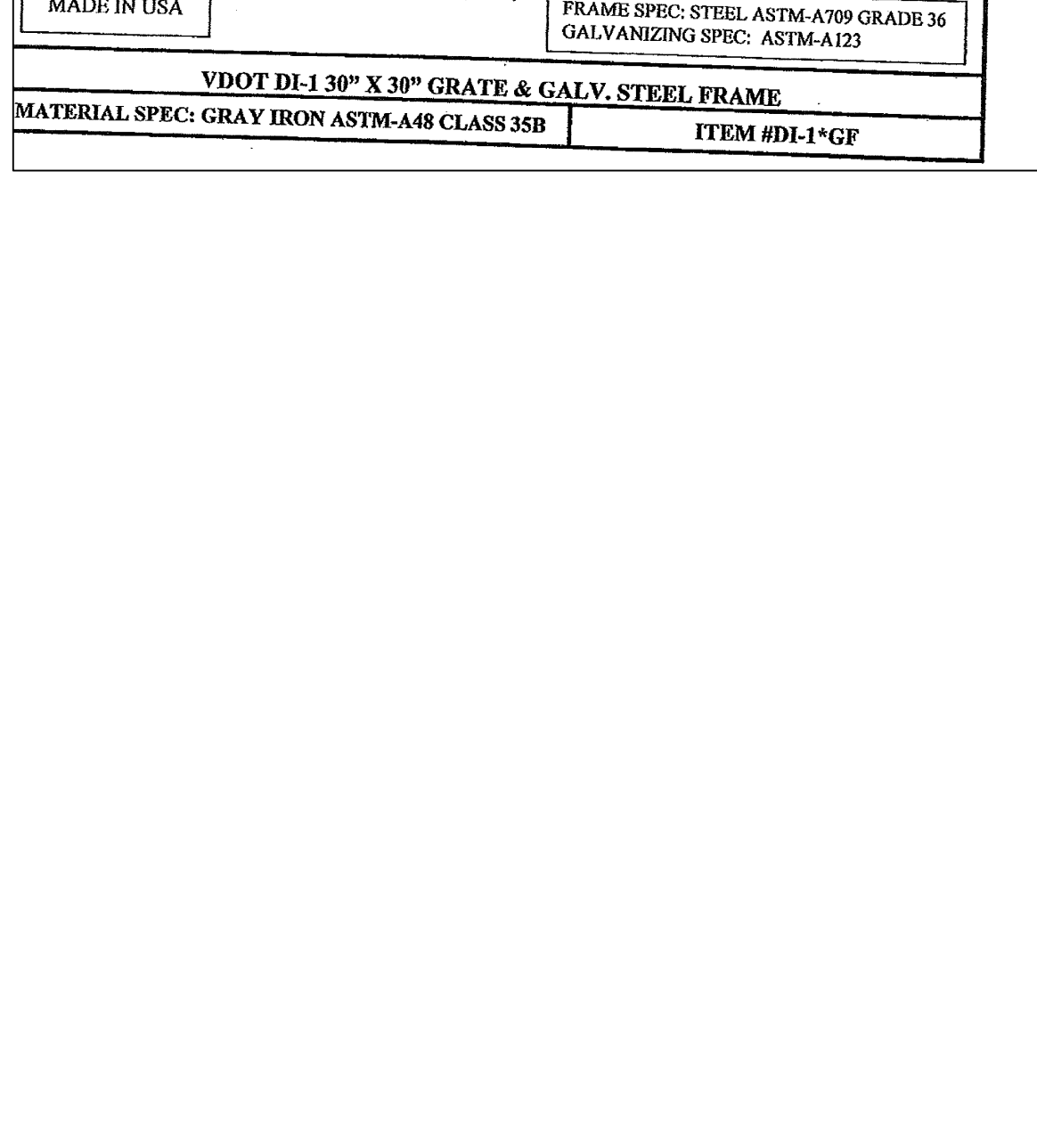
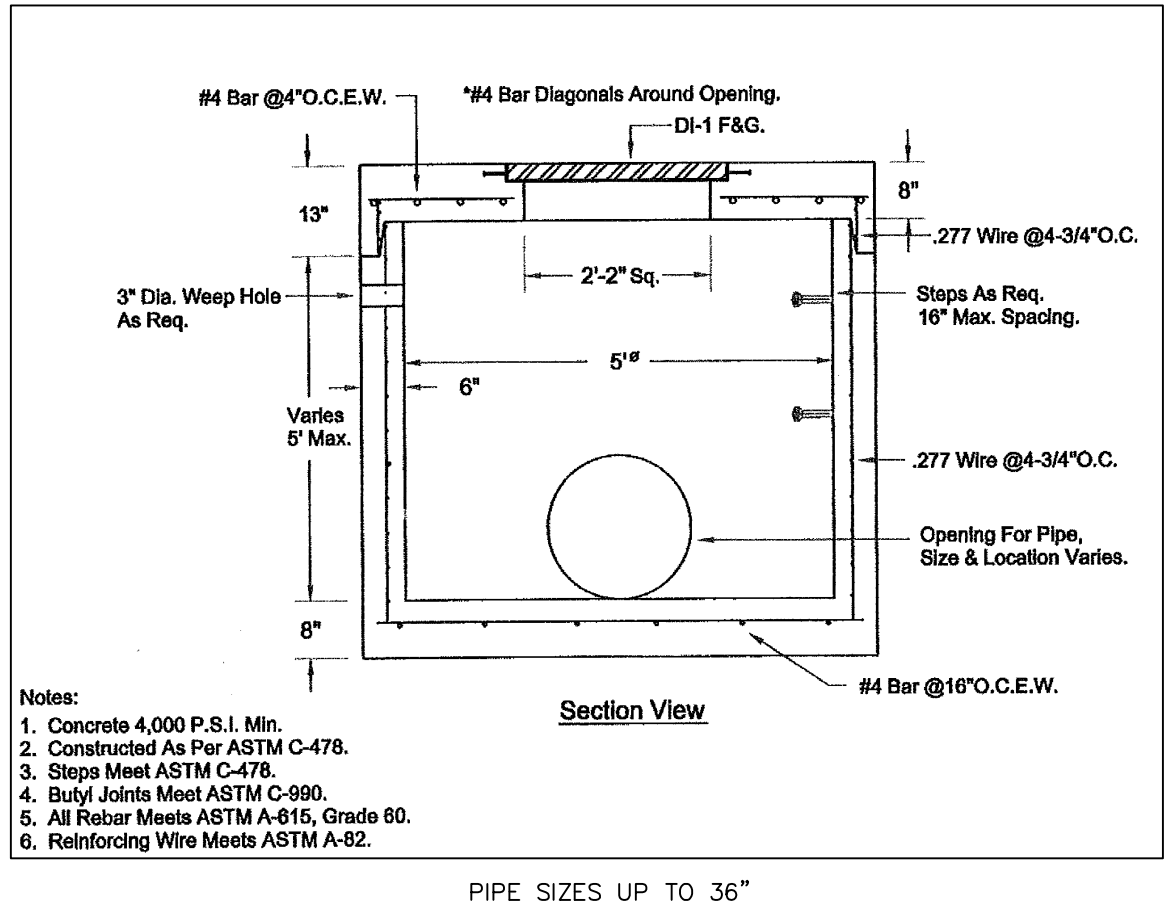
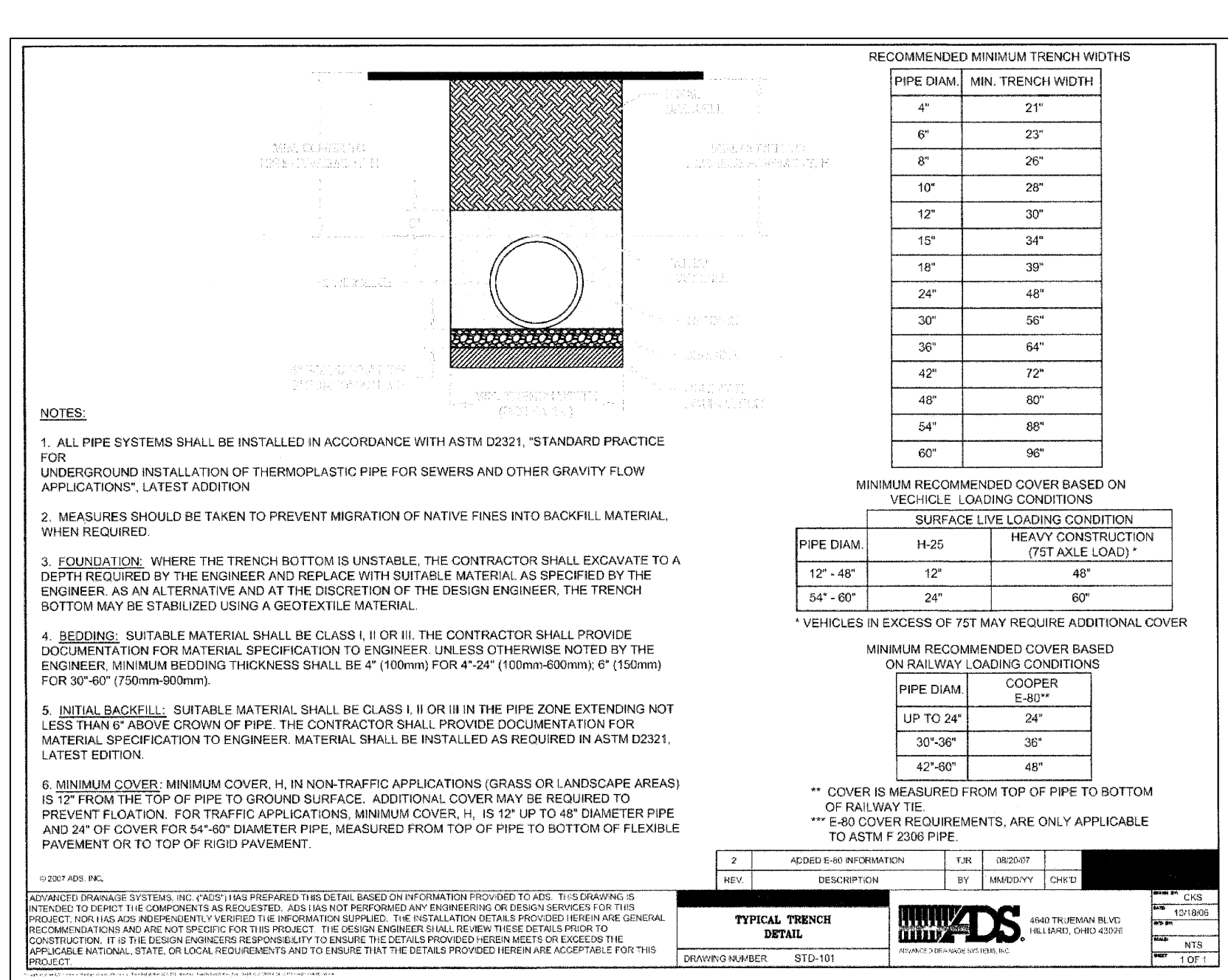
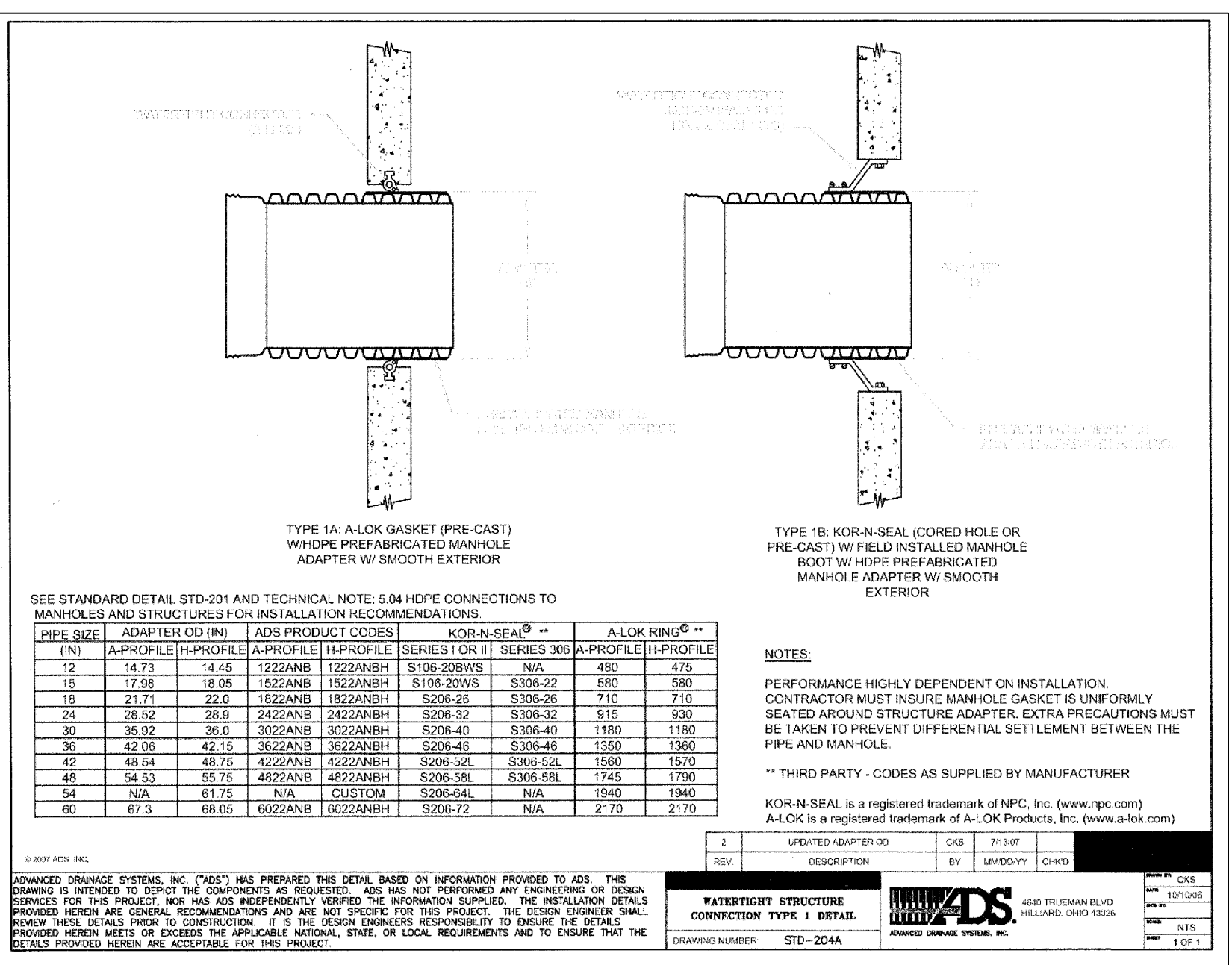
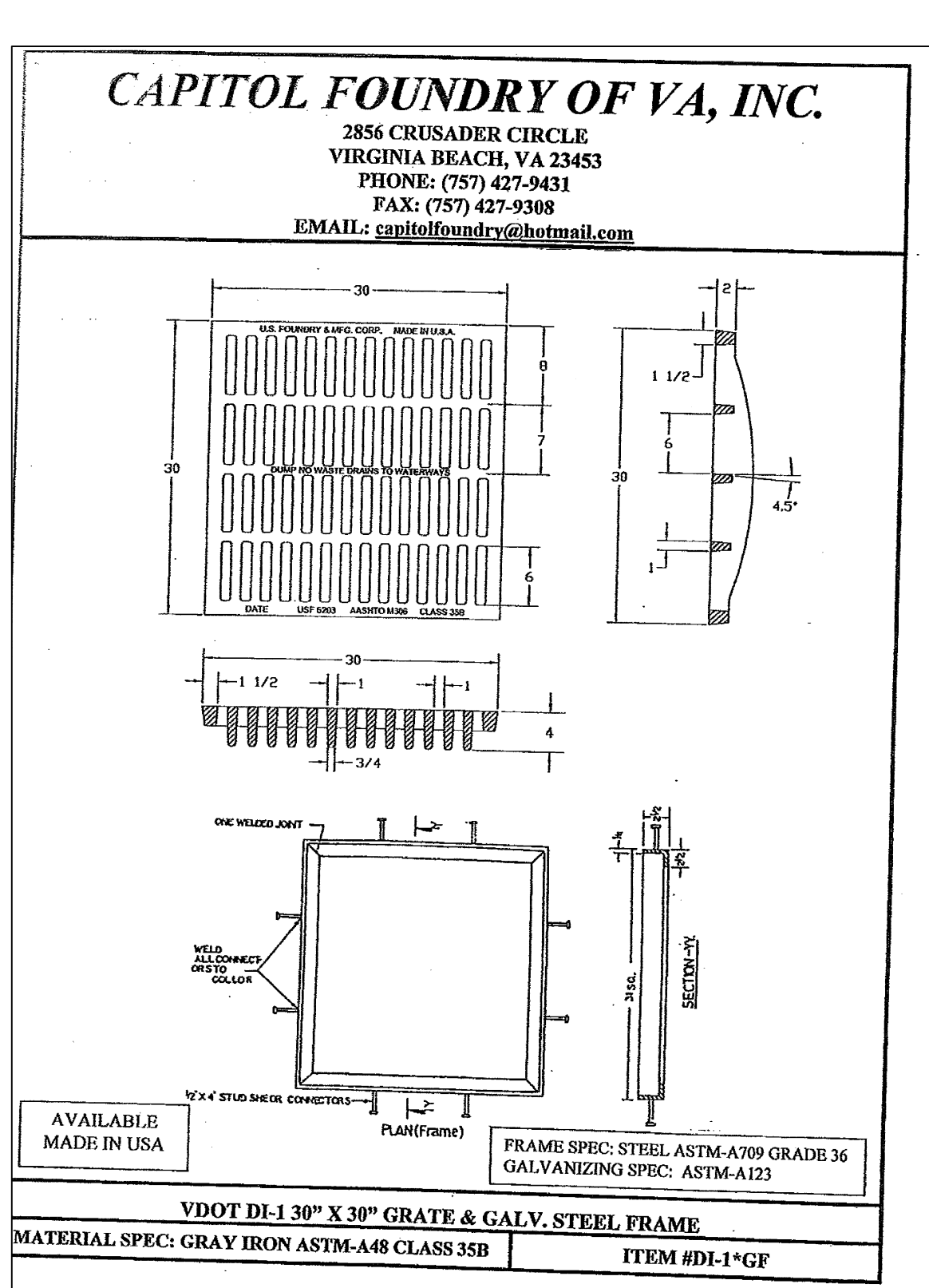
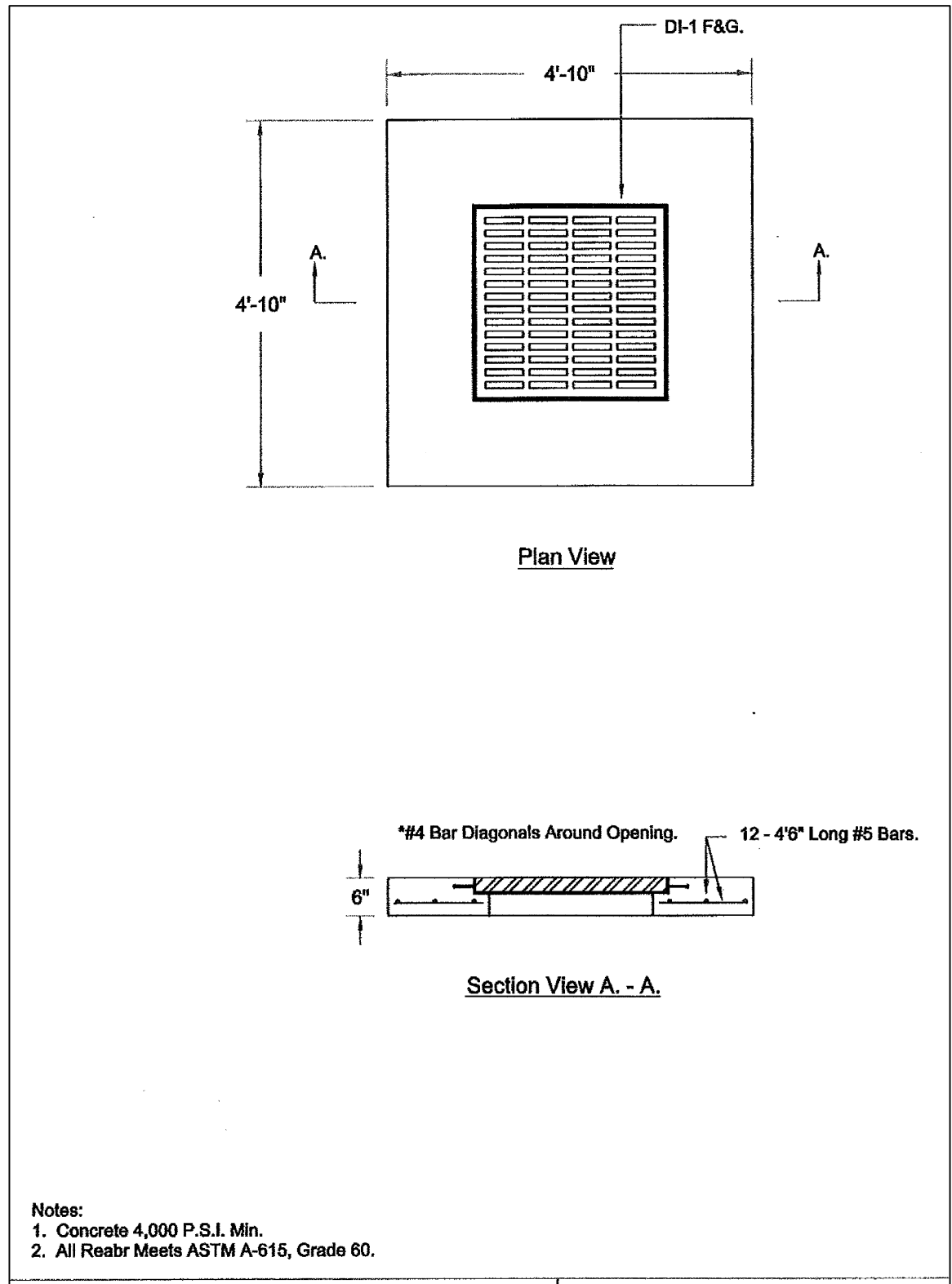
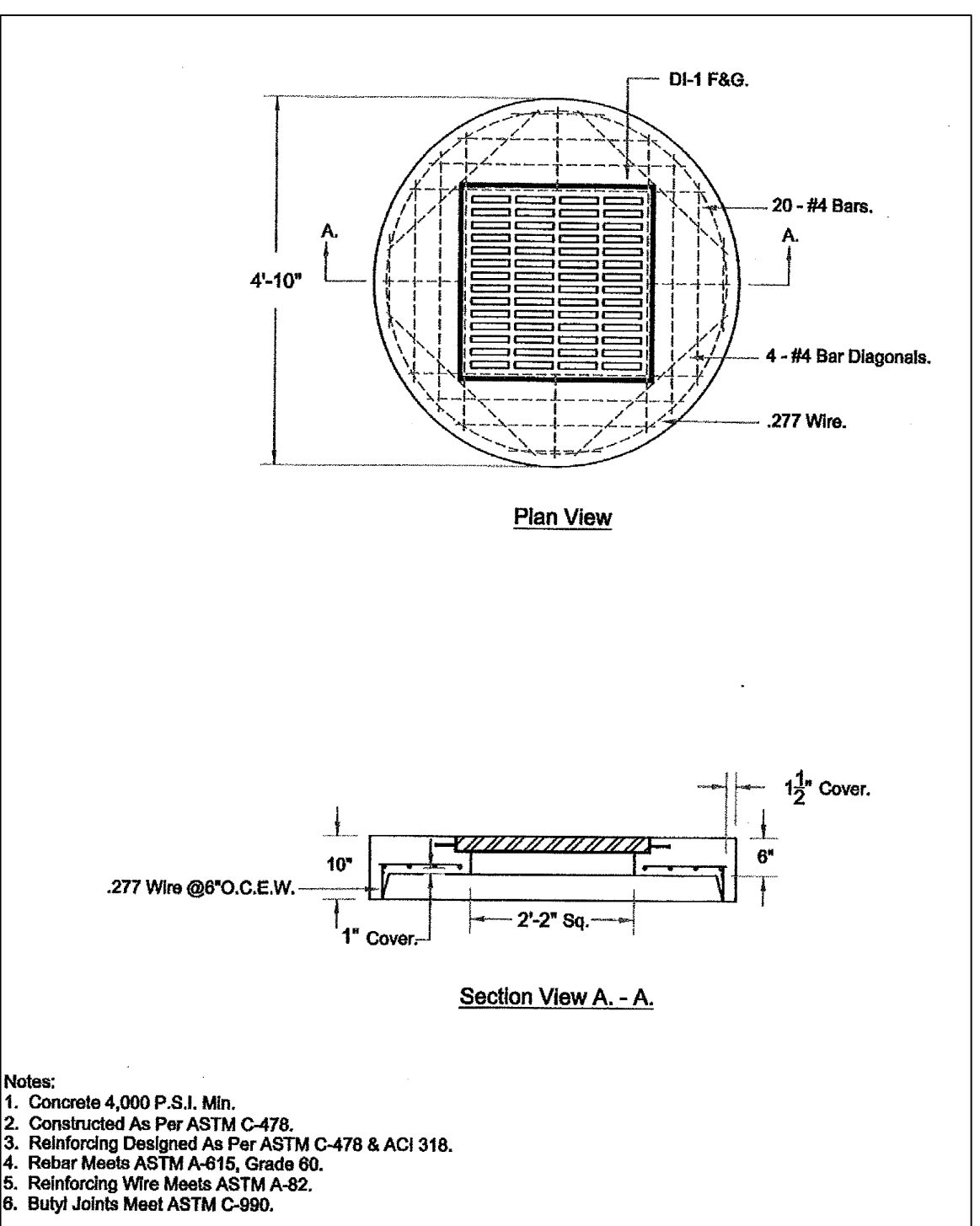
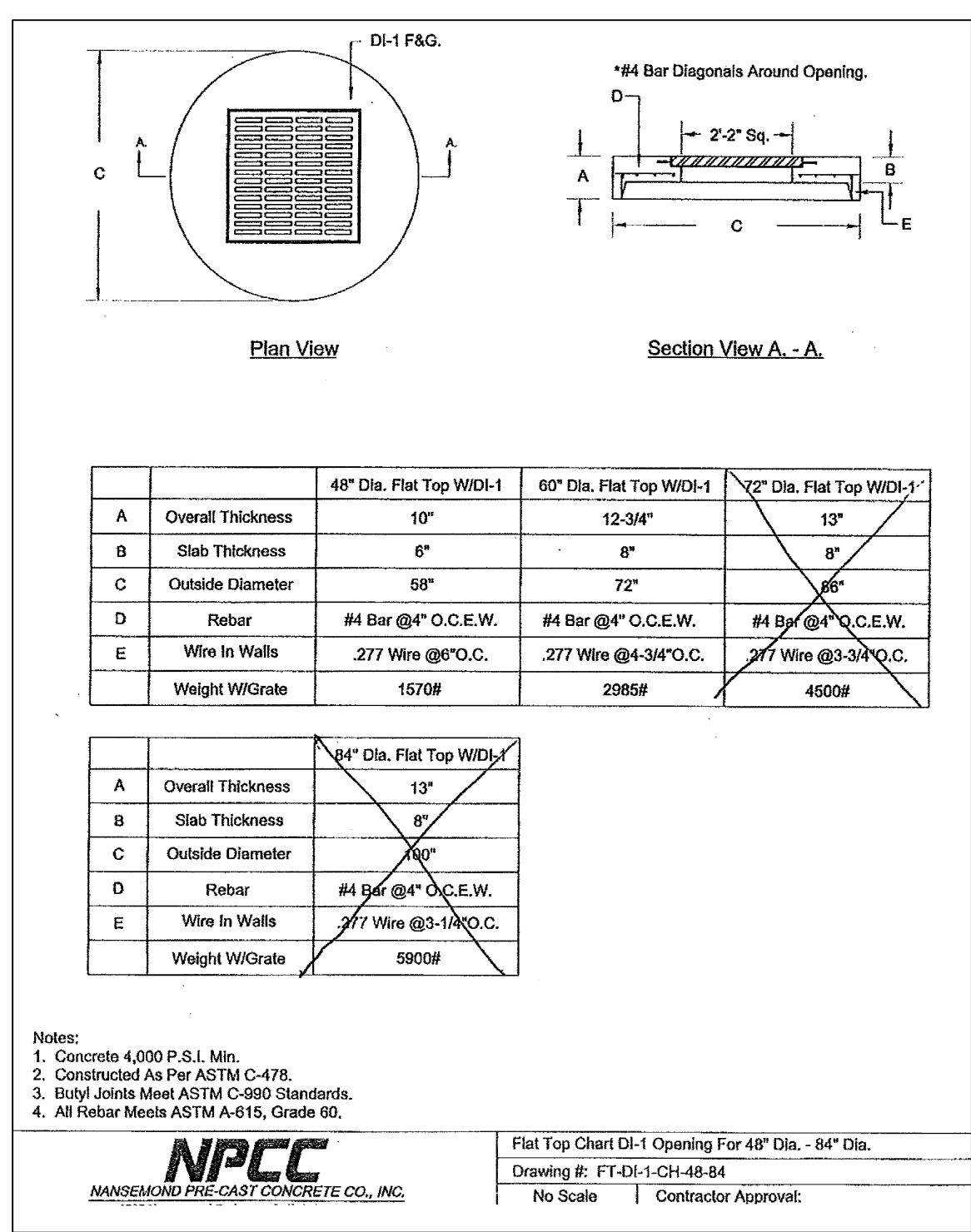
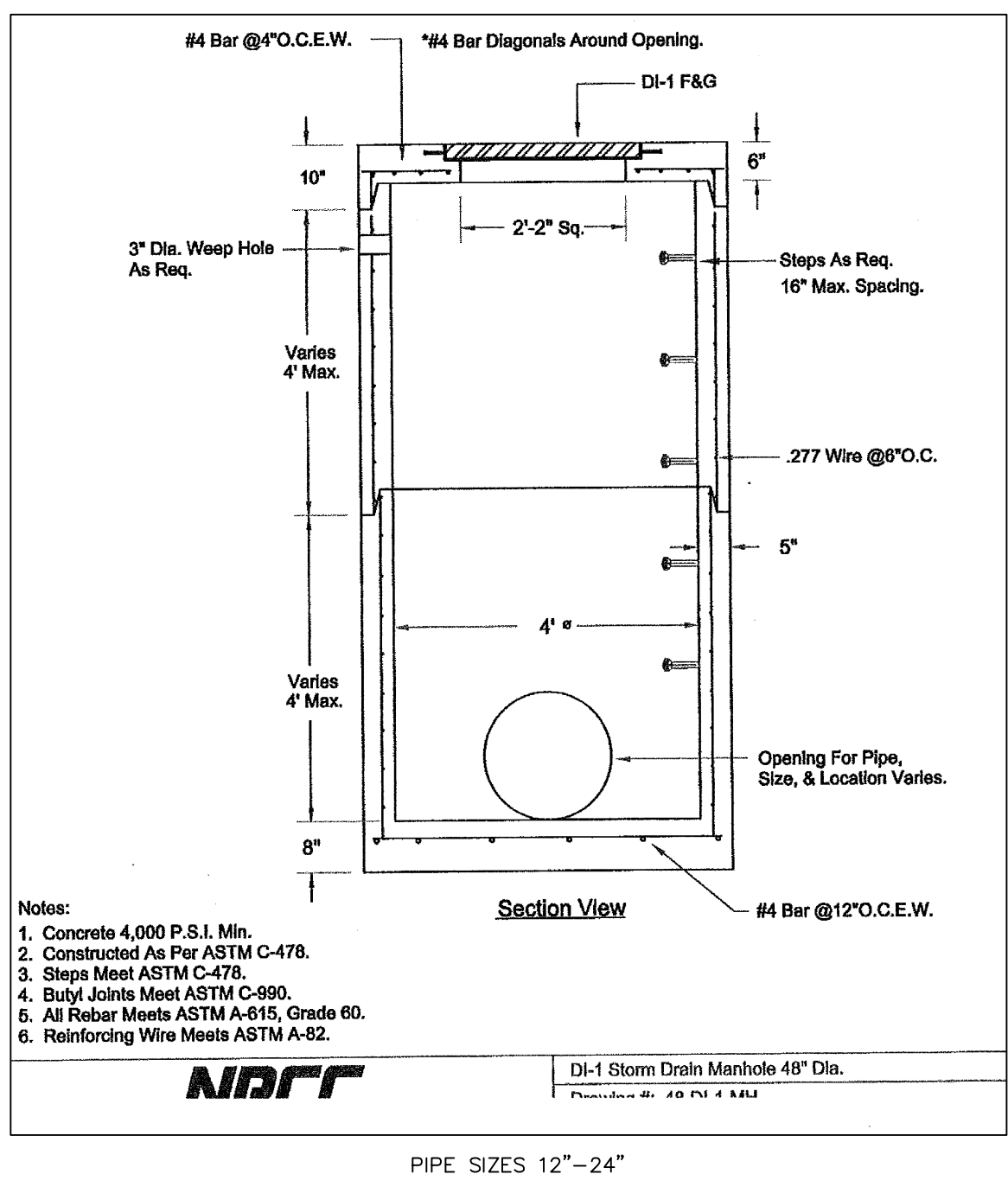
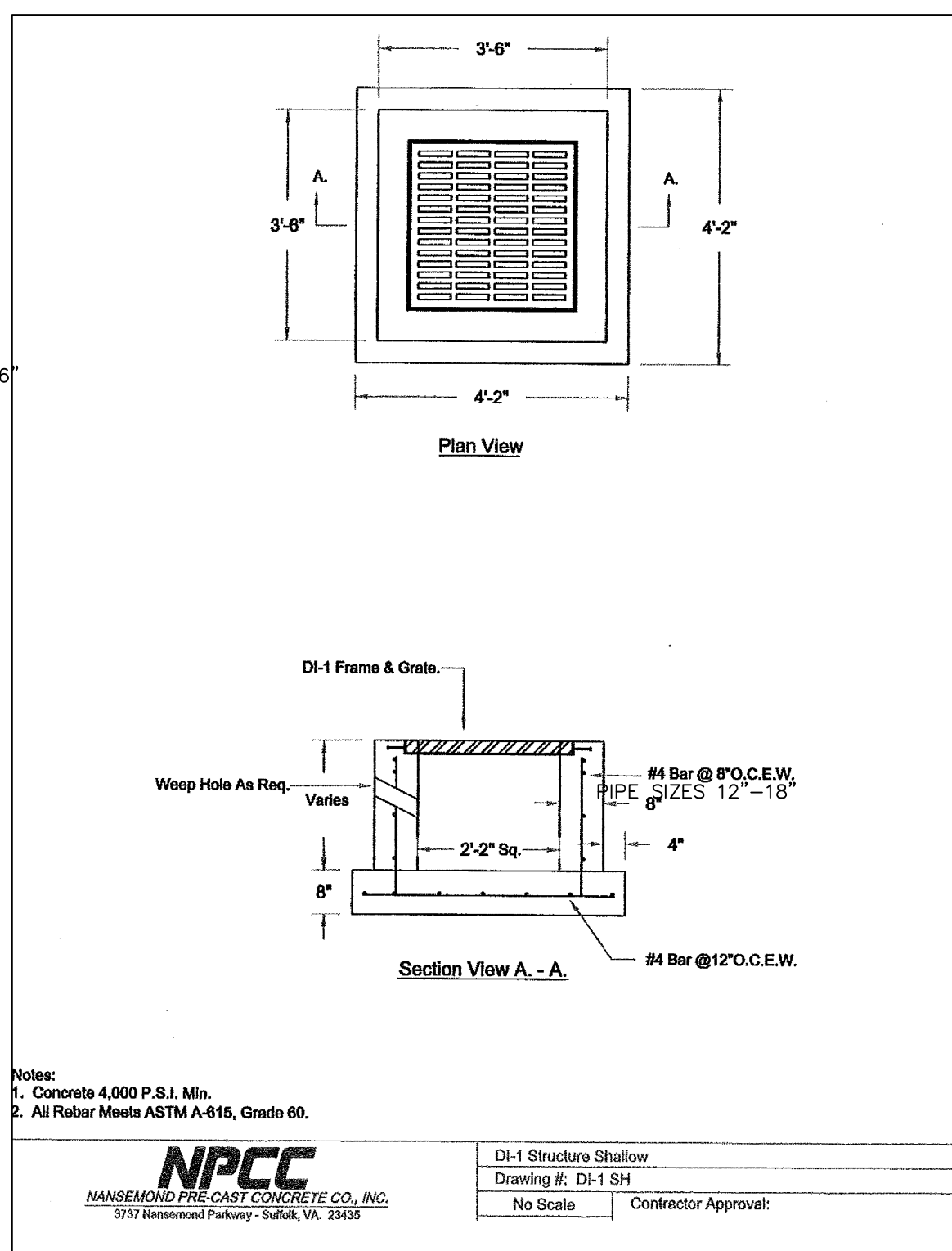
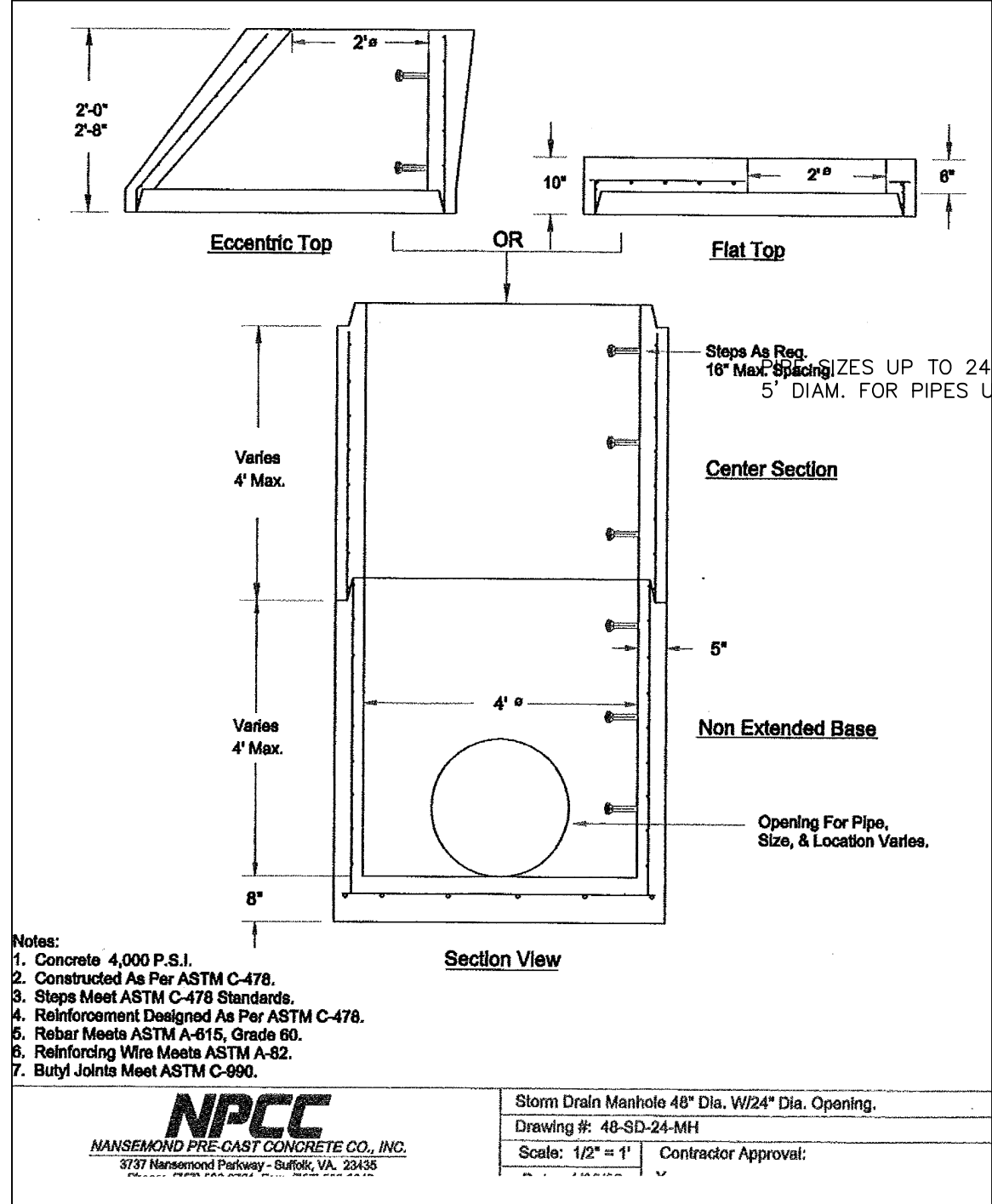
VIRGINIA STATE PLANE  
SOUTH ZONE  
NAD 1983

SOUTHERN BRANCH OF THE  
ELIZABETH RIVER

GRADING PLAN AND UTILITY PLAN			
PORTSMOUTH TERMINAL FACILITY			
PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 30'	SHEET 5/13

C5

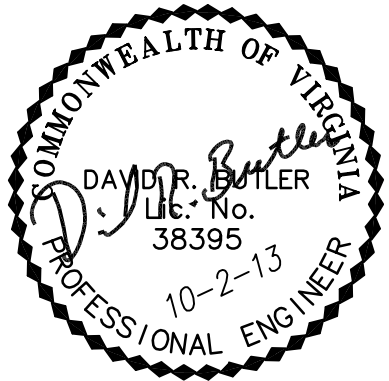




# DRAINAGE DETAILS AND NOTES PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA	MADE FOR: PER PROPERTIES
DESIGN BY: DRB	DRAWN BY: JB
CHECKED BY: DRB	DATE: OCTOBER 2, 2013
SCALE: N/A	SHEET: 6/13
FILE NO.:	C6

GALLUP  
 SURVEYORS & ENGINEERS, LTD.  
 323 FIRST COLONIAL ROAD  
 VIRGINIA BEACH, VIRGINIA 23454  
 (757)428-8132 (757)425-2390 FAX



DATE	COMMENT

REVISION SCHEDULE



CONFIRM SIZE WITH MANUFACTURER PRIOR TO ORDERING

1. EACH SILTSACK SHOULD BE INSPECTED AFTER EVERY MAJOR STORM EVENT
2. IF THERE HAVE BEEN NO MAJOR STORM EVENTS, SILTSACK SHOULD BE INSPECTED EVERY 2-3 WEEKS.
3. THE YELLOW RESTRAINT CORD SHOULD BE VISIBLE AT ALL TIMES. IF THE CORD IS COVERED WITH SEDIMENT, THE SILTSACK SHOULD BE EMPLIED.

### 3.0 Construction Sequence

### 3.1 General

**3.1.1** To install Siltsack in the catch basin, remove the grate and place the sack in the opening. Hold approximately six inches of the sack outside the frame. This is the area of the lifting straps. Replace the grate to hold the sack in place.

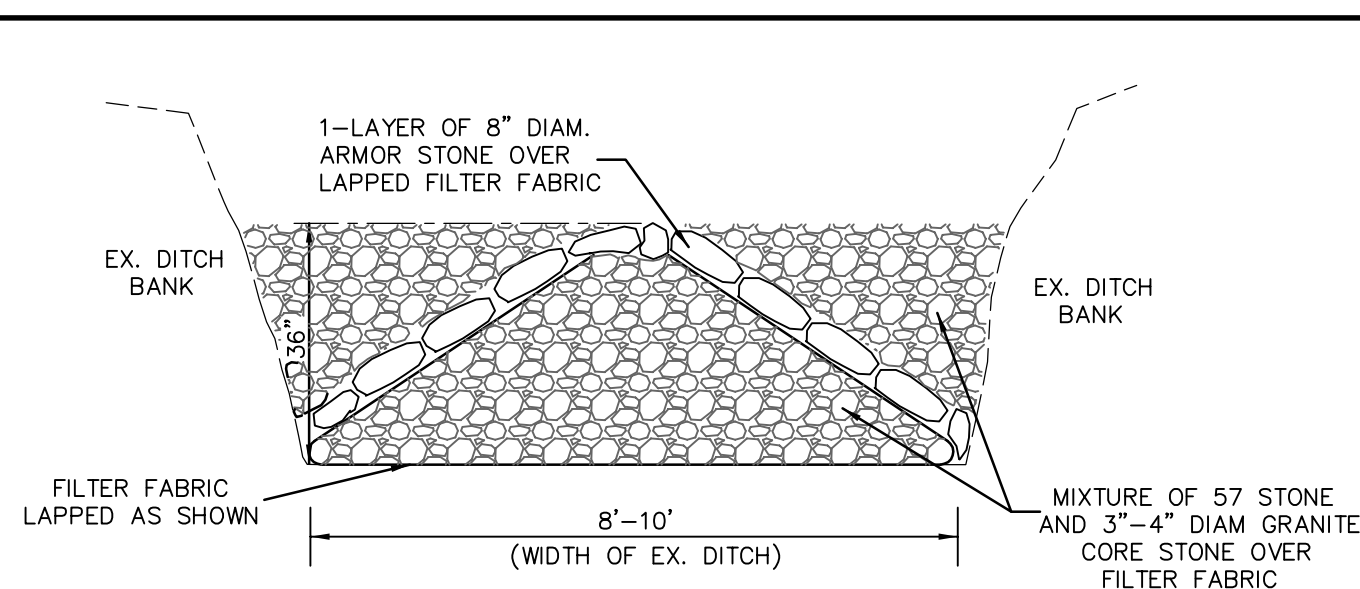
**3.1.2** When the restraint cord is no longer visible, Siltsack is full and should be emptied.

**3.1.3** To remove Siltsack, take two pieces of 1" diameter rebar and place through the lifting loops on each side of the sack to facilitate the lifting of Siltsack.

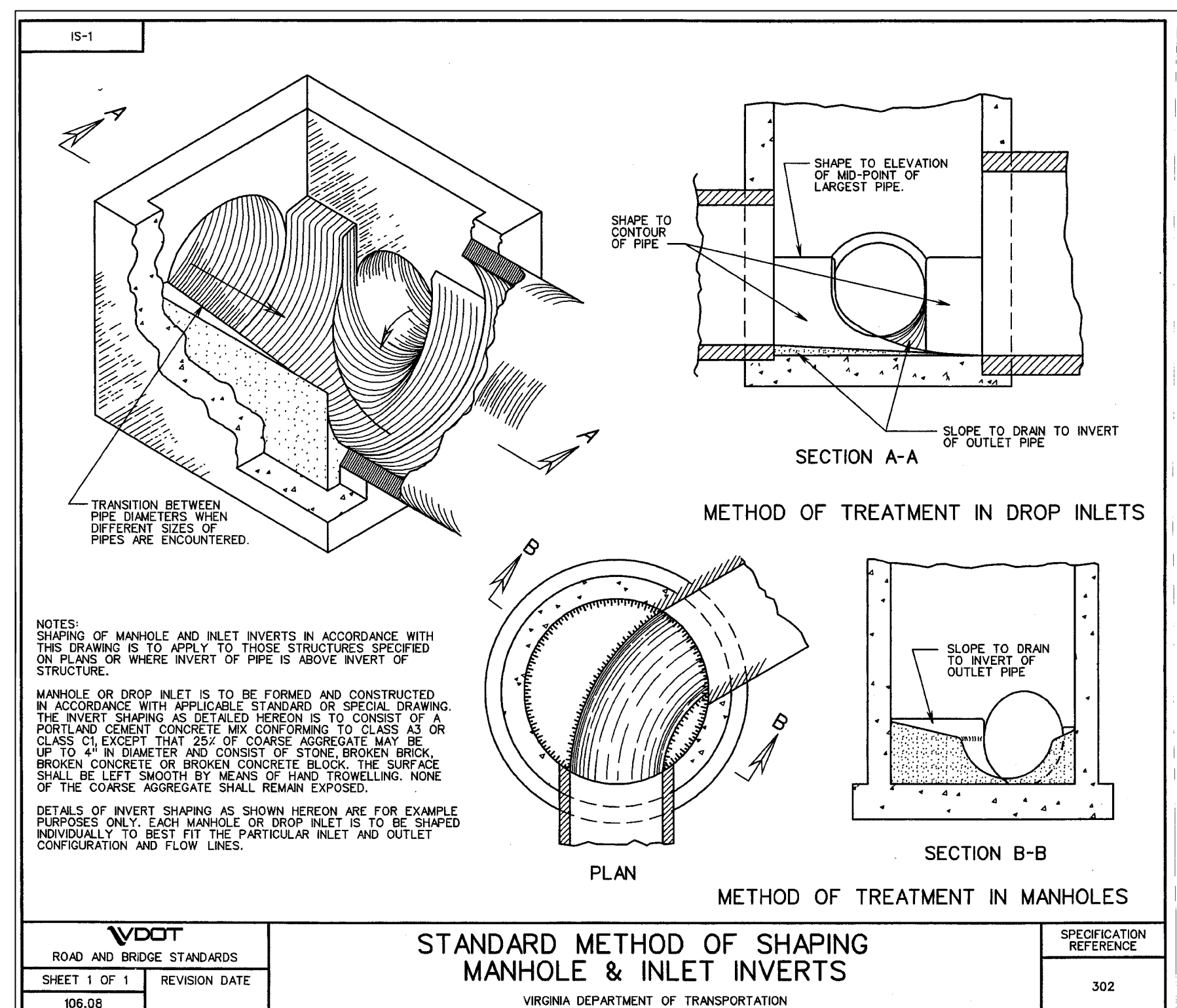
**3.1.4** To empty Siltsack, place unit where the contents will be collected. Place the rebar through the lift straps (connected to the bottom of the sack) and lift. This will lift Siltsack from the bottom and empty the contents. Clean out and rinse. Return Siltsack to its original shape and place back in the basin.

**3.1.5** Siltsack is reusable. Once the construction cycle is complete, remove Siltsack from the basin and clean. Siltsack should be stored out of sunlight until next use.

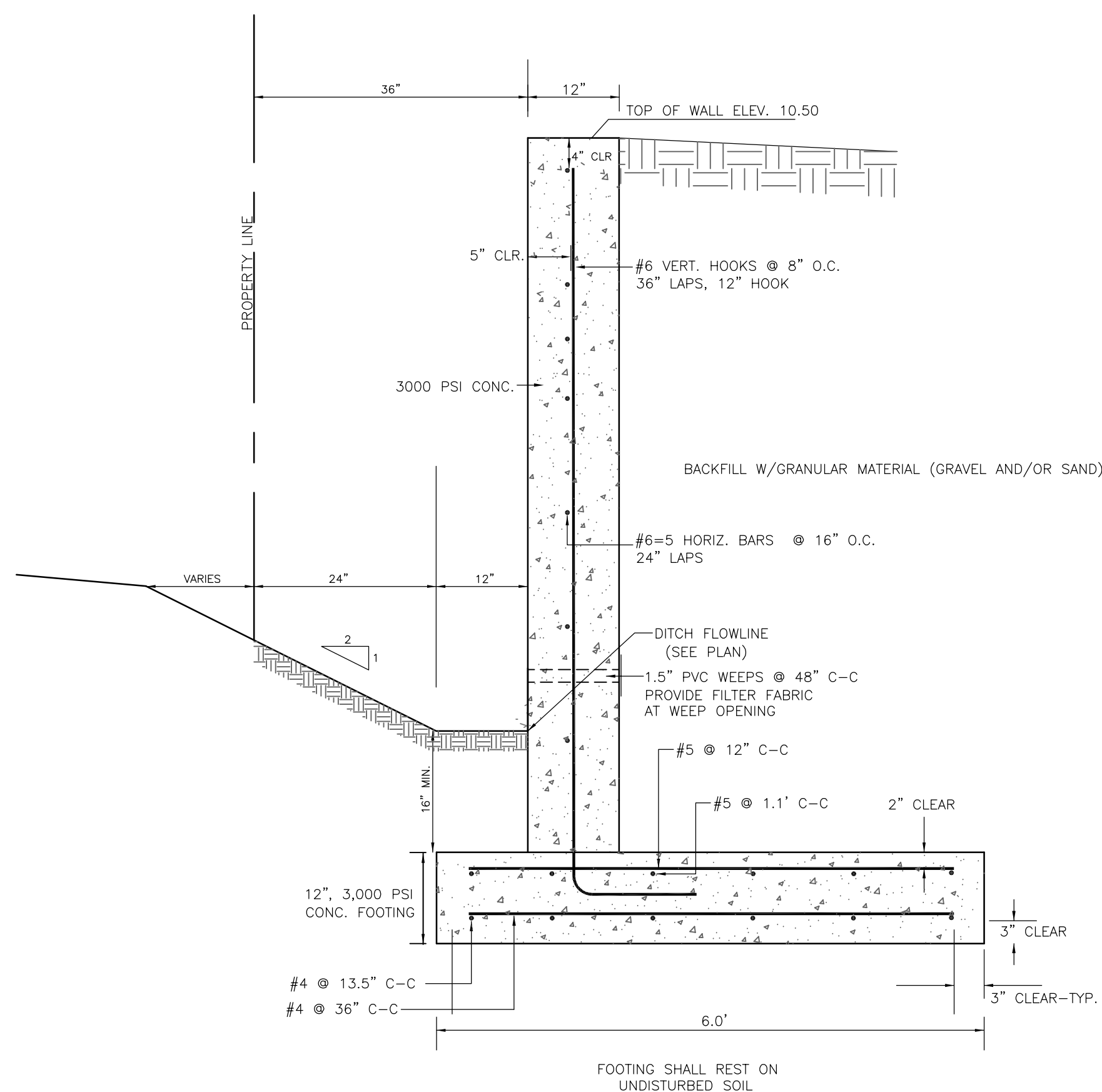
THE SILT SACK PRODUCT SHOWN ON THIS SHEET  
TO BE USED IN ALL STORM DRAIN INLETS AND IS TO REMAIN  
PERMANENT FOR DRAINAGE STRUCTURES 12-22



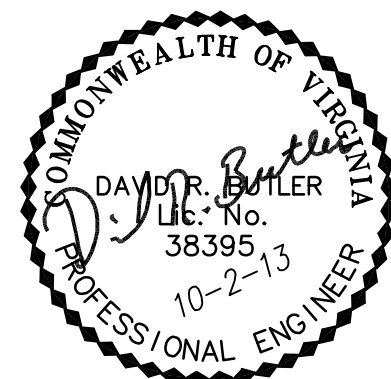
CHECK DAM AT SW CORNER  
OF BOUNDARY  
(NO SCALE)




ALL DRAINAGE STRUCTURES ARE TO RECEIVE INLET  
SHAPING WITH THE EXCEPTION OF STRUCTURES 12-22.



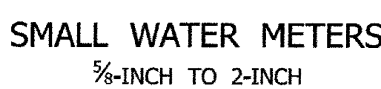
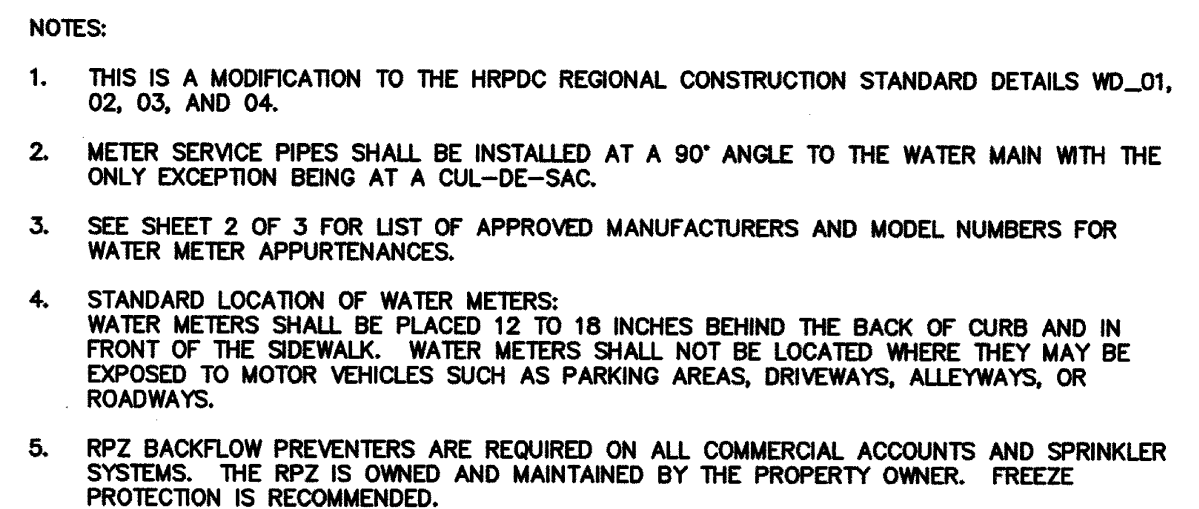
TYPICAL SECTION ALONG WEST  
PROPERTY LINE  
(NO SCALE)



DATE	COMMENT
REVISION SCHEDULE	

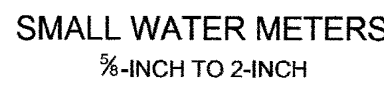
PROJECT LOCATED IN:			MADE FOR:	
VIRGINIA BEACH, VIRGINIA			PER PROPERTIES	
DESIGN BY:	DRAWN BY:	CHECKED BY:	DATE:	
DRB	JB	DRB	OCTOBER 2, 2013	
 <b>GALLUP</b> <b>SURVEYS &amp; ENGINEERS, LTD.</b> 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23464 (757) 425-8132 (757) 425-2580 FAX			SCALE:	SHEET
			N/A	
			FILE NO.:	9/13



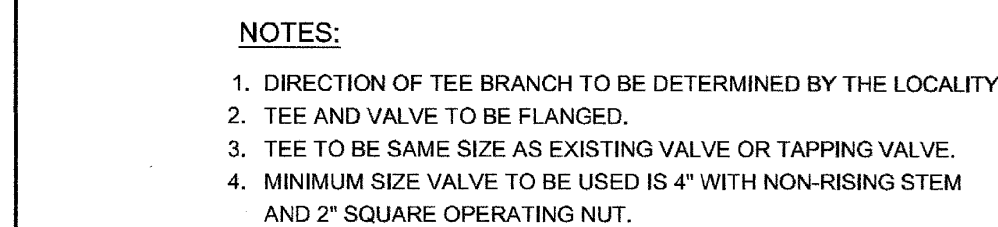


Date : 1/10/07	Revised :
Scale : N.T.S.	
Sheet No. : 1 of 3	
Detail No. : WD-01	

APPURTENANCES	METER SIZE (In.)				
	%	%	1	1 1/2	2
Corporation Stop Criteria	Corporation Stop shall have nominal sized ball valve, AWWA taper thread inlet, and pack joint for type K copper outlet.				
Corporation Size (In.)	%		1	1 1/2	2
A.Y. McDonald Ford Mueller	4071B-22 FB1000 P-2500B		4071B-22 FB1000 P-2500B	4701B-22 FB1000 P-2500B	4701B-22 FB1000 P-2500B
	Tea Head adapter shall be provided.				
Tapping Criteria for Ductile Iron and Cast Iron Pipe	% and 1-inch direct tapping.		1 1/2 and 2-inch taps shall include a full circle stainless steel clamp. The clamp shall have stainless steel studs, bolts and nuts, plus a full circle tap gasket.		
Ford Romac Smith-Blair			FS 1 or 2 SS1 264 or 265	FS 1 or 2 SS2 264 or 265	
Tapping Criteria for 2-inch HDPE Pipe	% and 1-inch taps shall include a gasketed bronze saddle with bronze or stainless steel hardware.		1 1/2 and 2-inch taps shall not be made on 2-inch HDPE		
Ford Mueller A.Y. McDonald	S70 S-13000 3891		S70 S-13000 3891		
Copper	Nominal size type K copper				
Meter Sitter Criteria	Copper setter shall be horizontal with nominal sized setter valve, inlets and outlets. Setter depth shall be 12-inches. Setter shall fit displacement meter.				
Meter Length (In.)	7.5	9	10.75	13	17
Inlet and Outlet Connections	Setter inlet pack joint and outlet pipe thread. Meter inlet and outlet pipe thread.			Setter inlet pack joint and outlet pipe thread. Meter inlet and outlet shall be AWWA range.	
A.Y. McDonald Ford Mueller	26-12MX23D3 VB71-11/2 HP1578		26-412W2GD44 VB72-44-33 HP15751	26-612W2NF-66 VB7672-12-11/66 HP-1422-2	26-712W2NF-37 VB7772-12-11/66 HP-1422-00
Meter Box Criteria	PVC Box with PVC Cover 20.6-inches x 11.35-inches			PVC Box with Cast Iron Cover 30-inches x 18-inches	
Saurtheastern Distributors, Inc.	Cover Box 190	189-Sensu			Cover Box MSBC-1730-R MSBC-1730-18
Carson Industries					
NOTES:					
1.	Each 1 or 2-inch meter connection requires full time City inspection.				
2.	Service pipeline shall be jointless from corporation stop to meter setter.				
3.	Service pipeline size shall only be changed at the inlet to the meter setter, and the changed size is only allowed with a standard brass reducer.				



Date: 1/10/07	Revised: 3/28/07
Scale: N.T.S.	4/23/12
Sheet No. : 2 of 3	
Detail No. : WD-02	



FORCE MAIN CONNECTION  
TO H.R.S.D. FORCE MAIN

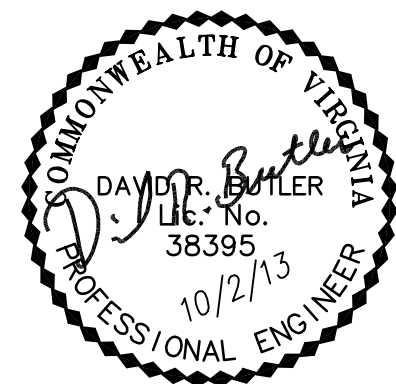
NOT TO SCALE

REFERENCE 200.803	CATEGORY SANITARY SYSTEMS	DATE 12/10	SHEET No. 1 OF 1	DETAIL No. SS 18
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1. All materials and construction methods shall conform to the Hampton Roads Planning District Commission (HRPDC) Regional Standards, fifth edition, as amended by the City of Portsmouth Special Provisions and any other applicable City Ordinance or Code.
2. The Contractor is responsible for locating all public or private utilities, which lie in the construction area prior to any excavation or construction. Any changes to the proposed utility alignments shall be approved by the Engineer. The Contractor shall be responsible for the repair, at his expense, of all existing utilities damaged during construction
3. The Contractor shall use only approved material in the backfill of utility trenches.
4. All utility trenches shall be backfilled and compacted to within .33' of final subgrade elevation and graded to drain. Excess material shall be removed at the Contractor's expense. All finished slopes in utility easements or in right-of-way not subject to paving shall be topsoiled and seeded in accordance with current HRPDC and City of Portsmouth specifications and shall not exceed the maximum as follows - cut slope 4:1, fill slope 4:1.
5. The Contractor shall provide temporary drainage to relieve areas that may cause damage to the roadways, and erosion protection during construction as directed by the City of Portsmouth, the HRPDC Regional Standards, and Virginia Erosion and Sediment Control Handbook.
6. All concrete shall be class "AS" air entrained (3,000 psi) unless noted otherwise.
7. All storm sewer pipe shall be as specified on the plan sheets and shall conform to current HRPDC and City of Portsmouth Standards. All pipes shall be reinforced concrete tongue and groove.
8. Prior to construction or excavation, the contractor shall call "Miss Utility" at 1-800-552-7001. In addition, the contractor shall call the offices of any and all public or private utilities and request location of utilities that may exist and cross through the construction area, whether or not said utilities are shown on the plans. Utility companies shall be notified 48 hours in advance of any excavation in the proximity of their utilities. The contractor is responsible for the repair, at his expense, for any damage caused to utilities during construction.
9. All storm sewer pipes, drop inlets and catch basins shall be cleaned of debris and eroding material during the last stage of construction.
10. Gutterbody, or approved equal, inlet filter shall be placed around all existing and proposed drainage inlets.
11. Any defective, faulty, cracked, or broken valves, driveways, handicapped ramps or curb and gutter, as determined by the Engineer, shall be removed and replaced to the nearest joint prior to final acceptance at no additional expense to the City. Patching is not acceptable.

12. Any items or instructions, which are noted on the plans but are not included in the Bid Price Schedule shall not be paid for separately, but shall be included in other bid items. Frames and covers for sewer manholes and drainage structures shall be by Capital Foundry, Dewey Brothers, or approved equal.
13. All curb and walks to be removed shall be taken out to the nearest joint. All new walk limits shall be determined in the field and approved by the Engineer.
14. Relocation, removal and/or replacement of all signs shall be coordinated with the Department of Traffic Engineering.
15. All conflicting private utilities, lines and poles will be relocated by others.
16. Contractor shall remove and reset all mailboxes as required (non pay item).
17. All concrete drives shall be 7" thick minimum from roadway to the right-of-way. Concrete drives extending past the right-of-way shall be 4" thick minimum (See Plans for locations).
18. Contractor is responsible for coordinating closure of driveways with individual property owners and must provide access to the houses.
19. Contractor shall protect all trees and shrubs as directed by the Engineer.
20. Removal of existing utilities in same trench as proposed utilities shall not be a pay item.
21. All utility and storm drain lines must be inspected by the Engineering Department prior to backfilling.
22. Disposal of excess material within the City of Portsmouth shall require prior approval from the Engineer. Prior to construction within any existing public right-of-way the contractor shall obtain a permit from the Engineering Department, City of Portsmouth, Virginia. A copy of the approved traffic control plan is to be submitted with the right-of-way permit application.
23. The contractor shall be responsible for replacing with matching materials any pavement, driveways, walks, curbs, etc., that must be cut or that are damaged during construction.
24. When materials which are unsuitable for foundations, subgrades, or other roadway purposes occur within the limits of street construction, the contractor shall be required to excavate such materials below the grade shown on plans and the areas so excavated shall be back filled with approved suitable materials. The extent of undercutting and backfilling to be determined by the Engineering Division, City of Portsmouth, Virginia.
25. Replacement of pavement shall be in accordance with standard pavement patching details (STD. Drawing 7.1. or 7.2) Specifications and standards for the Department of Public Works, or in accordance with the right-of-way permit specifications, Engineering Department, City of Portsmouth, Virginia.

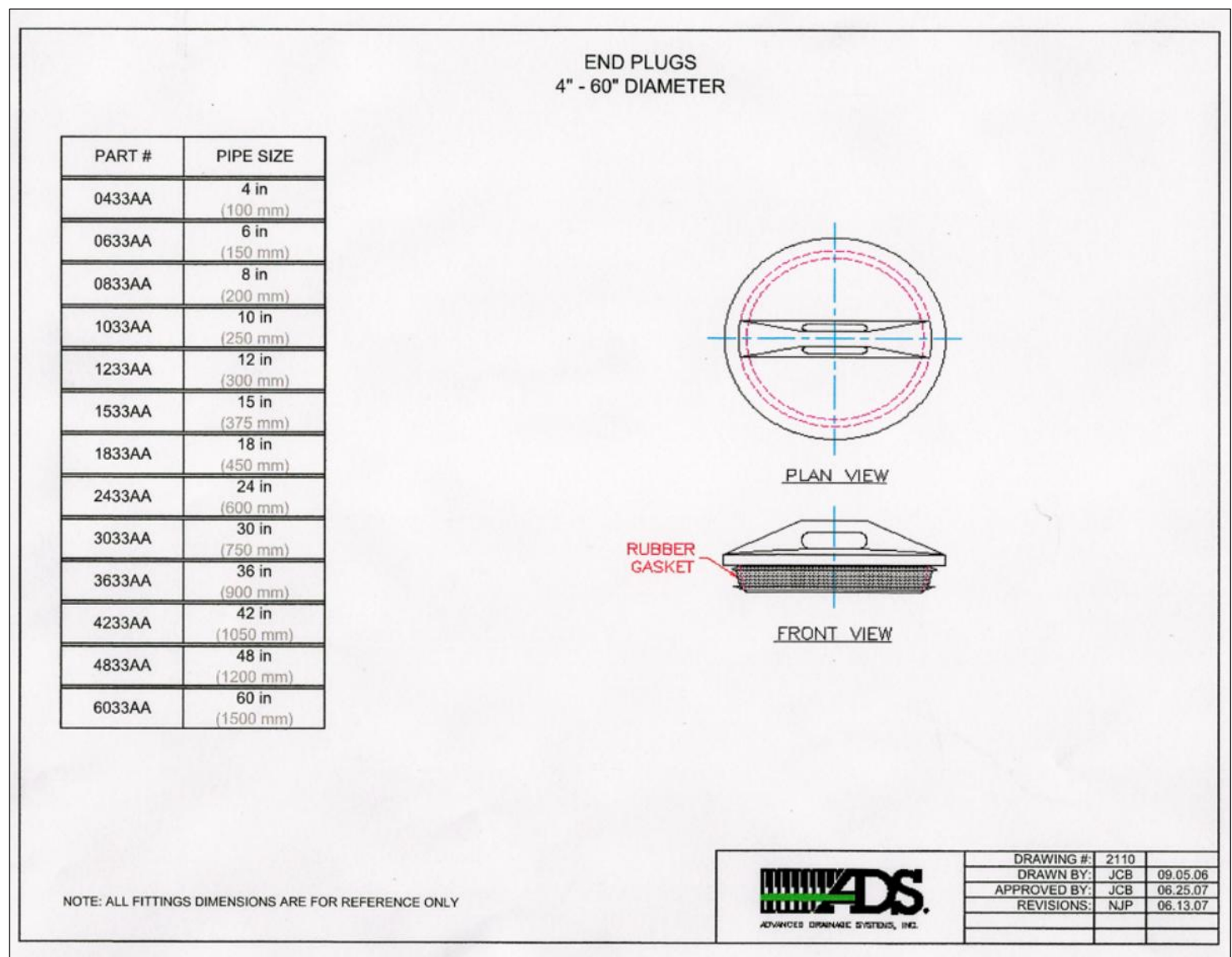
1. Maximum allowable slopes on driveways shall be 12:1. Driveways shall be placed to nearest joint. Contractor to verify limits of all drives with the Engineer.
2. Preserve all power poles not in conflict. Coordinate relocation of conflicting power poles with the Engineer and company. Cost of utility pole relocations shall be by utility owner.
3. All drives shall be concrete in the R.O.W.
4. There shall be a minimum of six inches between adjacent driveway entrance aprons as measured at the curb.
5. Removal and replacement of gravel drives and tie-ins at the edge of aprons is the responsibility of the contractor. Coordinate limits of work with the Engineer. Drives shall be a minimum of 4" gravel beyond existing R.O.W. (see plans for locations).
6. All water meters and sanitary sewer cleanouts must be set behind the curb within the City right-of-way.
7. Coordinate replacement of outdated meters with the Engineer and the City Public Utilities Department.
8. All fence removal and replacement shall be coordinated by the Engineer and homeowner.
9. The Contractor shall adjust the tie-in length for new walks to accommodate steps as directed by the Engineer.
10. The Contractor shall remove and replace curb and gutter as necessary to complete utility work. Curb and gutter shall be replaced in 10 foot sections. The cost of replacing this curb and gutter will not be measured separate for payment and will be included in the respective utility pay item.
11. All items of work required by the documents to complete the project, but not specifically included in a pay item shall be considered an incidental item in accordance with Specification Section 109.



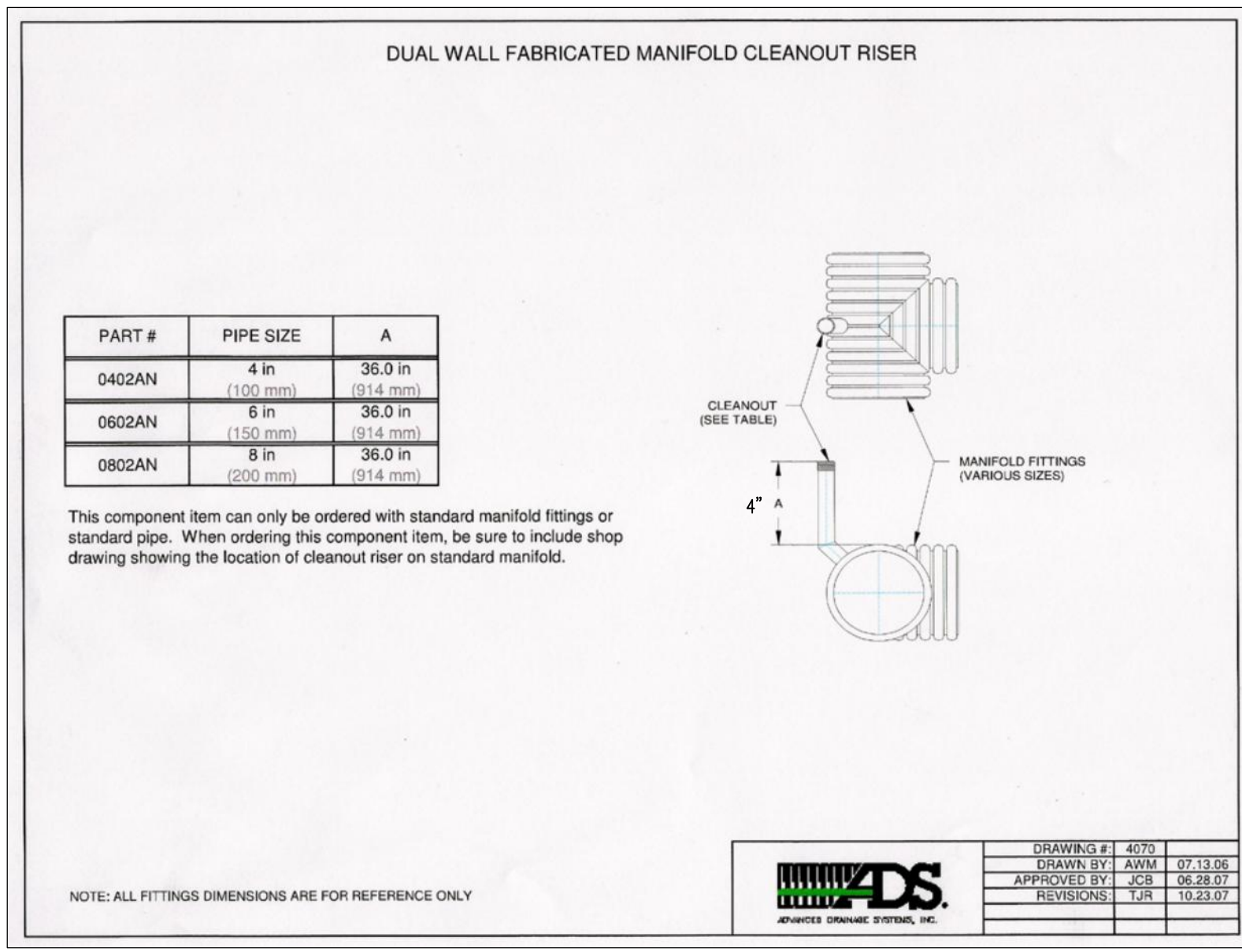
DATE	COMMENT
REVISION SCHEDULE	

PROJECT LOCATED IN:			MADE FOR:	
VIRGINIA BEACH, VIRGINIA			PER PROPERTIES	
DESIGN BY:	DRAWN BY:	CHECKED BY:	DATE:	
DRB	JB	DRB	OCTOBER 2, 2013	
	<b>GALLUP</b> <b>SURVEYS &amp; ENGINEERS, LTD.</b> 323 FIRST COLONIAL ROAD, VIRGINIA BEACH, VIRGINIA 23454 (757)425-8132 (757)425-2580 FAX		SCALE:	SHEET
			N/A	
			FILE NO:	8 / 13
				C8

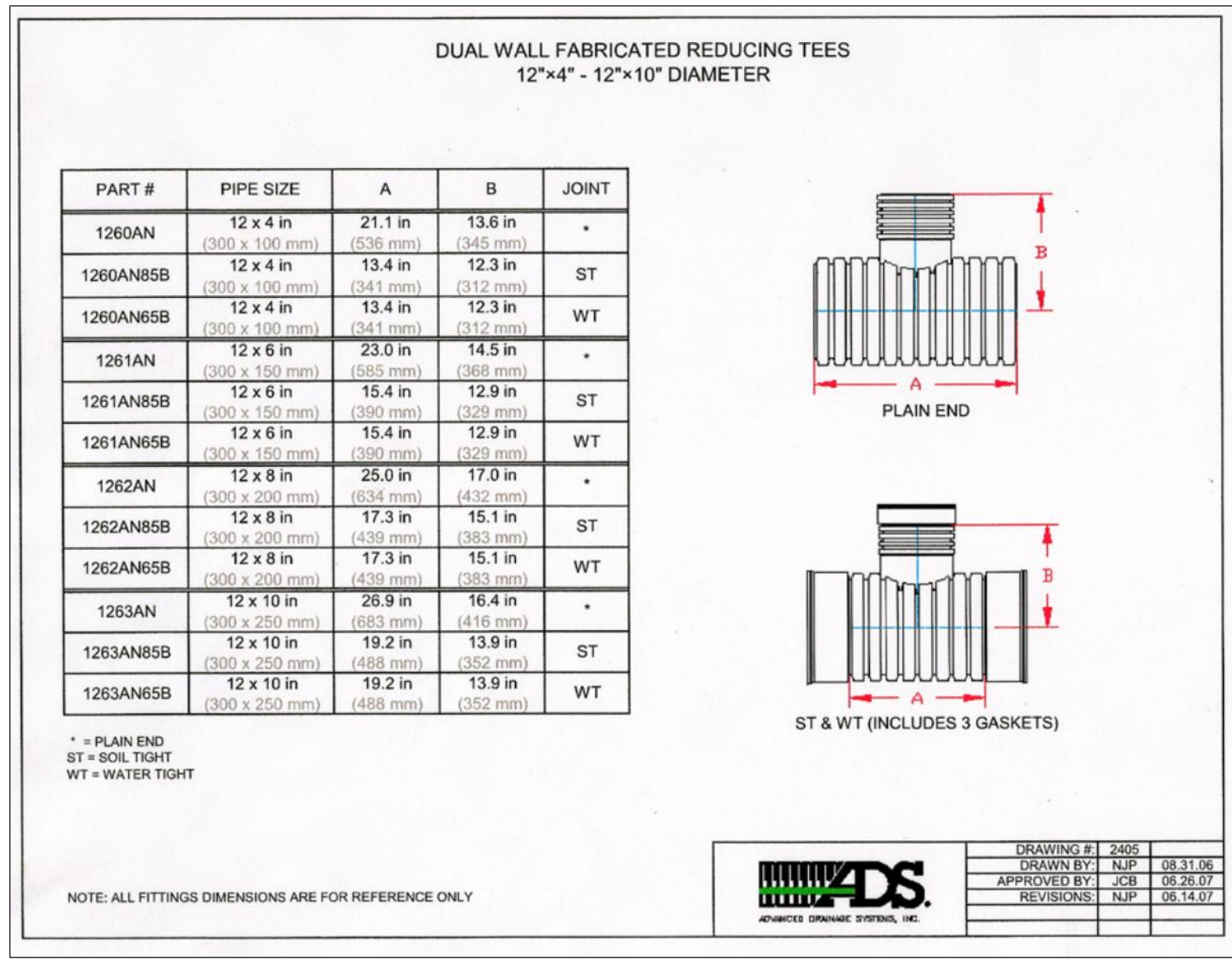




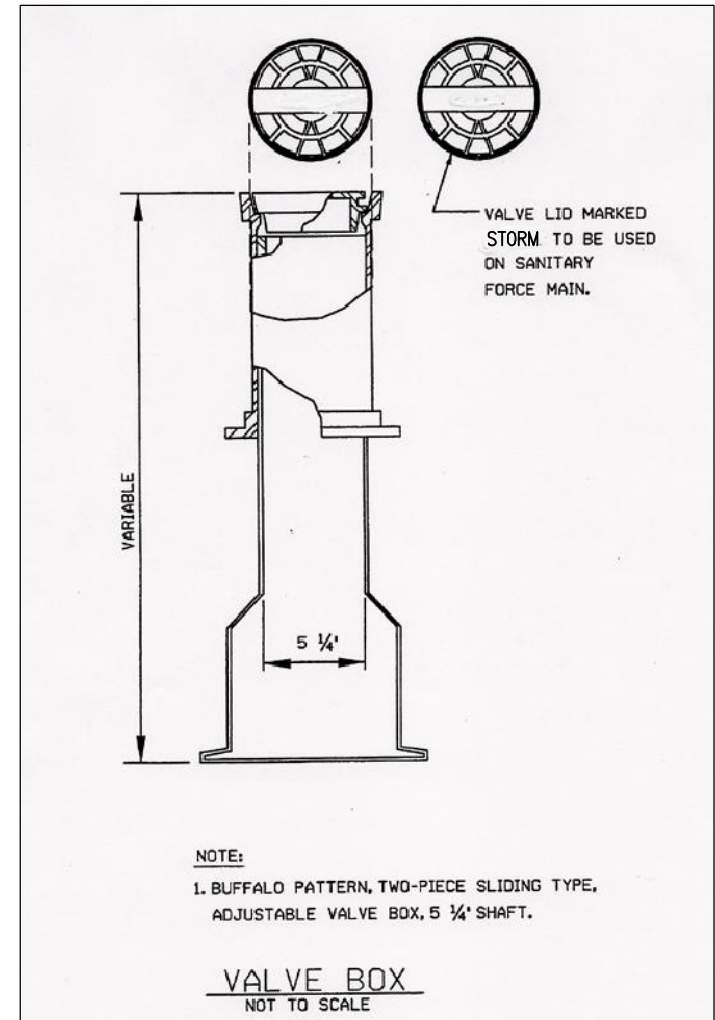
THIS DETAIL TO BE USED FOR THE 6" & 12" PLUGS FOR OBSERVATION WELL CAPS



THIS DETAIL TO BE USED FOR THE OBSERVATION WELLS



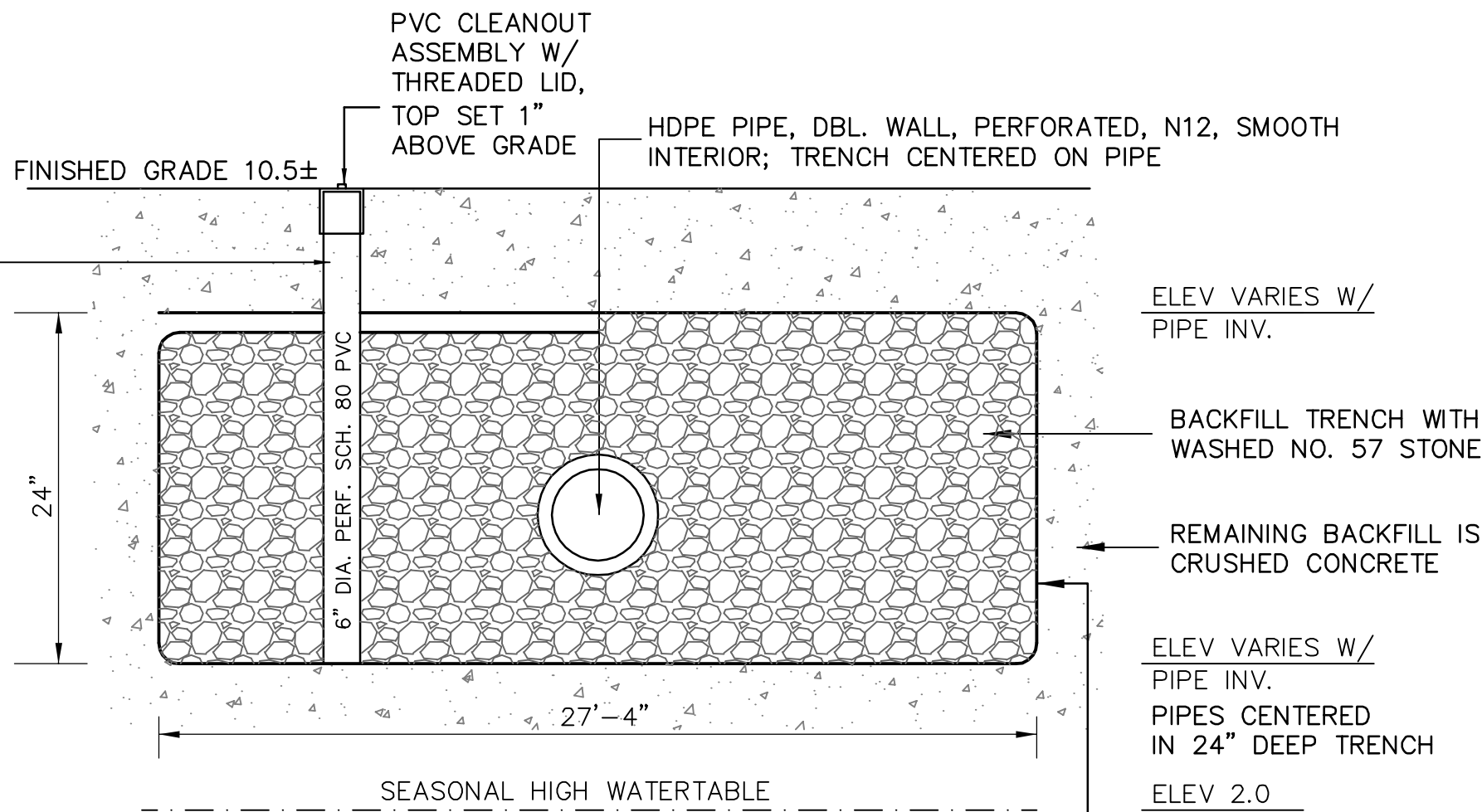
THIS DETAIL TO BE USED FOR THE 6" X 12" TEES



#### BMP MAINTENANCE SCHEDULE

1. INSPECT BMP INFILTRATION SYSTEM MONTHLY AND AFTER MAJOR STORM EVENTS FOR DEBRIS.
2. OBSERVATIONS WELLS SHOULD BE CHECKED EVERY 3 MONTHS FOR CONTAMINATION, WITH MAINTENANCE SCHEDULED AT MINIMUM SIX-MONTH INTERVALS.
3. SHOULD TRENCH FAIL TO DRAIN IN A REASONABLE AMOUNT OF TIME, (48-72 HOURS) OWNER SHALL HAVE PERFORATED PIPES JETTED AND VACUUED VIA 4" OBSERVATION WELLS AND INLETS.
4. IN THE EVENT OF COMPLETE FAILURE OF THE BMP INFILTRATION FACILITY, I.E., WATER FAILS TO EXFILTRATE WITHIN 72 HOURS AND IS VISIBLE FROM THE OBSERVATION WELLS, THE FILTER FABRIC AND DRAIN SOCKS SHALL BE EXCAVATED, AND REPLACED UTILIZING THE ORIGINAL DESIGN INVERTS AND DIMENSIONS.
5. THE OWNER SHALL KEEP A LOG OF THESE INSPECTIONS ON LOCATION FOR REVIEW BY THE CITY OF PORTSMOUTH, DEPARTMENT OF PUBLIC WORKS.
6. THE TOP 6" OF SURFACE SURROUNDING EACH STORM INLET SHOULD CONSIST OF 57 STONE ONLY, NO CRUSHED CONCRETE, IN ORDER TO PREVENT FINES FROM ENTERING THE INLETS AND CAUSING FAILURE. MINIMUM AREA OF 57 STONE AROUND EACH INLET SHOULD BE 30' DIAMETER OR GREATER.

6" DIAMETER PERFORATED SCH. 80 PVC; PERFORATIONS TO BE 3/8" DIA., SPACED ON STAGGERED ROWS 4" C-C. PROVIDE "DRAIN SOCK" OR EQUAL ON ENTIRE PERFORATED PIPE TO EXTEND FROM FINISHED GRADE SURFACE TO THE BOTTOM OF THE INFILTRATION TRENCH

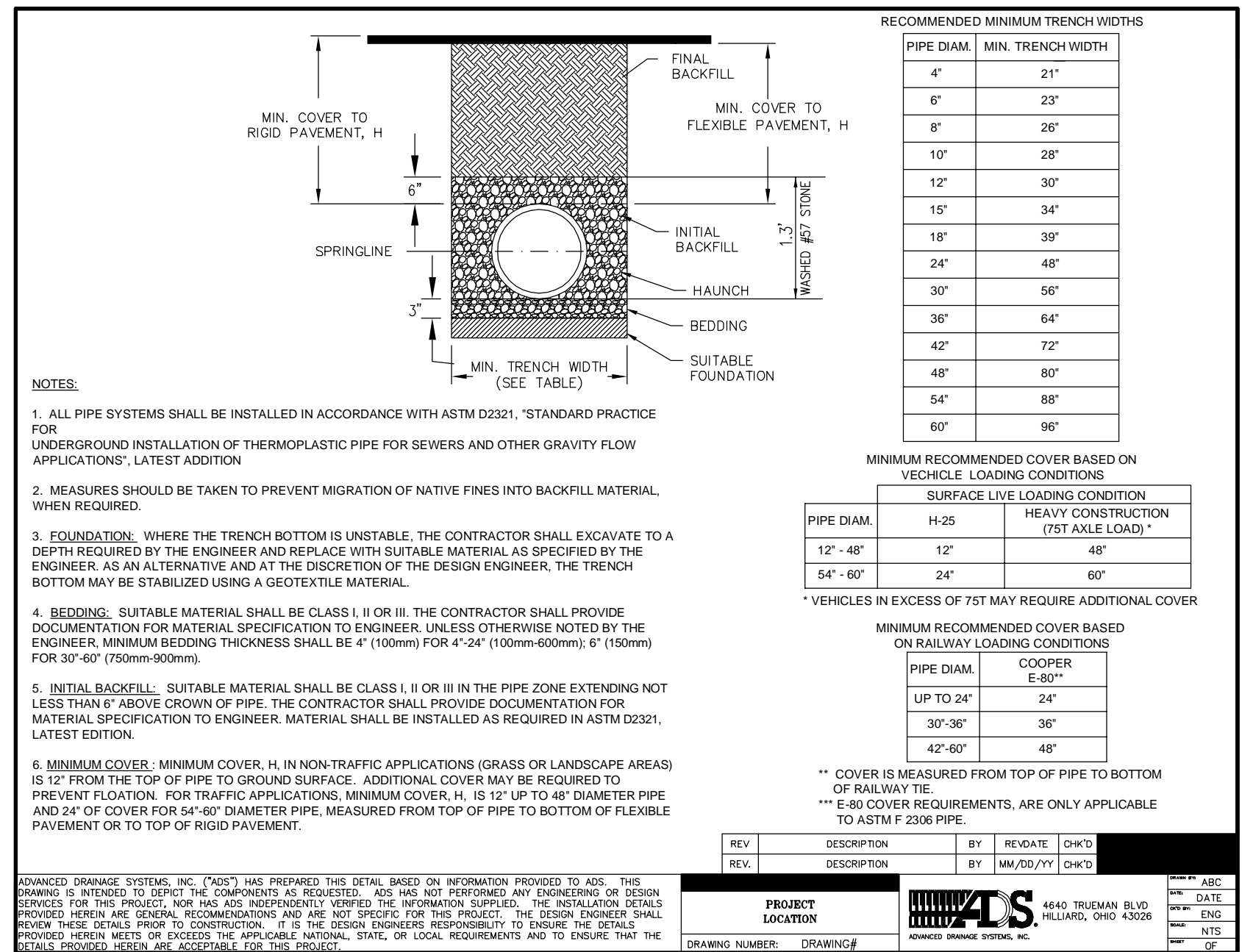


SEE SHEET 2 FOR PIPE INVERTS, LENGTHS, SLOPES, ETC.

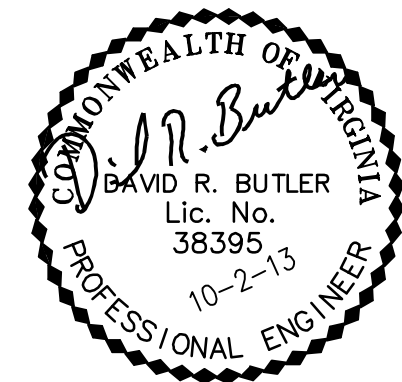
#### DETAIL

INFILTRATION BEST MANAGEMENT PRACTICE WITH OBSERVATION WELLS

NO SCALE



HDPE PIPE SHALL BE DUEL WALL, SMOOTH INTERIOR, N-12 BY ADVANCED DRAINAGE SYSTEMS, INC., OR APPROVED EQUAL

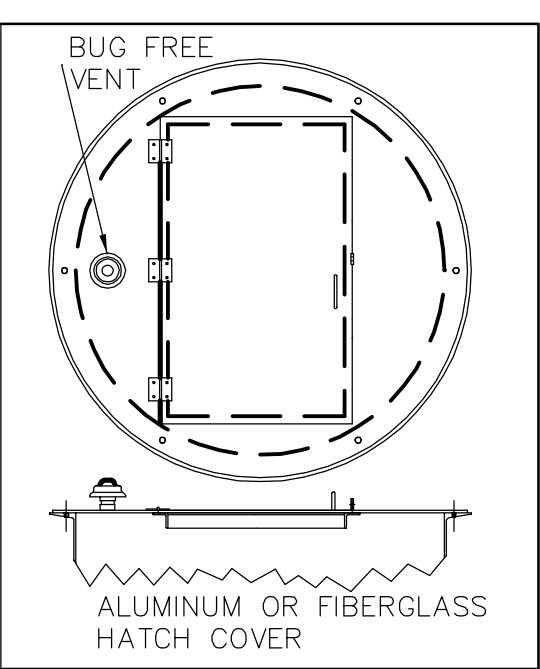
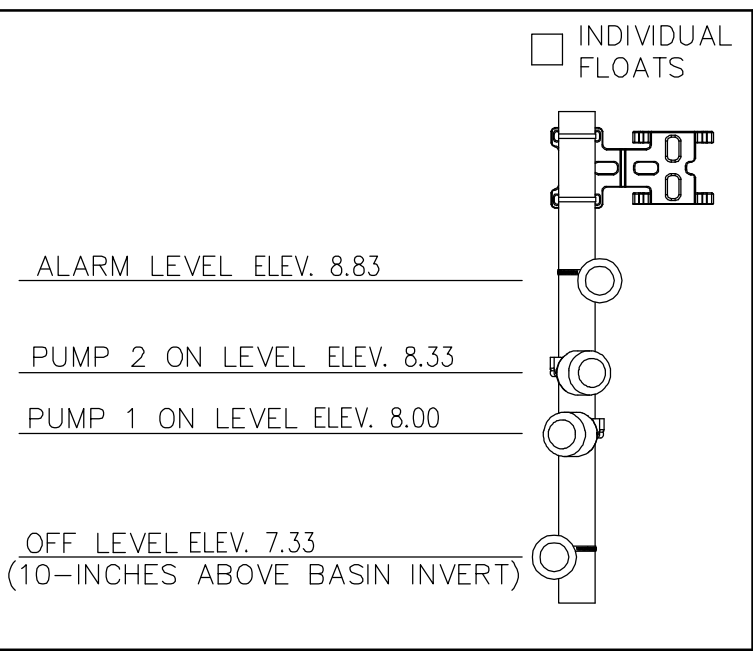
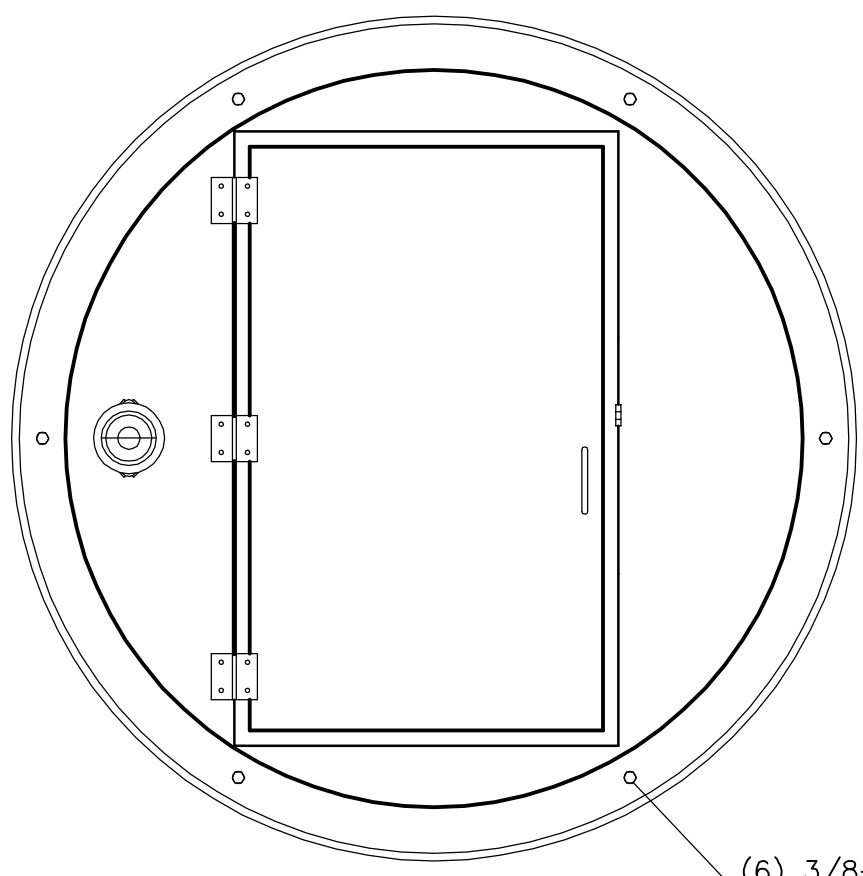
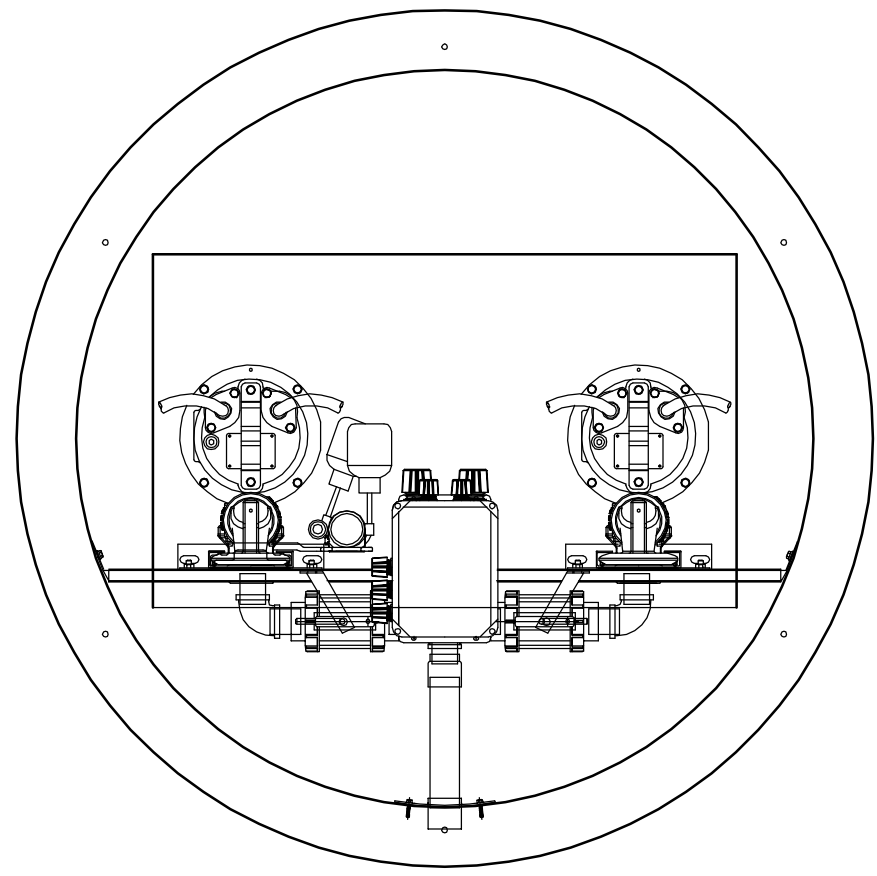


#### BMP NOTES & DETAILS

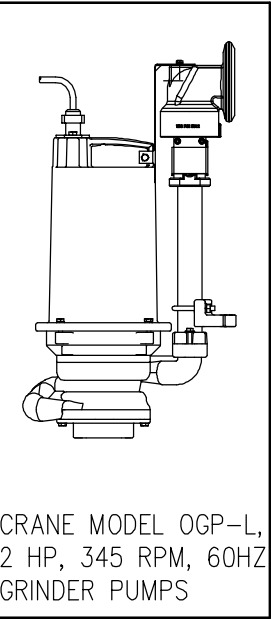
#### PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: 1" = 10'	SHEET 9/13
REVISION SCHEDULE		C9	





PUMP OPTION:

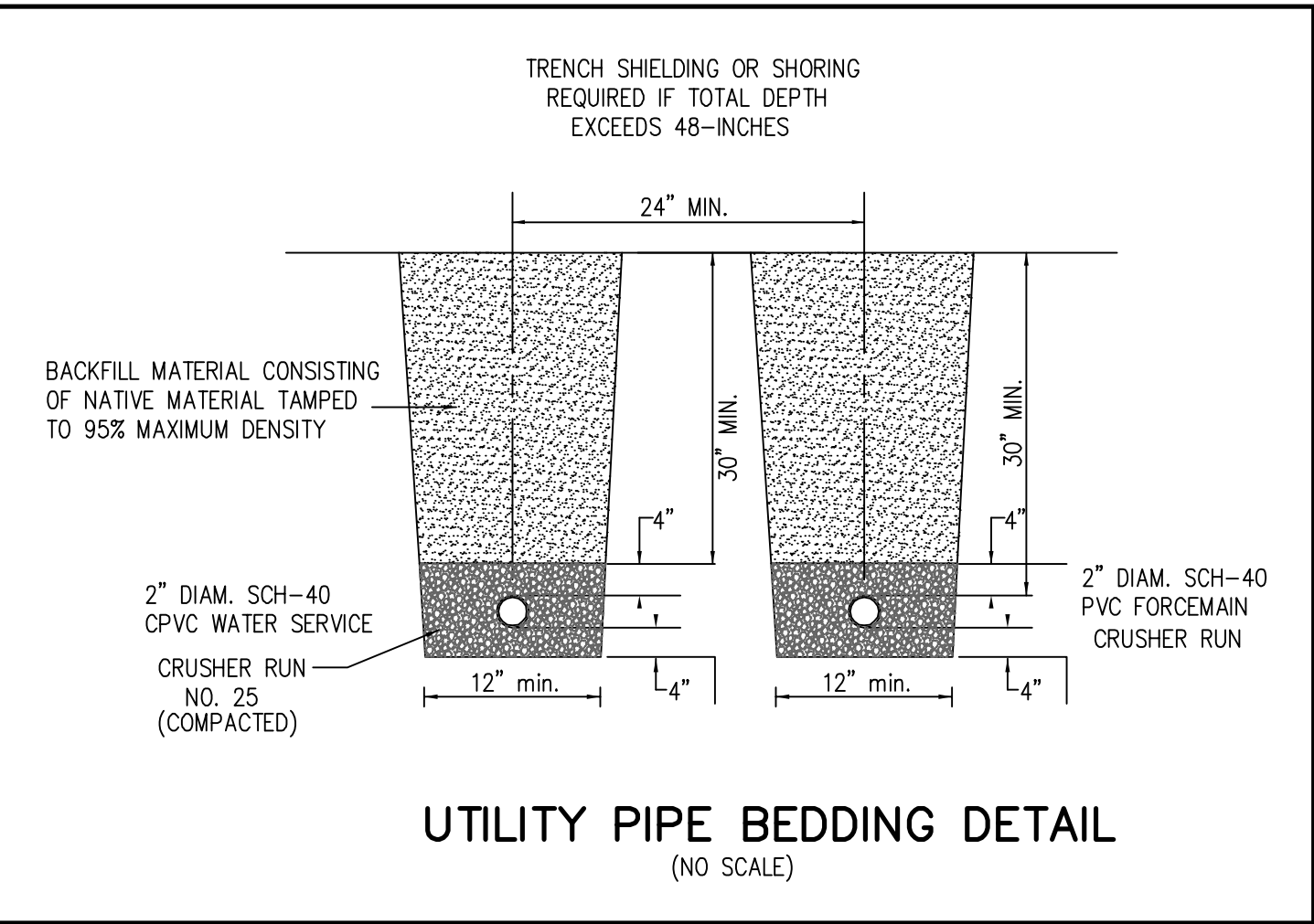
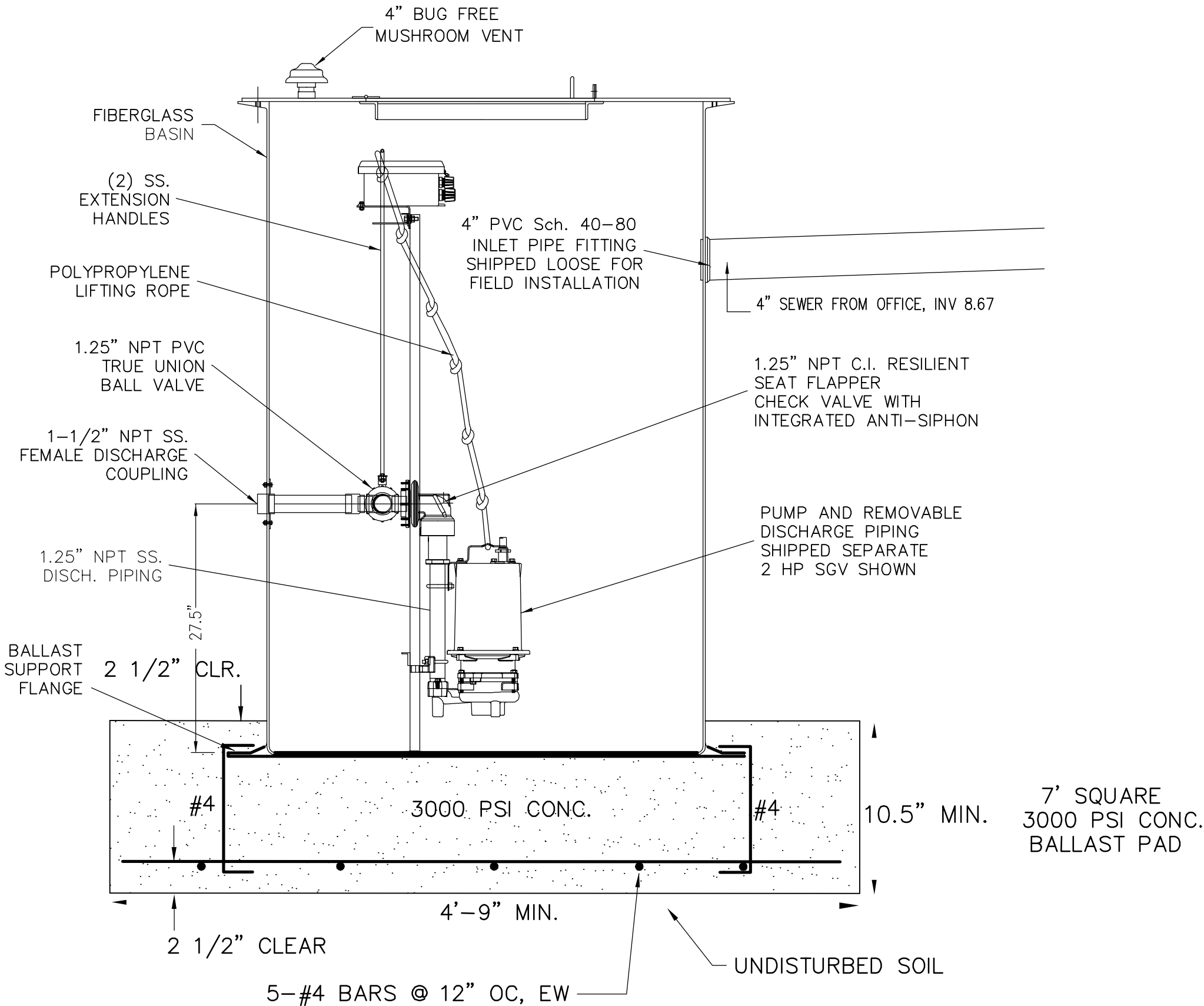
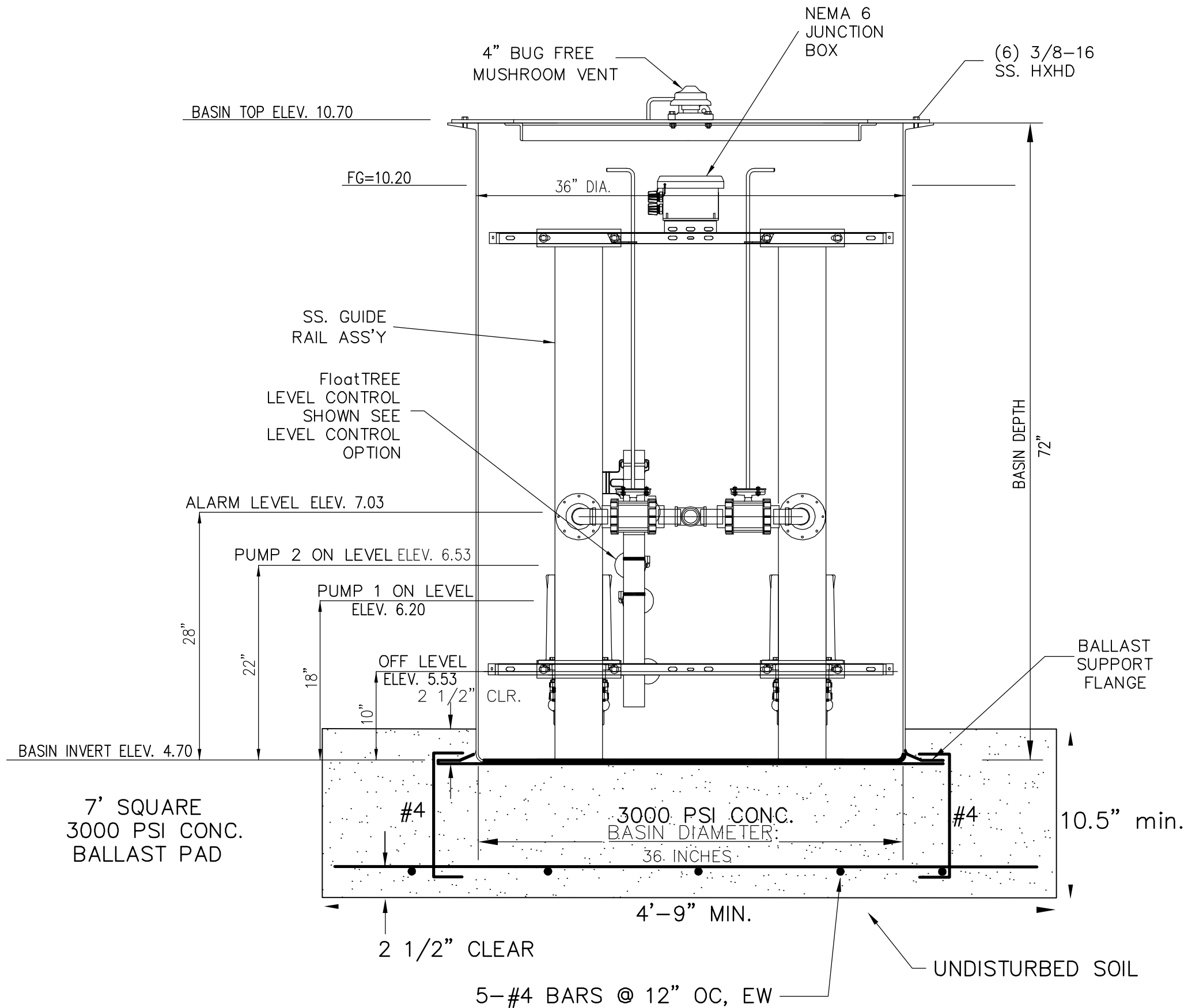


Pump Station Notes:

- Furnish and install a submersible duplex grinder pump station in accordance with the specifications. The pump shall be equipped with a 2 HP submersible electric motor. The pump shall be capable of delivering 30 GPM at 31 feet of head. Pump shall be a Crane Series OGP-L, 2 HP Grinder Pump, Single Phase, 240 V, or equal. Low voltage protection shall be provided for the motor. Installer to verify available power before ordering pumps. Impeller size: 4-inch.
- Exfiltration: All force mains shall be tested at a minimum pressure of at least 50% above the design operation pressure. Leakage shall not exceed the amount driven by the following formula:  $L = ND \frac{1}{2} \frac{3700}{P}$  Where L is allowable Leakage in gallons per hour N is the number of pipe joints D is the Pipe Diameter in inches P is the Test Pressure in PSI. The contractor shall test the pump station and force main for a minimum of 30 minutes.
- Audio and visual alarm system must be provided with and alarm test function. The alarm shall be on an independent circuit. The alarm system at the station shall be equipped with an alarm test function. Alarm shall monitor high water and power failure.
- NEMA 1 control panel to be located on the exterior wall and mounted in accordance with the NEC.
- Electrical service outlet receptacle shall be available in the vicinity of the pump station.
- A backflow prevention device will be provided on any faucet within 50 feet of the pump station.
- Provide minimum of 185 gal. of storage between alarm level and overflow elevation (top of station) within the pump well.
- A back-up power supply for the alarm system shall be provided with a minimum capacity of 24 hours.
- A weatherproof sign, containing notification procedures in the event of pump failure, shall be placed adjacent to the audio / visual alarm.

NOTES :

- ALL DIMENSIONS TO BE  $\pm 1/4"$  UNLESS OTHERWISE SPECIFIED.
- CONTACT STUART TAYLOR, TENCARVA MACHINERY CO. TO COORDINATE SALES AND DELIVERY OF EQUIPMENT  
933 CORPORATION LANE  
CHESAPEAKE, VA. 23320  
757-548-0400  
EMAIL: STAYLOR@TENCARVA.COM



PACKAGE PUMP STATION DETAILS

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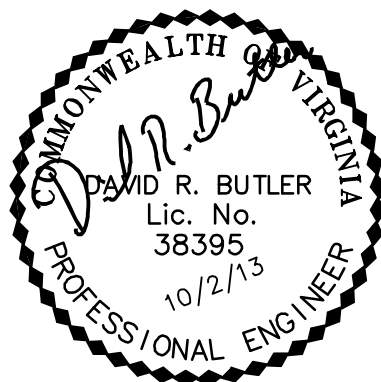
WWW.BARNESPUMPS.COM

REV  
A

CRANE

PUMPS & SYSTEMS

BARNES  
PRESSURE  
SYSTEMS



DATE	COMMENT
REVISION SCHEDULE	

PUMP STATION DETAILS

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA		MADE FOR: PER PROPERTIES	
DESIGN BY: BWG	DRAWN BY: JB	CHECKED BY: BWG	DATE: OCTOBER 2, 2013
GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX		SCALE: NO SCALE	SHEET 10/13
FILE NO.:		C10	



# "C" Channel Guide Rails for 1 1/4" NPT Moveable Fittings

www.cranepumps.com

## Accessories

15-001

## "C" Channel Guide Rails for 1 1/4" NPT Discharge Simplex or Duplex

## Specifications:

The "C" channel guide rail assembly is made of 300 series stainless steel. The guide rail mounts to the upper and lower horizontal brackets attached to the basin wall. The rail also rest on the bottom of the basin floor. The stainless steel guide rail supports the pump's required discharge from the basin floor. Guide brackets (installed with the Moveable Fitting Assembly) are attached to the pump for positioning of the unit on the guide rail during installation and removal.

The stationary of the hydraulically sealed discharge is powder coated machined cast iron. The stationary fitting has a fiber reinforced neoprene diaphragm clamped between the stainless steel rail and the stationary pressure vessel. The moveable fitting is held against the stationary fitting by the construction of the stainless steel rail, aligning the moveable fitting to the flexible diaphragm for proper sealing of the two surfaces.

### Each assembly includes:

- 300 Series Stainless Steel Guide Rail
- 300 Series Stainless Steel Upper and Lower Support Brackets
- Available For Basin Depths 4" to 16" (1.2M to 3.9m)
- 300 Series Stainless Steel Intermediate support Brackets for Basin Depths 14" (3.7m) and Greater
- Powder Coated Cast Iron Stationary Fitting
- Fiber Reinforced Neoprene Diaphragm

Quantity of One (1) each for Simplex and Two (2) for Duplex.

SECTION #  
PAGE  
DATE 11/03

**CRANE** PUMPS & SYSTEMS

www.craneumps.com

PS-051

## Specifications:

<b>DISCHARGE</b>	1½" NPT, Vertical, Ball-Joint Flange
<b>LIQUID TEMPERATURE</b>	104°F (40°C) Continuous
<b>VOLUME</b>	Cast Iron ASTM A-48, Class 30
<b>MOTOR HOUSING</b>	Cast Iron ASTM A-48, Class 30
<b>SEAL PLATE</b>	Cast Iron ASTM A-48, Class 30
<b>IMPELLERS:</b>	
Design:	12 Vane, Vortex, With Pumps Out Vokes On Back Side, Dynamically Balanced, ISO G-2.5
Material:	56-5-5 Bronze
<b>IMPELLER SPACER</b>	300 Series Stainless Steel
<b>SHREDDING RING</b>	Hardened 40C Stainless Steel
<b>CUTTER</b>	Hardwell® C-65, Hardened 40C Stainless Steel, Rockwell-C-65
<b>SHAFT</b>	416 Stainless Steel
<b>SQUARE RINGS</b>	Bar-N-V
<b>HARDWARE</b>	300 Series Stainless Steel
<b>PAINT</b>	Oil Dry Enamel
<b>SEAL:</b>	
Design:	Sing's Mechanical
Material:	Rotating Faces - Silicon Carbide Stationary Faces - Silicon Carbide Elastomer - Buna-N
Hardware:	330 Series Stainless Steel
Notes:	1) 8 Min. Seal, Correl. Custom Molded Quick Connect, for Sealing and Strain Relief
<b>CORD ENTRY</b>	
Manual:	CSA/UL Approved 1232 Type 50W
<b>UPPER BEARING:</b>	
Design:	Single Row, Angular contact Ball
Lubrication:	Oil
Load:	Radial & Thrust
<b>LOWER BEARING:</b>	
Design:	Single Row, Angular contact Ball
Lubrication:	Oil
Load:	Radial & Thrust
<b>MOTOR:</b>	
Design:	NEALA-Single Phase Torque Curve, Of-Flid, Squirrel Cage Induction Fan
Insulation:	Capacitor Start/Capacitor Run.
<b>SINGLE PHASE</b>	

**Model OGPR**  
Reduced Vortex

## Submersible Grinder Pumps

**Series: OGP**  
7HP, 3450RPM, 60Hz


CSA 100-File No. LR16667  
UL 776

### DESCRIPTION:

THE GRINDER PUMP IS DESIGNED TO  
REDUCE DOMESTIC SEWAGE TO A FINELY  
GROUND SLURRY.

**CRANE** PUMPS & SYSTEMS

SECTION A  
DATE 3/07



www.cranepumps.com

# Fiberglass Basin

With Ballast Support Flange

Accessories

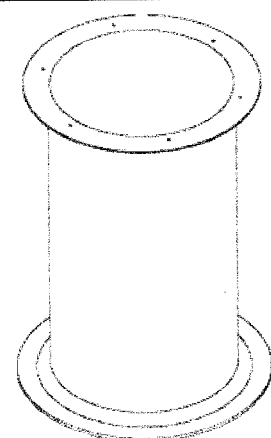
## Specifications:


Basin construction is custom molded fiberglass reinforced polyester resin.

The wall thickness shall be sufficient to withstand a water-saturated sand load of 120 lbs per cubic foot (1.9 grams/cm) with a 1.5 safety factor.

The Ballast support flange shall extend a minimum of three inches (76mm) on the radius of the basin. The flange is glassblasted to the bottom of the basin. When secured properly to a concrete pad or pouring concrete over and around the flange, prevents the basin from rising, or floating out of the ground when empty as a result of static ground pressure.

The basin will withstand a maximum temperature of 150°F (66°C).





**CRANE**

A Crane Co. Company

**PUMPS & SYSTEMS**

USA: (837) 778-8947 • Canada: (905) 457-6223 • International: (937) 615-3598

**SECTION #**

**PAGE**

**DATE**

1100

## True Union Ball Valves

1½" NPT

Product of  
USA  
www.craneump.com

### Accessories

An isometric line drawing of a True Union Ball Valve. It features a T-shaped handle with a flat top and a cylindrical grip, connected to a valve body with a flared, bellows-like end.

True Union Valves  
1½" NPT P/N: 085115

A side-view line drawing of the True Union Ball Valve handle and body. The handle is a simple L-shape, and the body is a vertical rod with a flared, bellows-like end.

Extension Handles

A logo for ISA 9001:2015 certification. It features the text "ISA 9001:2015" in a bold, sans-serif font, with "MEMBER" written below it in a smaller font.

A Crane Co. Company

### Specifications:

#### True Union Ball Valves:

The True Union Ball Valves are manufactured of Type I Schedule 80 PVC, (Cell Classification 12454-B) with EPDM O-rings for superior chemical and corrosion resistance. These valves are at 150 PSI, (10.8 kg/cm<sup>2</sup>) non-stick, with a maximum operating pressure at 73°F (23°C). The valves are of quick disconnect design for maintenance and can be repaired to component level, also full port bore, 1/4 turn, leak tight shut-off are listed by NSF for use in portable water service.

#### Extension Handle:

Made From 316\* (10mm) diameter 300 series stainless steel and can be used with 1½" NPT true union ball valves.

SECTION #  
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DATE 11/03

**CRANE**  
A Crane Co. Company

**PUMPS & SYSTEMS**

USA: (937) 778-8947 • Canada: (905) 467-6223 • International: (937) 815-3

## Level Controls

### Individual Floats Assembly,™ Duplex for Barnes™ C Channel Rail System

ESTABLISHED 1957  
www.cranepumps.com

#### Accessories

#### Individual Floats Assembly

The universal mounting bracket allows the Individual Floats to be located on either side of the "C" channel rail for ease of installation around existing inlets or other obstructions.

#### Specifications:

The Mercury Level Controls are pilot duty devices which control function of motor load devices, such as contactors, motor starters and power relays, to automatically cycle a pump or pumps. They can also be used for alarm signaling devices.

Qty. 4 floats for Duplex, Pump Off, Pump 1 On, Pump 2 On, Alarm

##### Floats Assembly:

**CORD** 182 SJOW, 29 (7.4mm) Dia

**MOUNTING** Clip, ABS/nylon and 300 series Bandspool

**FLOAT HOUSING** Polypropylene

**TEMPERATURE RATING** 97° C

**FLOAT SWITCH** Mercury, Narrow Angle, Horizontal

**FLOAT SWITCH RATING** 4.5A @ 115VAC RES  
2.5A @ 230VAC RES

**POLE** PNC

A Crane Co. Company

USA (637) 778-8947 • Canada (905) 457-6223 • International (037) 615-3590

SECTION F  
PAGE 26  
DATE 1193

www.cranepumps.com

PS-003

## Specifications:

The Moveable Fitting assembly is used with the BARNES Stainless "C" Channel Guide Rails for installation in basins.

### Each moveable assembly includes:

A stainless steel upper pump bracket with stainless hardware, stainless steel pipe nipples, cast iron flapper style check valve (powder coated) with resilient seat flapper, integrated anti-siphon and a cast iron powder coated lower guide bracket.

PUMP MODEL	SIZE-NPT Inch (mm)	PART No. W/ VALVE
OGP	1.25 (32)	1105968

Pump Not Included. Moveable fitting assembly to pump when ordered with basin package.

## Moveable Fitting Assembly for Stainless "C" Channel Guide

Access

Moveable Fitting assembly with 322" jump for Basinless or only

### Moveable Fitting Assembly 1½" NPT Discharge

#### DISCREPANCY

THE BREAK-AWAY FITTING IS DESIGNED TO ALLOW THE SUBMERSIBLE PUMP BE INSTALLED OR REMOVED WITHOUT REQUIRING PERSONNEL TO ENTER A WET WELL.

**CRANE** PUMPS & SYSTEMS

A Crane Co. Company

USA - (801) 776-8947 • Canada: (905) 437-6223 • International: (857) 616-5098

SECTION  
PAGE  
DATE

DAVID R. BUTLER  
Lic. No. 38395  
10/2/13  
COMMONWEALTH OF VIRGINIA  
PROFESSIONAL ENGINEER



GENERAL EROSION AND SEDIMENT CONTROL NOTES

- ES-1: Unless otherwise indicated, all vegetative and structural erosion and sediment control practices will be constructed & maintained according to minimum standards and specifications of the Virginia Erosion & Sediment Control Regulations (4VAC50-50).
- ES-2: All erosion and sediment control measures are to be placed prior to or as the first step in clearing.
- ES-3: A copy of the approved erosion and sediment control plan shall be maintained on the site at all times.
- ES-4: Prior to commencing land disturbing activities in areas other than indicated on these plans (including, but not limited to, off-site borrow or waste areas), the contractor shall submit a supplementary erosion control plan to the owner for review and approval by the City of Portsmouth.
- ES-5: The contractor is responsible for installation of any additional erosion control measures necessary to prevent erosion and sedimentation as determined by the City Erosion & Sediment Control inspector.
- ES-6: All disturbed areas are to drain to approved sediment control measures at all times during land disturbing activities and during site development until final stabilization is achieved, after which, upon approval of the City's Erosion & Sediment Control inspector, the controls may be removed. Trapped sediment and the disturbed soil areas resulting from the removal of temporary measures shall be permanently stabilized to prevent further erosion and sedimentation.
- ES-7: During dewatering operations, water shall be pumped into an approved filtering device.
- ES-8: The contractor shall inspect all erosion control measures at least every 2 weeks and immediately after each runoff-producing rainfall event. Any necessary repairs or cleanup to maintain the effectiveness of the erosion control devices shall be made immediately.
- ES-9: The contractor is responsible for the daily removal of sediment that has been transported onto a paved or public road surface.
- ES-10: The contractor shall be responsible for preventing surface and air movement of dust from exposed soils which may present health hazards, traffic safety problems, or harm animal or plant life.

NOTE:

ALL LAND DISTURBING ACTIVITIES MUST CONFORM WITH THE APPLICABLE REGULATIONS OF THE CITY OF PORTSMOUTH CODES, ORDINANCES, AND PWSS AND THE VIRGINIA DEPARTMENT OF CONSERVATION AND RECREATION EROSION AND SEDIMENT CONTROL HANDBOOK. THE CONTRACTOR SHALL EXERCISE EVERY REASONABLE PRECAUTION, INCLUDING THE APPLICATION OF TEMPORARY AND/OR PERMANENT MEASURE DEEMED NECESSARY BEFORE, DURING, AND AFTER CONSTRUCTION TO CONTROL EROSION AND PREVENT/MINIMIZE SEDIMENT RUNOFF. THE ENGINEERING DEPARTMENT/PERMITS AND INSPECTIONS DIVISION SHALL ENFORCE THESE REQUIREMENTS. THE CITY INSPECTOR RESERVES THE RIGHT TO REQUIRE OTHER MEASURES NOT SPECIFICALLY DESCRIBED HEREIN TO CORRECT ANY EROSION OR SILTATION CONDITION.

TABLE 3.02-A  
CONSTRUCTION SPECIFICATIONS  
FOR FILTER CLOTH UNDERLINER

Fabric Properties <sup>1</sup>	Light-Duty Entrance <sup>2</sup> (Graded Subgrade)	Heavy-Duty Entrance <sup>2</sup> (Rough Graded)	Test Method
Grab Tensile Strength (lbs.)	200	220	ASTM D1682
Elongation at Failure (%)	50	220	ASTM D1682
Mullen Burst Strength (lbs.)	190	430	ASTM D3786
Puncture Strength (lbs.)	40	125	ASTM D751 (modified)
Equivalent Opening Size (mm)	40-80	40-80	U.S. Standard Sieve CW-02215

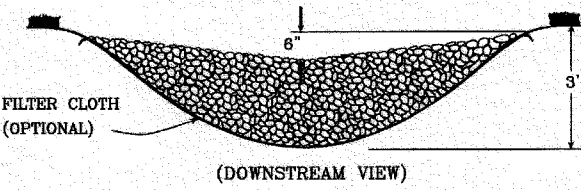
<sup>1</sup> Fabrics not meeting these specifications may be used only when design procedure and supporting documentation are supplied to determine aggregate depth and fabric strength.

<sup>2</sup> Light Duty Entrance: Sites that have been graded to subgrade and where most travel would be single axle vehicles and an occasional multi-axle truck. Examples of fabrics which can be used are: Trevira Spunbond 1115, Mirafi 100X, Typar 3401, or equivalent.

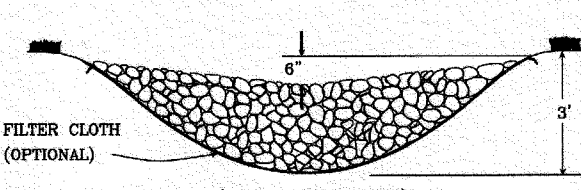
<sup>3</sup> Heavy Duty Entrance: Sites with only rough grading and where most travel would be multi-axle vehicles. Examples of fabrics which can be used are: Trevira Spunbond 1135, Mirafi 600X, or equivalent.

ROCK CHECK DAM

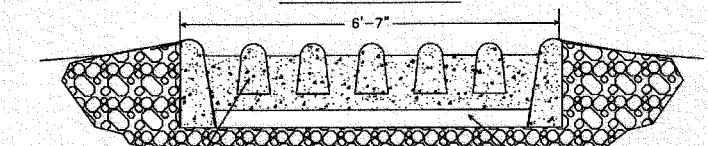
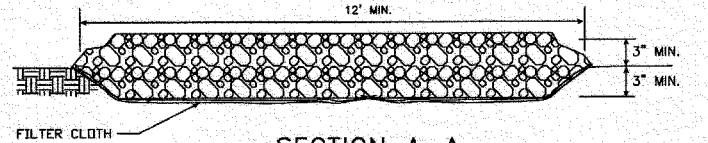
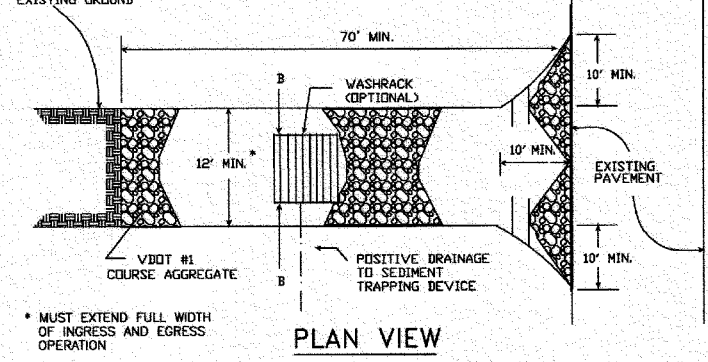
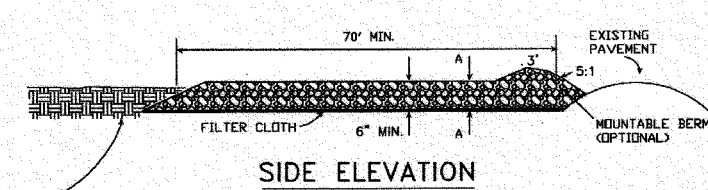
2 ACRES OR LESS OF DRAINAGE AREA:



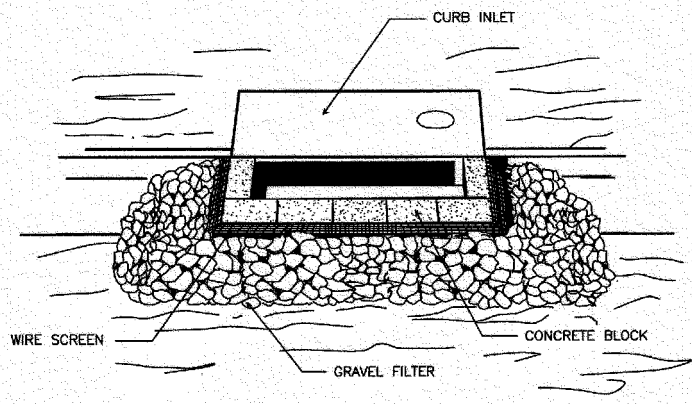
2-10 ACRES OF DRAINAGE AREA:



STONE CONSTRUCTION ENTRANCE



BLOCK & GRAVEL CURB INLET  
SEDIMENT FILTER

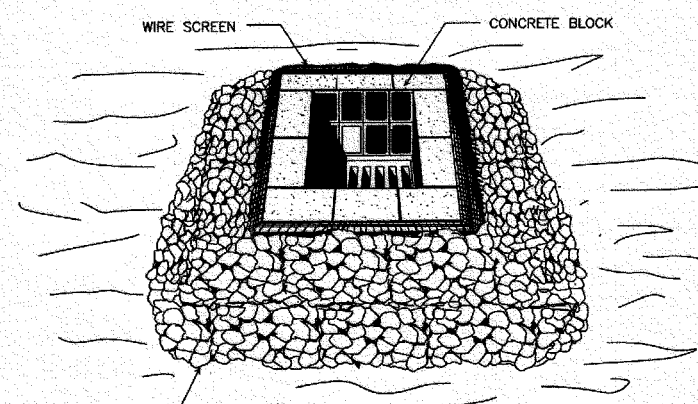


SPECIAL APPLICATION

THIS METHOD OF INLET PROTECTION IS APPLICABLE AT CURB INLETS WHERE AN OVERFLOW CAPABILITY IS NECESSARY TO PREVENT EXCESSIVE PONDING IN FRONT OF THE STRUCTURE.

- GRAVEL SHALL BE VDOT #3, #57 OR #5 COARSE AGGREGATE.

BLOCK AND GRAVEL DROP INLET  
SEDIMENT FILTER

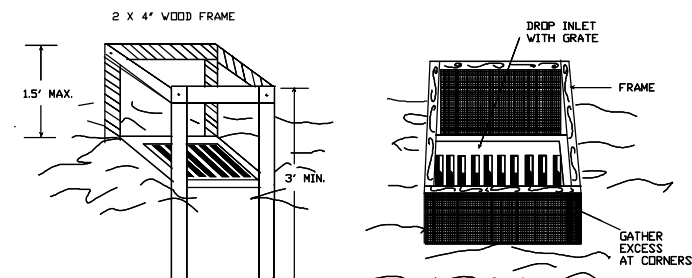


SPECIFIC APPLICATION

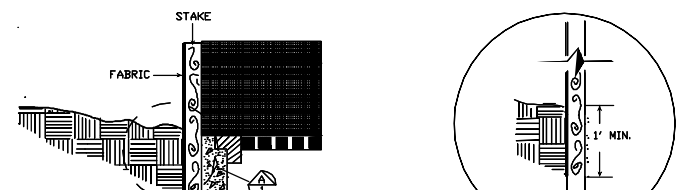
THIS METHOD OF INLET PROTECTION IS APPLICABLE WHERE HEAVY FLOWS ARE EXPECTED AND WHERE AN OVERFLOW CAPACITY IS NECESSARY TO PREVENT EXCESSIVE PONDING AROUND THE STRUCTURE.

- GRAVEL SHALL BE VDOT #3, #57 OR #5 COARSE AGGREGATE.

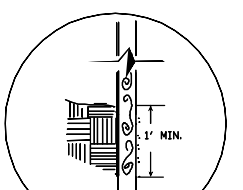
SILT FENCE DROP INLET  
PROTECTION



PERSPECTIVE VIEWS



ELEVATION OF STAKE AND  
FABRIC ORIENTATION



SPECIFIC APPLICATION

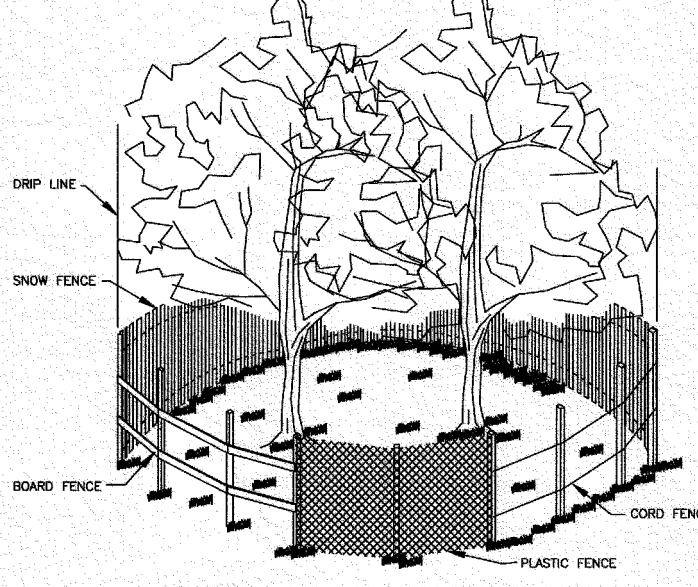
THIS METHOD OF INLET PROTECTION IS APPLICABLE WHERE THE INLET DRAINS A RELATIVELY FLAT AREA (SLOPE NO GREATER THAN 3%) WHERE THE INLET SHEET OR OVERLAND FLOWS NOT EXCEEDING 1 C.F.S.) ARE TYPICAL. THE METHOD SHALL NOT APPLY TO INLETS RECEIVING CONCENTRATED FLOWS, SUCH AS IN STREET OR HIGHWAY MEDIANS.

SOURCE: N.C. Erosion and Sediment Control Planning and Design Manual, 1988

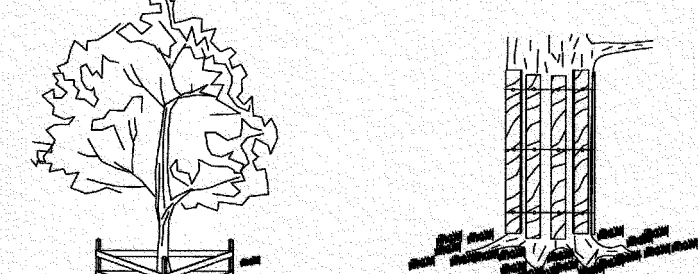
PLATE 3.07-1

INLET PROTECTION  
STANDARD & SPEC. 3.07

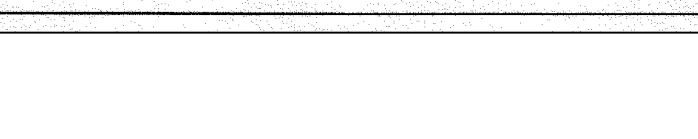
FENCING AND ARMORING



CORRECT METHODS OF TREE FENCING

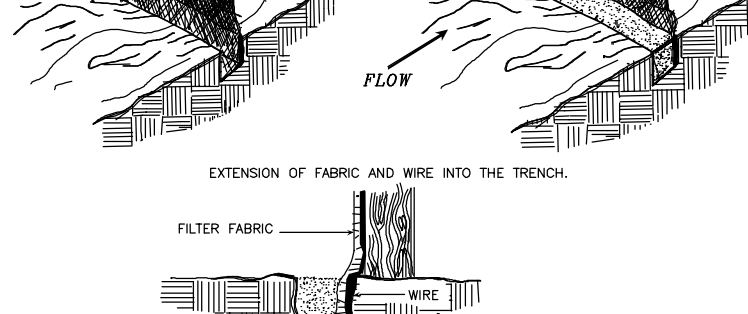
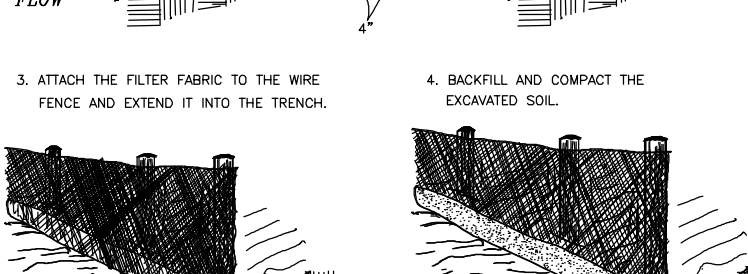
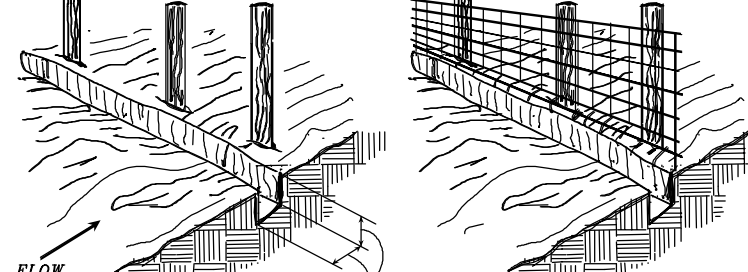


CORRECT TRUNK ARMORING



CONSTRUCTION OF A SILT FENCE  
(WITH WIRE SUPPORT)

- SET POSTS AND EXCAVATE A 4"x4" TRENCH UP-SLOPE ALONG THE LINE OF POSTS.
- STAPLE WIRE FENCING TO THE POSTS.



SILT FENCE (SF)

TABLE 3.32-E  
(Revised June 2003)  
PERMANENT SEEDING SPECIFICATIONS FOR COASTAL PLAIN AREA

LAND USE	SPECIES	APPLICATION RATES
Minimum Care Lawn (Commercial or Residential)	Tall Fescue <sup>1</sup> or Bermudagrass <sup>1</sup>	175 - 200 lbs. 75 lbs.
High-Maintenance Lawn	Tall Fescue <sup>1</sup> or Bermudagrass <sup>1</sup> (seed) or Bermudagrass <sup>1</sup> (by other vegetative establishment method, see Std. & Spec. 3.34)	200-250 lbs. 40 lbs. (unhulled) 30 lbs. (hulled)
General Slope (3:1 or less)	Tall Fescue <sup>1</sup> Red Top Grass or Creeping Red Fescue Seasonal Nurse Crop <sup>2</sup>	128 lbs. 2 lbs. 20 lbs. TOTAL: 150 lbs.
Low-Maintenance Slope (Steeper than 3:1)	Tall Fescue <sup>1</sup> Bermudagrass <sup>1</sup> Red Top Grass or Creeping Red Fescue Seasonal Nurse Crop <sup>2</sup> Sericea Lespedeza <sup>3</sup>	93-108 lbs. 0-15 lbs. 2 lbs. 20 lbs. 20 lbs. TOTAL: 150 lbs.

1 - When selecting varieties of turfgrass, use the Virginia Crop Improvement Association (VCIA) recommended turfgrass variety list. Quality seed will bear a label indicating that they are approved by VCIA. A current turfgrass variety list is available at the local County Extension office or through VCIA at 804-746-4884 or at <http://sudan.cses.vt.edu/html/Turf/turf/publications/publications2.html>

2 - Use seasonal nurse crop in accordance with seeding dates as stated below:

February, March - April	Annual Rye
May 1 <sup>st</sup> - August	Foxtail Millet
September, October - November 15 <sup>th</sup>	Annual Rye
November 16 <sup>th</sup> - January	Winter Rye

3 - May through October, use hulled seed. All other seeding periods, use unhulled seed. If Weeping Lovegrass is used, include in any slope or low maintenance mixture during warmer seeding periods, increase to 30 -40 lbs/acre.

FERTILIZER & LIME

- Apply 10-20-10 fertilizer at a rate of 500 lbs. / acre (or 12 lbs. / 1,000 sq. ft.)
- Apply Pulverized Agricultural Limestone at a rate of 2 tons/acre (or 90 lbs. / 1,000 sq. ft.)

NOTE:

- A soil test is necessary to determine the actual amount of lime required to adjust the soil pH of site.
- Incorporate the lime and fertilizer into the top 4 - 6 inches of the soil by disk or by other means.
- When applying Slowly Available Nitrogen, use rates available in Erosion & Sediment Control Technical Bulletin # 4, 2003 Nutrient Management for Development Sites at <http://www.dcr.state.va.us/sw/e&s.htm#pubs>

TABLE 3.32-D  
(Revised June 2003)  
PERMANENT SEEDING SPECIFICATIONS FOR PIEDMONT AREA

LAND USE	SPECIES	APPLICATION PER ACRE
Minimum Care Lawn (Commercial or Residential)	Tall Fescue <sup>1</sup> Perennial Ryegrass Kentucky Bluegrass <sup>1</sup>	95-100% 0-5% 0-5% TOTAL: 175-200 lbs.
High-Maintenance Lawn	Tall Fescue <sup>1</sup>	TOTAL: 200-250 lbs.
General Slope (3:1 or less)	Tall Fescue <sup>1</sup> Red Top Grass or Creeping Red Fescue Seasonal Nurse Crop <sup>2</sup>	128 lbs. 2 lbs. 20 lbs. TOTAL: 150 lbs.
Low-Maintenance Slope (Steeper than 3:1)	Tall Fescue <sup>1</sup> Red Top Grass or Creeping Red Fescue Seasonal Nurse Crop <sup>2</sup> Crownvetch <sup>3</sup>	108 lbs. 2 lbs. 20 lbs. 20 lbs. TOTAL: 150 lbs.

1 - When selecting varieties of turfgrass, use the Virginia Crop Improvement Association (VCIA) recommended turfgrass variety list. Quality seed will bear a label indicating that they are approved by VCIA. A current turfgrass variety list is available at the local County Extension office or through VCIA at 804-746-4884 or at <http://sudan.cses.vt.edu/html/Turf/turf/publications/publications2.html>

2 - Use seasonal nurse crop in accordance with seeding dates as stated below:

February 16 <sup>th</sup> - April	Annual Rye
May 1 <sup>st</sup> - August 15 <sup>th</sup>	Foxtail Millet
August 16 <sup>th</sup> - October	Annual Rye
November - February 15 <sup>th</sup>	Winter Rye

3 - Substitute Sericea lespedeza for Crownvetch east of Farmville, VA (May through September use hulled seed, all other periods, use unhulled Sericea). If Flattop is used, increase rate to 30 lbs./acre. If Weeping Lovegrass is used, include in any slope or low maintenance mixture during warmer seeding periods, increase to 30 -40

FERTILIZER & LIME

- Apply 10-20-10 fertilizer at a rate of 500 lbs. / acre (or 12 lbs. / 1,000 sq. ft.)
- Apply Pulverized Agricultural Limestone at a rate of 2 tons/acre (or 90 lbs. / 1,000 sq. ft.)

NOTE:

- A soil test is necessary to determine the actual amount of lime required to adjust the soil pH of site.
- Incorporate the lime and fertilizer into the top 4 - 6 inches of the soil by disk or by other means.
- When applying Slowly Available Nitrogen, use rates available in Erosion & Sediment Control Technical Bulletin # 4, 2003 Nutrient Management for Development Sites at <http://www.dcr.state.va.us/sw/e&s.htm#pubs>

TABLE 3.31-B  
(Revised June 2003)  
TEMPORARY SEEDING SPECIFICATIONS  
QUICK REFERENCE FOR ALL REGIONS

APPLICATION DATES	SPECIES	APPLICATION RATES
Sept. 1 - Feb. 15	50/50 Mix of Annual Ryegrass (lolium multi-florum) & Cereal (Winter) Rye (Secale cereale)	50 - 100 (lbs/acre)
Feb. 16 - Apr. 30	Annual Ryegrass (lolium multi-florum)	60 - 100 (lbs/acre)
May 1 - Aug. 31	German Millet	50 (lbs/acre)

FERTILIZER & LIME


- Apply 10-10-10 fertilizer at a rate of 450 lbs. / acre (or 10 lbs. / 1,000 sq. ft.)
- Apply Pulverized Agricultural Limestone at a rate of 2 tons/acre (or 90 lbs. / 1,000 sq. ft.)

NOTE:

- A soil test is necessary to determine the actual amount of lime required to adjust the soil pH of site.
- Incorporate the lime and fertilizer into the top 4 - 6 inches of the soil by disk or by other means.
- When applying Slowly Available Nitrogen, use rates available in Erosion & Sediment Control Technical Bulletin # 4, 2003 Nutrient Management for Development Sites at <http://www.dcr.state.va.us/sw/e&s.htm#pubs>

EROSION CONTROL  
DETAILS & NOTES

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA			MADE FOR: PER PROPERTIES		
DESIGN BY: DRB	DRAWN BY: JB	CHECKED BY: DRB	DATE:		
 GALLUP SURVEYORS & ENGINEERS, LTD. 323 FIRST COLONIAL ROAD VIRGINIA BEACH, VIRGINIA 23454 (757)428-8132 (757)425-2390 FAX			SCALE: NO SCALE	SHEET	C12
			FILE NO.:	12/13	



EROSION AND SEDIMENT CONTROL NARRATIVE

EROSION AND SEDIMENT CONTROL NARRATIVE

PROJECT DESCRIPTION

THE PURPOSE OF THIS PROJECT IS THE EVENTUAL CONSTRUCTION OF A MULTI-PURPOSE TRANSLOADING FACILITY. THE OWNER WILL CONSTRUCT A SERIES OF BUILDINGS, SILOS, A RAILROAD SIDING, AND A WHARF TO LOAD AND OFFLOAD AGRICULTURAL COMMODITIES, SUCH AS GRAIN. THE SITE IS SERVED BY CITY WATER, A PUMP AND FORCEMAIN WILL BE USED TO CONVEY EFFLUENT TO AN EXISTING SANITARY FOREMAN. THE PURPOSE OF THIS PARTICULAR PLAN IS TO SHOW GRADING AND FILLING NECESSARY TO CONSTRUCT THE PROPOSED FACILITY. THE PROPOSED WHARF NECESSARY TO ACCOMMODATE SHIP AND BARGE TRAFFIC WILL BE PERMITTED UNDER A STANDARD JOINT PERMIT PLAN. A COMMERCIAL SITE PLAN WILL BE SUBMITTED IN THE FUTURE FOR THE TRANSLOADING FACILITY. THE POST DEVELOPED IMPERVIOUS AREA WILL BE GREATER THAN THE IMPERVIOUSNESS OF THE WATERSHED. THE DISTURBED AREA DURING CONSTRUCTION WILL BE 11.2 ACRES. THE SITE IS CURRENTLY DENuded AND PARTIALLY FILLED WITH GRAVEL AND CRUSHED CONCRETE.

EXISTING SITE CONDITIONS

THE PROPOSED SITE IS RELATIVELY FLAT (SLOPE < 1.5%) AND DRAINS TOWARDS THE RIVER MOST OF THE SITE CONSISTS OF A MIXTURE OF GRAVEL AND CRUSHED CONCRETE.

ADJACENT PROPERTY

ADJACENT PROPERTIES ARE INDUSTRIAL AND A NAVAL SHIPYARD. THE NORFOLK NAVAL SHIPYARD IS LOCATED ALONG THE NORTHERN BOUNDARY. THE SOUTHERN BRANCH OF THE ELIZABETH RIVER FORMS THE EASTERN BOUNDARY OF THE SITE AND ELM AVENUE IS LOCATED ALONG THE SOUTHERN END OF THE SITE. RECONSTRUCTION OF THE JORDAN BRIDGE, LOCATED ON ELM AVENUE, BEGAN THIS YEAR AND AS A RESULT, ELM AVENUE IN THIS AREA IS CLOSED. CONSTRUCTION OF THE PER SITE, AND THE ATLANTIC WOOD INDUSTRIES SUPERFUND PROJECT WILL OCCUR SIMULTANEOUSLY.

OFF-SITE AREAS

MINOR WORK IS PROPOSED IN THE RIGHT OF WAYS TO INCLUDE UTILITY HOOKUPS. NO STREET CONSTRUCTION IS PROPOSED. ALL DEMOLISHED HARDSCAPE WILL BE HAULED TO AN APPROVED DUMP SITE. ALL CONCRETE EXISTING HAS BEEN CRUSHED AND SPREAD ONSITE. SOILS

THE SOILS REPORT PERFORMED INDICATES A CLAYEY SAND, SILTY SAND, AND LOW PLASTICITY CLAY (MIXTURE) INDICATING A LOW TO AVERAGE ERODIBILITY. THE DEPTH TO THE LOCAL GROUNDWATER TABLE IS APPROXIMATELY 2- FEET TO 6.5- FEET BELOW THE GROUND SURFACE, WITH THE SEASONAL ADJUSTED HIGH WATER TABLE ELEVATION AT 2.0

CRITICAL EROSION AREAS

THE SITE HAS SLOPES RANGING FROM 0 TO 1.5 PERCENT INDICATING A LOW EROSION HAZARD ON THE HIGH GROUND, AND 10% SLOPES ALONG THE SHORE, INDICATING A HIGH POTENTIAL FOR EROSION. THE PROPOSED WHARF WILL STOP THE EROSION.

EROSION AND SEDIMENT CONTROL MEASURES

UNLESS OTHERWISE INDICATED, ALL VEGETATIVE AND STRUCTURAL EROSION AND SEDIMENT CONTROL PRACTICES SHALL BE CONSTRUCTED AND MAINTAINED ACCORDING TO MINIMUM STANDARDS AND SPECIFICATIONS OF THE HANDBOOK. THE MINIMUM STANDARDS OF THE VESCR SHALL BE ADHERED TO UNLESS OTHERWISE WAIVED OR APPROVED BY A VARIANCE. WAIVERS MAY BE APPROVED ONLY THROUGH WRITTEN VARIANCE REQUESTS APPROVED BY THE CITY OF PORTSMOUTH.

STRUCTURAL PRACTICES

SILT FENCE BARRIER – 3.05

SILT FENCE BARRIERS WILL BE INSTALLED DOWN SLOPE OF AREAS WITH MINIMAL GRADES TO FILTER SEDIMENT-LADEN RUNOFF FROM SHEET FLOW AS INDICATED ON THE PLAN. SILT FENCE BARRIERS WILL ALSO BE PLACED AROUND THE PERIMETER NEAR THE PROPERTY LINE AND AROUND THE STOCKPILE.

TEMPORARY CONSTRUCTION ENTRANCE – 3.02

TWO 12' X 80' AND ONE 12' X 62' GRAVEL CONSTRUCTION ENTRANCES WILL BE USED FOR CONSTRUCTION ACCESS AS SHOWN ON THIS PLAN. DURING MUDDY CONDITIONS, DRIVERS OF CONSTRUCTION VEHICLES WILL BE REQUIRED TO WASH THEIR WHEELS BEFORE ENTERING THE ROADWAY. A STANDARD STONE CONSTRUCTION ENTRANCE IS SPECIFIED ON THIS PLAN.

MANAGEMENT STRATEGIES

- CONSTRUCTION WILL BE SEQUENCED SO THAT GRADING OPERATIONS CAN BEGIN AND END AS QUICKLY AS POSSIBLE.
- THE SITE IS BEING FILLED WITH GRAVEL AND CRUSHED CONCRETE. SEED AND MULCH IS NOT REQUIRED. INSTALLATION.
- THE JOB SUPERINTENDENT SHALL BE RESPONSIBLE FOR THE INSTALLATION AND MAINTENANCE OF ALL EROSION AND SEDIMENT CONTROL PRACTICES.
- AFTER ACHIEVING FULL DEVELOPMENT, THE TEMPORARY E&S CONTROLS WILL BE CLEANED UP AND REMOVED.
- STOCKPILES OF SOIL SHALL RECEIVE TEMPORARY SEEDING.

PERMANENT STABILIZATION

FILL SLOPES WILL BE STABILIZED WITH GRAVEL AND/OR RIP RAP.

STORMWATER RUNOFF CONSIDERATIONS

THE SITE WILL UTILIZE PERFORATED PIPE SURROUNDED BY GRAVEL AND WILL ALLOW FOR INFILTRATION PROVIDING BOTH WATER QUALITY AND QUANTITY CONTROL.

MAINTENANCE

IN GENERAL, ALL EROSION AND SEDIMENT CONTROL MEASURES WILL BE CHECKED DAILY AFTER EACH SIGNIFICANT RAINFALL. THE FOLLOWING ITEMS WILL BE CHECKED IN PARTICULAR:

- THE SILT FENCE BARRIER WILL BE CHECKED REGULARLY FOR UNDERMINING OR DETERIORATION OF THE FABRIC. SEDIMENT SHALL BE REMOVED WHEN THE LEVEL OF SEDIMENT DEPOSITION REACHES HALF WAY TO THE TOP OF THE BARRIER.
- EROSION CONTROLS WILL BE CHECKED REGULARLY AND ACCUMULATED SEDIMENT SHALL BE REMOVED AS NEEDED TO ENSURE THE PROPER FUNCTION OF THE DEVICES.
- INLET PROTECTION WILL BE CHECKED REGULARLY FOR SEDIMENT BUILDUP WHICH WILL PREVENT DRAINAGE. IF THE INLETS ARE CLOGGED BY SEDIMENT, THEY SHALL BE CLEANED OF SEDIMENT AND DEBRIS AND THE SEDIMENTS AND DEBRIS WILL BE HAULED TO AN APPROVED DUMP SITE.
- THE DEVELOPER SHALL MAINTAIN THE STONE CONSTRUCTION ENTRANCES BY RE-DRESSING OR REPLACING THE STONE, AS NECESSARY, TO PREVENT TRACKING OF SEDIMENTS ONTO PAVED AREAS.

CALCULATIONS

PRE AND POST DEVELOPED 10-YEAR STORM RUNOFF CALCULATIONS HAVE BEEN PERFORMED AS WELL AS WATER QUALITY CALCULATIONS. SEE "STORMWATER RUNOFF CONSIDERATIONS" ABOVE.

MITIGATION

2,721 SQ. FT. OF VEGETATED WETLANDS LOCATED AT THE SOUTHWEST CORNER OF THE SITE WILL BE FILLED BY THE EPA WITH THE PROJECT KNOWN AS "EAST SIDE CONTAINMENT FROM ATLANTIC WOOD INDUSTRIES SUPERFUND SITE." A CASH IN LIEU OF AGREEMENT IS BEING WORKED OUT BY THE DEVELOPER AND THE STATE.

DCR PLAN REVIEW MINIMUM STANDARD CHECKLIST

YES NO NA

[X] [ ] [ ] [ ]  
[X] [ ] [ ] [ ]  
[X] [ ] [ ] [ ]  
[X] [ ] [ ] [ ]  
[X] [ ] [ ] [ ]

MS-1 Have temporary and permanent stabilization been addressed in narrative?

Are practices shown on the plan?

Seed specifications?

Mulching?

Gravel?

(Permanent or temporary soil stabilization shall be applied to denuded areas within seven days after final grade is reached on any portion of the site. Temporary soil stabilization shall be applied within seven days to denuded areas that may not be at final grade but will remain dormant for longer than 30 days. Permanent stabilization shall be applied to areas that are to be left dormant for more than one year.)

[X] [ ] [ ] [ ]  
[X] [ ] [ ] [ ]

MS-2 Has stabilization of soil stockpiles been addressed in narrative?

Are sediment trapping measures provided?

(During construction of the project, soil stock piles and borrow areas shall be stabilized or protected with sediment trapping measures. The applicant is responsible for the temporary protection and permanent stabilization of all soil stockpiles on site as well as borrow areas and soil intentionally transported from the project site.)

[X] [ ] [ ] [ ]

MS-3 Has maintenance of permanent stabilization been addressed?

(A permanent vegetative cover shall be established on denuded areas not otherwise permanently stabilized. Permanent vegetation shall not be considered established until a ground cover is achieved that is uniform, mature enough to survive and will inhibit erosion.)

[ ] [ ] [X] [ ]  
[ ] [ ] [X] [ ]

MS-4 Are sediment-trapping facilities to be constructed as a first step in LDA?

Has maintenance of practices been addressed? (i.e. repair of structures and removal of accumulated sediment)

(Sediment basins and traps, perimeter dikes, sediment barriers and other measures intended to trap sediment shall be constructed as a first step in any land-disturbing activity and shall be made functional before upslope land disturbance takes place.)

[ ] [ ] [X] [ ]

MS-5 Has stabilization of earthen structures been addressed?

(Stabilization measures shall be applied to earthen structures such as dams, dikes and diversions immediately after installation.)

[ ] [ ] [X] [ ]

MS-6 Are sediment basins required where needed?

(Sediment traps and sediment basins shall be designed and constructed based upon the total drainage area to be served by the trap or basin.  
a. The minimum storage capacity of a sediment trap shall be 134 cubic yards per acre of drainage area and the trap shall only control drainage areas less than three acres.  
b. Surface runoff from disturbed areas that is comprised of flow from drainage areas greater than or equal to three acres shall be controlled by a sediment basin. The minimum storage capacity of sediment basin shall be 134 cubic yards per acre of drainage area. The outfall system shall, at minimum, maintain the structural integrity of the basin during a 25-year storm of 24-hour duration. Runoff coefficients used in runoff calculations shall correspond to a bare earth condition or those conditions expected to exist while the sediment basin is utilized.)

[X] [ ] [ ] [ ]

MS-7 Has stabilization of cut and fill slopes been adequately addressed?

(Cut and fill slopes shall be designed and constructed in a manner that will minimize erosion. Slopes that are found to be eroding excessively within one year of permanent stabilization shall be provided with additional slope stabilizing measures until the problem is corrected.)

[ ] [ ] [X] [ ]

MS-8 Are paved flumes, channels, or slope drains required where necessary?

(Concentrated runoff shall not flow down cut or fill slopes unless contained within an adequate temporary or permanent channel, flume or slope drain structure.)

[ ] [ ] [X] [ ]

MS-9 Have water seeps from slope face, adequate drainage or other protection addressed?

(Whenever water seeps from a slope face, adequate drainage or other protection shall be provided.)

[X] [ ] [ ] [ ]

MS-10 Is adequate inlet protection required on all operational storm sewer inlets?

(All storm sewer inlets that are made operable during construction shall be protected so that sediment-laden water cannot enter the conveyance system without first being filtered or otherwise treated to remove sediment.)

[X] [ ] [ ] [ ]

MS-11 Are channel lining and/or outlet protection required on stormwater conveyance channels?

(Before newly constructed stormwater conveyance channels or pipes are made operational, adequate outlet protection and any required temporary or permanent channel lining shall be installed in both the conveyance channel and receiving channel.)

[X] [ ] [ ] [ ]

MS-12 Are in-stream construction measures required so that channel damage is minimized?

(When work in a live watercourse is performed, precautions shall be taken to minimize encroachment, control sediment transport and stabilize the work area to the greatest extent possible during construction. Nonerodible material shall be used for the construction of causeways and cofferdams. Earthen fill may be used for these structures if armored by nonerodible cover materials.)

[ ] [ ] [X] [ ]

MS-13 Are temporary stream crossings of non-erodible material required where necessary?

(When a live watercourse must be crossed by construction vehicles more than twice in any sixmonth period, a temporary vehicular stream crossing constructed of nonerodible material shall be provided.)

[ ] [ ] [X] [ ]

MS-14 Are all applicable federal, state and local regulations pertaining to working it or crossing live watercourses being met?

(All applicable federal, state and local chapters pertaining to working in or crossing live watercourses shall be met.)

[ ] [ ] [X] [ ]

MS-15 Has re-stabilization of areas subject to in-stream construction been adequately addressed?

(The bed and banks of a watercourse shall be stabilized immediately after work in the watercourse is completed.)

[X] [ ] [ ] [ ]

MS-16 Has stabilization of utility trenches been addressed?

(Underground utility lines shall be installed in accordance with the following standards in addition to other applicable criteria:  
a. No more than 500 linear feet of trench may be opened at one time.  
b. Excavated material shall be placed on the uphill side of trenches.  
c. Effluent from dewatering operations shall be filtered or passed through an approved sediment-trapping device, or both, and discharged in a manner that does not adversely affect flowing streams or off-site property.  
d. Material used for backfilling trenches shall be properly compacted in order to minimize erosion and promote stabilization.  
e. Restabilization shall be accomplished in accordance with this chapter.  
f. Applicable safety chapters shall be complied with.)

YES NO NA

[X] [ ] [ ] [ ]

MS-17 Has the prevention of transporting of soil and mud onto public roadways been adequately addressed? (i.e. Construction entrances, wash racks, daily cleaning of roadways, transport of sediment to a trapping facility.)

(Where construction vehicle access routes intersect paved or public roads provisions shall be made to minimize the transport of sediment by vehicular tracking onto the paved surface. Where sediment is transported onto a paved or public road surface, the road surface shall be cleaned thoroughly at the end of each day. Sediment shall be removed from the roads by shoveling or sweeping and transported to a sediment control disposal area. Street washing shall be allowed only after sediment is removed in this manner. This provision shall apply to individual development lots as well as to larger land-disturbing activities)

[X] [ ] [ ] [ ]

MS- 18 Has the removal of temporary practices been addressed?

(All temporary erosion and sediment control measures shall all be removed within 30 days after final site stabilization or after the temporary measures are no longer needed unless otherwise authorized by the local program authority. Trapped sediment and the disturbed soil areas resulting from the disposition of temporary measures shall be permanently stabilized to prevent further erosion and sedimentation.)

[X] [ ] [ ] [ ]

MS-19 Are properties and waterways downstream from the development adequately protected from erosion and sediment deposition due to increases in peak stormwater runoff?

(Properties and waterways downstream from development sites shall be protected from sediment deposition, erosion and damage due to increases in volume, velocity and peak flow rate of stormwater runoff for the stated frequency storm of 24-hour duration in accordance with the following standards and criteria:

- Concentrated stormwater runoff leaving a development site shall be discharged directly into an adequate natural or man-made receiving channel, pipe or storm sewer system. For those sites where runoff is discharged into a pipe or pipe system, downstream stability analyses at the outfall of the pipe or pipe system shall be performed.
- Adequacy of all channels and pipes shall be verified in the following manner:
  - The applicant shall demonstrate that the total drainage area to the point of analysis within the channel is one hundred times greater than the contributing drainage area of the project in question; or
  - (a) Natural channels shall be analyzed by the use of a two-year storm to verify that stormwater will not overtop channel banks nor cause erosion of channel bed or banks.  
(b) All previously constructed man-made channels shall be analyzed by the use of a ten-year storm to verify that stormwater will not overtop its banks and by the use of a two-year storm to demonstrate that stormwater will not cause erosion of channel bed or banks; and  
(c) Pipes and storm sewer systems shall be analyzed by the use of a ten-year storm to verify that stormwater will be contained within the pipe or system.
- If existing natural receiving channels or previously constructed man-made channels or pipes are not adequate, the applicant shall:
  - Improve the channels to a condition where a ten-year storm will not overtop the banks and a two-year storm will not cause erosion to channel the bed or banks; or
  - Improve the pipe or pipe system to a condition where the ten-year storm is contained within the appurtenances;
  - Develop a site design that will not cause the pre-development peak runoff rate a two-year storm to increase when runoff outfalls into a natural channel or will not cause the pre-development peak runoff rate from a ten-year storm to increase when runoff outfalls into a man-made channel; or
  - Provide a combination of channel improvement, stormwater detention or other measures which is satisfactory to the plan approving authority to prevent downstream erosion.
- The applicant shall provide evidence of permission to make the improvements.
- All hydrologic analyses shall be based on the existing watershed characteristics and the ultimate development condition of the subject project.
- If the applicant chooses an option that includes stormwater detention, he shall obtain approval from the locality of a plan for maintenance of the detention facilities. The plan shall set forth the maintenance requirements of the facility and the person responsible for performing the maintenance.
- Outfall from a detention facility shall be discharged to a receiving channel, and energy dissipators shall be placed at the outfall of all detention facilities as necessary to provide a stabilized transition from the facility to the receiving channel.
- All on-site channels must be verified to be adequate.
- Increased volumes of sheet flows that may cause erosion or sedimentation on adjacent property shall be diverted to a stable outlet, adequate channel, pipe or pipe system, or to a detention facility.
- In applying these stormwater management criteria, individual lots or parcels in a residential, commercial or industrial development shall not be considered to be separate development projects. Instead, the development, as a whole, shall be considered a single development project. Hydrologic parameters that reflect the ultimate development condition shall be used in all engineering calculations.
- All measures used to protect properties and waterways shall be employed in a manner which minimizes impacts on the physical, chemical and biological integrity of rivers, streams and other waters of the state.

EROSION CONTROL NOTES

PORTSMOUTH TERMINAL FACILITY

PROJECT LOCATED IN: VIRGINIA BEACH, VIRGINIA

MADE FOR: PER PROPERTIES

DESIGN BY: BWG

DRAWN BY: JB

CHECKED BY: BWG

DATE: OCTOBER 2, 2013

SCALE: NO SCALE

SHEET: 13/13

FILE NO.: .

REVISION SCHEDULE

GALLUP SURVEYORS & ENGINEERS, LTD.

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